TREATISE

OF

ARCHITECTURE.

IN SEVEN BOOKS.

CONTAINING

All that is Necessary to be known in Building, with several New Designs of Houses, &c. and also the Plans of their different Situations.

In a Manner entirely New and Pleafant.

BEING AN EASY

INTRODUCTION

TO THE

Knowledge of ARCHITECTURE and BUILDING,

And for the better understanding the RULES of

VITRUVIUS, PALLADIO, SCAMOZZI,

And others both ANTIENT and MODERN.

By THOMAS ROWLAND, of New-Windsor, Gent.

To WHICH IS ADDED,

A WORK of infinite Labour and Expence, confisting of TABLES for the Mensuration of all Sorts of Works us'd in Building, of great Use and Service to all ARCHITECTS, ARTIFICERS, and MEASURERS whatsoever.

LONDON:

Printed by HENRY PARKER in Jewin-Street,

For the AUTHOR, and Sold by J. Cole, Engraver, at the Crown in Great Kirby-Street, Hatton-Garden. M.DCC.XXXII.

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PREFACE.

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ERE it not that Architecture is a Science so very large and extensive, it would hardly be imagined how so many Books could be made
without repeating one and the same thing over and over again; but in
this there is no Danger, for all that can, or ever will be said, on this
Subject, will fall infinitely short of Perfection; new Beauties will a-

rise, and elevate the Spirits of the Ingenious; there being Matter enough in the Works of Antiquity to exercise the Minds of those who delight in this Study for many Ages yet to come: I need only mention one among the many, which has not been explain'd, so as to form any just I deas of it, and that is the famous Labyrinth built by Psamniticus King of Egypt, on the Banks of the River Nile, situated on the South of the Pyramides; it is said to contain a thousand Houses and twelve Royal Palaces, all covered with Marble; a Work so stupendiously great, that it almost surpasses Belief, were it not that we are well assured, that those People were accustomed to such Works as are not to be found in any other Part of the World, as the Pyramides now standing do abundantly testify; so that I say, there is yet a large Field for those who have Leisure and Ability to oblige the World with their Labours.

I shall not presume to lay down new Rules to that which is commonly called the Orders of Architecture, I mean those of the Columns, whose several Parts and Divisions are so well establish'd, that, in my Opinion, nothing can be added to make them more beautiful; several Attempts of that Kind are to be met with, but whether with Success, must be left to Time and the Authority of the Learned in this Art; but notwithstanding this, a Man may, and must in his Compositions, use his Judgment in chusing and disposing of whatever is agreeable to him either in the Works of the Moderns or in Antiquity; but in this I am satisfied many Difficulties will arise, for it is next to impossible to bit the Taste of all, who bave different Ideas, according to their Knowledge of these Things, and indeed considering the different Customs and Humours of People in one Country or Kingdom in themselves (in some Measure of Necessity, so by the Difference of the Clime and other Accidents of Nature) and between those of Foreign Nations, that it is no Wonder to see the strange and unaccountable Variety in the several Buildings of this World, but however there are some certain and positive Rules to be used in all Countries and Places, which shall be observed in its proper Place.

MY Design, therefore, in the following Treatise, is not to give you an elegant and curious History of Architecture, that being already done by several very eminent and learned Authors; but to give you a plain, easy and familiar Method, adapted to the Understandings of those who are not at all skill in Building, and to explain all the difficult Parts (which cannot be so well comprehended in Words) by Drawings graved on Copper Plates with proper Explanations.

PREFACE

IT must be confess'd, that many and great Dissibilities attend the Study of this Art; some Books giving only Instructions how to make the several Orders of Columns, with the Divisions of their Parts, without shewing how or in what Manner, those Columns should be dissord of, nor so much as mentioning any other Part of Building; and others giving very good Directions in general, without shewing any Method, how or in what Manner to make or do what is proposed, it being very easy to say, that a Building should be durable and commodious, that the Roofs and other Parts should be framed or wrought in a strong and substantial manner, and that the Water should be carefully conveyed from the Top or Roof, &c. to some proper and convenient Place: These and many more useful Hints we often meet with in Books of Architecture, without so much as the least Directions, as is said above, how or in what Manner they should be done, the want of which after great Expence and Labour in Books and Study, leaves you just where you were, or very little improved.

IN the following Treatife you will find some or most of those Things which are so much wanted, my Design (with the Blessing of Almighty God) being to introduce all, that in my Opinion will be of Use and Service to our Buildings, that I can collect from our great Masters Vitruvius, Palladio, Scamozzi, and others both Ancient and Modern, and also from the celebrated Buildings that are in the most known Parts of the World; and to dispose of the several Parts, as well as the whole, in such a moderate Way, that the Expence shall not exceed what may reasonably be spared from the Estate of the Builder; and in this I shall use my utmost Diligence, that I may, in most humble manner, contribute all in my Power to the Advancement of this Noble Art, which I most heartly wish may be brought to the utmost Perfection in these Nations, that Great Britain may be as samous for all useful Arts and Sciences, as she is renowned for her victorious Arms abroad, both by Sea and Land.

IT will be a great Satisfaction to me, if, in the Opinion of knowing and wife Men, I have done any thing in this Treatife for the Good of Trade, by encouraging our Nobility and Gentry to amuse themselves with delightful Speculations in this fine Science, which may be a Means to induce them to lay out their Money in a good and frugal Way, to employ the poor and industrious Tradesmen, and others, who, for want of Employment, are very often reduced to the utmost Necessity. There remains nothing more to say, but that I give to Almighty God the Praises due to his most Holy Name, for enabling me to go through this very great and laborious Task, which I have done for my own Improvement, and for the Good and Benesit of Mankind in general, and that the learned and generous Reader would forgive any small Mistakes which is not possible to avoid in such a Work as this, which is divided into seven Books or Sections.

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ADDITION of WHOLE NUMBERS. and then my o from a I cannot, but a from a and there remains by that being

EXAMPLE I.

ET it be required to add, One thousand seven hundred and thirty one, to Five thousand four hundred and thirty two.

Set the Sums in Figures thus

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Then draw a Line under them, and begin at the Place of Unites. which is always the first Figure on the Right-hand, and say one and two makes three, fer the three down underneath in the Place of Unites; then fay three and three makes fix, fet the fix down in the Place of Tens; then fay feven and four makes eleven, fet down one in the

Place of Hundreds, and carry one to the next Place of Thousands, and fay, one that I carry'd, and one, is two, and five makes seven, which set down, and then you will find the Sum required to be Seven thousand one hundred and fixty three.

EXAMPLE

Let it be required to find the Sum of the following Numbers added together, viz. Nine hundred eighty feven millions, fix hundred fifty four thousand, three hundred and twenty one; Eighty seven millions, six hundred, fifty four thousand, three hundred and twenty one; Seven millions, fix hundred fifty four thousand, three hundred and twenty one; Six hundred fifty

four thousand, three hundred and twenty one; Fifty four thousand, three hundred and twenty one; Four thousand, three hundred and twenty one; Three hundred and twenty one; Twenty

one; and One or Unite.

Set the abovemention'd Sums one under another as before; the Unites under Unites, the Tens under Tens, and the Hundreds, Thoulands, Tens of Thoulands, &c. in their proper Places: Thus, viz. Nine hundred and eighty fever millions, fix hundred fifty four thousand, &c. Then Eighty seven millions, &c. and so on till you have set 987654321 down all the Sums: Then draw a Line under them, and begin at the Place of 87654321 Unites, and fay 1 and 1 is 2, and 1 is 3, and 1 is 4, and 1 is 5, and 1 is 6, and 7654321 1 is 7, and 1 is 8, and 1 is 9; fet the 9 down under the Line in the Place 654321 of Unites. Then begin at the Place of Tens, and fay 2 and 2 is 4, and 2 is 6, 5432I and 2 is 8, and 2 is 10, and 2 is 12, and 2 is 14, and 2 is 16; fet the 6 down 4321 in the Place of Tens, and carry One to the Place of Hundreds, and fay t 321 and 3 is 4, and 3 is 7, and 3 is 10, and 3 is 12, and 3 is 16, and 3 is 49, and 3 is 22; fet the 2 down under the Place of Hundreds, and carry the other 2 to 21 the next Place of Thousands, and say a and 4 is 6, and 4 is 10, and 4 is 14, and 4 is 18, and 4 is 22, and 4 is 26; fet down the 6 in the Place of Thoufands, and carry 2 to the Place of Ten thousands, and fay, 2 and 5 is 7, and 5 is 12, and 5 is 17, and 5 is 22, and 5 is 27; fet the 7 down, and carry the 2 to the next Place of Hundreds of thousands, and say, 2 and 6 is 8, and 6 is 14, and 6 is 20, and 6 is 26; fet down the 6, and carry the 2 to the next Place of Millions, and fay, 2 and 7 is 9, and 7 is 16, and 7 is 23; fet down the 3, and carry the 2 to the next Place of Tens of millions, and fay, 2 and 8 is 10, and 8 is 18; fet down the 8, and carry the 1 to the next and last Place of Hundreds of millions, and fay, 1 and 9 makes 10, which fet down, and then you will find the Sum of all the Numbers to be Ten hundred eighty three millions, fix hundred feventy fix thousand, three hundred and fixty nine. These two Examples comprehend all that need be faid in Addition of whole Numbers.

Containing forme Ufeful and Necessary Questions in .II . A H D

SUBTRACTION of WHOLE NUMBERS.

EXAMPLEI

Let it be required to subtract or take from One hundred forty five Pounds, or One hundred forty five Yards or Feet, &c. Ninety three Pounds, Yards or Feet, &c.

Set the Sums in Figures the fame as you did in Addition thus,

93

then begin at the Place of Unites, and fay 3 from 5 and there remains 2; set down the 2, and then say 9 from 4 I cannot, but 9 from 14 and there remains 5; that being set down makes the Remainder 52.

EXAMPLE II.

Let it be required to buy Eight thousand five hundred fixty seven Load or Feet of Timber, Stone, or other Materials, &c. out of which you have used or fold Seven thousand six hundred

thirty nine Loads or Feet, &c. the Question is, what remains.

Set the Sums as before, then begin at the Place of Unites, and fay 9 from 7 I cannot; therefore always in this Case borrow 1c, and add it to the upper Number which is here 7, and say 10 and 7 is 17, out of which you must take the 5, and say 9 from 17 and there remains 8, which set down, and say 1 that I borrow'd and 3 is 4, 8567 and 4 from 6 there remains 2, which set down, and say 6 from 5 I cannot, but 6 7639 from 15 and there remains 9, which set down, and say 7 and 1 that I borrowed is 8, and 8 from 8 remains nothing, which you may set down and describe by an e928 o or Cypher, or let it alone as you please, the Remainder will then be Nine hundred and twenty eight, and so much may suffice for Subtraction of Whole Numbers.

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MULTIPLICATION.

THE following Table being absolutely necessary to learn by heart, you must begin and fay twice 2 is 4, twice 3 is 6, and so on till you come to say twice or 2 times 12 is 24; then say 3 times 3 is 9, 3 times 4 is 12, and so on to the end of the Table, which I hope will be found so easy, that nothing more need be said by Way of Explanation.

The HA B L E. T on the Hold of the

EXAMPLE I.

Let it be required to multiply one hundred and thirty four by two, three, four and five.

Then fay twice 4 is 8, fet down the 8 in the place of Unites, then fay twice 3 is 6, which likewife fet down in the place of Tens, then fay twice 1 is 2, fet down the 2 in the place of Hundreds; then begin the next Multiplication by 3, and fay 3 times 4 is 12, fet down the 2 and caray 1 to the next Figure on the left hand, and fay 3 times 3 is 9 and 1 that I carry'd is 10, fet down the 0 or Cypher and carry one to the next place, and fay 3 times one is 3 and 1 that I carry'd is 4, which fet down; then begin the next Multiplication and fay 4 times 4 is 16, and fo on as you have already done in the foregoing Sums, till you have finish'd, and then you will find the Product to be, in the first Sum Two hundred and fixty eight, in the second Four hundred and two, in the third Five hundred and thirty fix, and in the fourth Six hundred and seventy.

EXAMPLE II.

Let it be required to multiply 5107 by 210, and also to multiply the Product which is 1072470, by 59, and again to multiply that Product which is 63275730 by 1795.

I be required to divide Nin handand and vigley found stillions fix bendered fifty fair

the second cined modered and tweeto, we low three handred and form slavers on the form of the fundered and

Let if be required in this case that A A A M A X 3

tients i, 32 times , and 19 times , and 1 renegating in the apprecial Sur

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character and one, de.

5107 Set down the Dimensions or Sums thus, and fay nought times 7 is nothing, nought times nought is nothing, nought 210 times i is o or nothing, and o times 5 is nothing, which fet down by cooo, 0000 then fay once 7 is 7, once nought is nought, once 1 is 1, and once 5 is 5, which 5107 fet down in the same manner as before; then say twice 7 is 14, set down 10214 the 4 and carry 1, and fay twice o or nought is nought, but I that I carry'd is 1, which fet down; then say twice 1 is 2, and twice 5 is 10, set down the 2 and the 10 as in the Example; then add or cast up the Sums as you have 1072470 been already shewn, and you will find the Product to be One million seventy two thousand four hundred and seventy, which Product multiply diby 59, wolld 19652230 produces Sixty three millions, two hundred feventy five thousand, feven hun- 9011/1 5362350 dred and thirty; that Product again multiply'd by the third Number propos'd, makes the Sum total One hundred and thirteen thousand, five hund ad line 's dred and seventy nine millions, nine hundred and thirty five thousand, three 315378650 hundred and fifty. There is nothing more to be observed here, but that you 569481570 always fet the Product of every Figure under its proper Place, the Unites under the Unites, the Tens under the Tens, and the Hundreds under the 442930110 Hundreds, &c. for if you please to observe when you began with o or no-63275730 thing in the Place of Unites, and faid nought times 7 is 0 or nothing, the o or 113579935350 nothing was fet down in the Place of Unites; the next Figure you began with was I in the Place of Tens, the Product of which was put in the Place of Tens; the next was 2 in the Place of Hundreds, and therefore you placed the first Figure of its Product, which was 4, in the Place of Hundreds, and so you must do when you come to Thousands and ten Thousand, &c. There is more expeditious ways of solving these Questions known to all Accomptants, and which may eafily be found in many Books wrote on purpose; but this being for those only who have made little or no Progress in Arithmetick, as well as for the take of Method, I am in hopes of being excused, and do most humbly desire the candid Reader to pass by what he has no Occasion for, and proceed to that Part which will require his more ferious Attention.

{ and a point of the control of the

DIVISION.

ET it be required to know how many times two there is in ninety fix, and how many times three, four and five there is in the same Sum.

Set the Sums down thus, and call the Number you divide by the Divisor, the Number which is to be divided, the Dividend, and the third Number (being so many times the Divisor in the Dividend) the Quotient; then say how many

| 2) 96 (48 8. | 3)96(32 | 4)96(24 | 5)96(19 |
|-------------------------|------------------------------|-----------------|--------------------------|
| 16 | | of the solution | |
| 1 6: 41 1 diploto 10 | l in ia dé i niya | adreis then b | uli lo s onic |

times 2 can I have in 9, which you may eafily find to be 4 times, therefore let down the 4 in the Quotient and fay 4 times 2 is 8, fet the 8 under the 9, then fubtract, and fay, 8 from 9 and there remains 1, fet that down, and then make a dot or prick under the 6, to fignify, that you have brought down the 6 to the 1, to make a new Dividend, which is a Rule you must always strictly observe; then say how many times 2 is there in 16, which you will find to be 8, set the 8 down in the Quotient and say, 8 times 2 is 16, set the 16 down underneath, and subtract as you did before, and you will find the Remainder to be 6, or nothing; so that you have 48 times 2 in 96. Now to know how many times 3, 4 and 5 there is in 96, you must begin again and say, the threes in 9 are 3 times, which must be set down in the Quotient, as in the Example, and say 3 times 3 is 9, set the 9 down under the 9 in the Dividend, and subtract as before, and bring down the 6 for a new Dividend, Sec. as in the first Example, till you have done all the Sums, or Questions, as above, and then you will find there is 48 times 2, 32 times 3, 24 times 4, and 19 times 5, and 1 remaining in the abovesaid Sum 96.

EXAMPLE II.

Let it be required to divide Nine hundred and eighty seven millions, six hundred sifty four thousand, three hundred and twenty one, by Five hundred and forty three, which is to know how many five hundreds and forty threes, there is in the abovelaid Sum of Nine hundred and eighty seven millions, &c.

ARITHMETICK. PART I.

Set down the Example in Figures thus, then fay how many times 542 can I have in 987 (the three first Figures of the Dividend) which can be but once, for twice 543 makes 1086 which is more than the 987, therefore you must set the I down in the Quotient, and fay, once 2 is 3, once 4 is 4, once 5 is 5, which fet down as you fee in the Example, then fubtract and fay, 3 from 7 and there remains 4, let that down, then fay 4 from 8 and there remains 4, fet that down, and lastly say, 5 from 9 and there remains 4, fet that down likewise, then make a prick or point under the 6, to fignify, that you have brought it down to the new Dividend, which will then be 4446, then try how many times 543 you can have in 4446, or which is easier, fay how many times 5 the first Figure towards the Lest-hand in the Divisor, can I have in 44, which you will find to be 8, fet down the 8 in the Quotient, and multiply the Divisor by it, and say 8 times 3 is 24, set down the 4 under the new Dividend, and carry 2, and fay 8 times 4 is 32, and 2 that I carry'd is 34, let down the 4 and carry 2, and fay 8 times 5 is 40, and three that I carry'd is 42, which fet down, and subtract that Sum out of the Dividend, as before, then bring down 5 the next Figure in the first Dividend, which will make you a new Dividend, and this Method must be continued till you have brought down all the Figures in the first Dividend, always remembring to make a dot or prick at the Figure when you

| 543 | 543 |
|-----------------------|--------------------------------|
| 4446 | 54566 52 7275536 9094420 |
| 1025 543 4824 | 987654012 |
| 4344 | 987654321 |
| 4803 4344 | rieste it Vervoit es |
| 45 9 2 4344 | en sio fa Standard |
| 2481 2172 | |
| 309 | |

bring it down, and also to observe, that when the first Figure of the Divisor is greater than the first Figure in the Dividend, you must take the two first Figures in the Dividend, as in the Example above, when you try'd how many times 5 there was in 44, for 4 in that new Dividend being less than 5 in the Divisor, was the Reason of the next Figure being added to it, and this is a constant Rule. The whole Work being done, you will find that there is, One million, eight hundred and eighteen thousand, eight hundred and eighty four times, five hundred and forty three (your Divisor) in Nine hundred eighty seven millions, six hundred sifty four thoufand, three hundred and twenty one, your Dividend, and three hundred and nine remaining. For the Proof of this, and all other Sums in Division, you must multiply the Divisor, by the Quotient, and take in the Remainder, when there is any, as in the Example, the Sum of this Multiplication with the remainder will always be the same as the Dividend, otherwise your Work

is falle,

CHAP. V.

ADDITION of MIXT NUMBERS.

EXAMPLE I.

ET it be required to add 36 Pounds 10 Shillings and one Penny, to 41 Pounds 5 Shillings and 6 Pence 3 Farthings.

Set them down thus, and add them together

36 10 I 41 05 6 4

This must be done in the manner as the foregoing Examples, with this difference only, that every fourth Farthing must be carried to the Pence,

and every twelfth Penny to the Shillings, and every twentieth Shilling to the Pounds, as follows in the fecond Example; there being in this but 3 in the Farthings, 7 in the Pence and 15 in the Shillings, nothing can be carried from one Denomination to the other, and therefore the 3-4ths or 3 Farthings must be set down under the Farthings; then go to the Pence, and fay 6 and 1 makes 7, fet that down under the Pence; then go to the Shillings and fay 5 and 10 is 15, which must be set under the Shillings; then in the Pounds say, 1 and 6 is 7 and 4 and 3 is 7, which being set down makes the Sum total Seventy seven Pounds sistem Shillings and seven Pence three Farthings.

EXAMPLE II.

Let it be required to add One hundred and fix Pounds twelve Shillings and nine Pence to the several Sums undermentioned, viz. Two hundred and nine Pounds three Shillings and two Pence farthing, five hundred and feven Pounds, fix Shillings and ten Pence halfpenny, One thoufand nine hundred and fifty three Pounds fixteen Shillings and five Pence three farthings, One 4500 50

hundred and twenty eight Pounds thirteen Shillings and eleven Pence farthing, Two thousand eight hundred and seven Pounds eleven Shillings and nine Pence halfpenny.

| Set down the Sums one under another thus | main (20) 03 02 4 |
|--|--|
| but the state of t | 507 06 10 1 |
| thems a februar down than my cross and array - | 1953 16 05. |
| the past of the party of the past of the p | 158 13 11. 4 |
| To which put the Sum required to be added, viz. | 105 72 09 |
| The basis and the second of the court court of the | 18118 Correction and State Contract of the Con |

Then begin with the Farthings and say, 2 and 1 is 3 and 3 is 6 and 2 is 3 and 1 is 9; then fee how many fourths there is according to the Rule aforemention'd, and you will find two and one remaining, for 2 fours make 8, which being taken out of 9 there remains 1, fet that down as before directed and carry 2 to the Pence and fay, 2 and 9 is 11 and 9 is 20, out of which take the twelfth Penny and make a dot or prick at the 9; then fay 8 that remains and 11 is 19, at which place make a dot and take 12 out of 19 there remains 7, which carry on and fay, 7 and 5 is 12, make another dot there; nothing remaining here, you must begin at the 10 and fay, 10 and 2 is 12, make another dot there, and fince there is nothing remaining you must set c, or nothing, down under the Pence, and count the number of the dots or pricks, which you will find to be 4, carry them to the Shillings and fay, 4 and 2 is 6 and 1 is 7 and 2 is 10 and 6 is 16 and 6 is 22 and 2 is 25, fet down the 5 in the place of Unites under the Shillings and carry the 2 to the next Line of Figures and fay, 2 and 1 is 3 and 1 is 4 and 1 is 5 and 1 is 6, this number being fo many 10 Shillings must be halved or divided by 2 to bring it into Pounds, say then the half of 6 is 2 and there remains nothing, set down the o, or nothing, and carry the 2 to the Pounds, which must be added up in the same manner you did in Whole Numbers, and whenever the Number of this Line of 10 Shillings is not even there will always be one or 10 Shillings remaining, as for example, suppose the Number to be 7, 9 or 11, the half of the first would be 31. 10s. the second 41. 10s. and the third 51. 10s. &c. which I or 10 Shilling must always be set down under the second Line or Column of the Shillings in the lame place where you fet the o, or Cypher.

Some Examples for the Exercise of the Learner.

| TO SECURE AND ADDRESS OF THE PARTY. | | 02 1 | 69 | | | | | | | 11 1 |
|-------------------------------------|----|-------|----|----|-----|-----|----------------------|----|--------|------|
| 75 | 16 | 03 4 | 11 | 11 | 11 | 1 | Samuel Samuel Samuel | | 三角 化二角 | 11 |
| 03 | 09 | OI 4 | 09 | 08 | 03 | 14 | | 03 | 04 | or. |
| 16 | 04 | 02 | 17 | 13 | 04 | 1/2 | | OI | 02 | 09 4 |
| 53 | 03 | 07. 1 | 31 | 02 | 09. | | | 05 | 03 | 02 |
| | | | | | | | | | | |

EXAMPLE II.

Let it be requir'd to add the feveral Quantities undermention'd together, viz. Eight hundred three Quarters feventeen Pounds and four Ounces, Seventeen hundred two Quarters fix Pounds twelve Ounces, Seven hundred one Quarter twenty fix Pounds, Fifteen hundred nineteen Pounds and eight Ounces, Four hundred one Quarter and twenty feven Pounds, and Thirty hundred three Quarters eleven Pounds and four Ounces.

| severy framely Englished rough be correct to the Person. | c. 2 | | ID | UZ. | |
|---|---------------|------|-----------------|----------------|------------|
| Set them down thus | 08 | 3 1 | 17 | 04 | |
| the property of the second of | 17 | 2 (| 06 | 12. | |
| This must be done the same as the Pounds, Shillings and Pence, &c. | 07 | | 20 March (2005) | Belling Daniel | |
| with this difference only, that every 16th Ounce must be carried to the | 15 | 0 1 | 19. | 08 | MONTH |
| Pounds, every 28th Pound must be carried to the Quarters, and every | 04 | 1 3 | 77. | 00 | |
| 4th Quarter must be carried to the Hundreds; as for example, begin at | 30 | 3 | 17. | 04 | 66 COThus |
| the 4 Ounces and fay, 4 and 8 is 12 and 12 makes 24, out of which if | To the second | | N. 20 43 | 3/4 | |
| you take 16, the Ounces in a Pound, and make a dot at 12, there will | 84 | 1 2 | 13 | 12 | STORY SANS |
| remain 8, which you must carry up and fav. 8 and 4 is 12, this being | a break | C311 | 414414 | W Ladd | |

less than 16 must be set down underneath, then carry the one Pound to the Pounds and say, 1 and 11 is 12 and 27 is 39 out of which you must take 28 and make a dot or prick at 27 and carry up the remainder, which is 11, and say 11 and 19 makes 30, out of which the 28 must be deducted as before, then make another dot or prick at 19 and carry up the remainder, which is 2, and say, 2 and 26 is 28, at which place make another dot, there being no remainder you must go on and say, 6 and 17 is 23, which being under the Number of Pounds in one Quarter of a Hundred you must set down underneath, and carry the number of dots or pricks, which is 2, to the Quarters of Hundreds and say, 3 and 3 is 6 and 1 is 7 and 1 is 8 and 2 is 10 and 3 is 13, every sourch part being taken out (which is the same as to divide 13

7

by 4) there will be 3 and 1 remaining, for 3 times 4 is 12 which from 13 remains 1, fet the 1 down and carry the 3 to the Hundreds and fay, 3 and 0 is 3 and 4 is 7 and 5 is 12 and 7 is 19, and so on as you did in Addition of Whole Numbers, and then you will find the Sum to be Eighty four Hundred one Quarter twenty three Pounds twelve Ounces. Be pleas'd to obferve here, that One hundred Weight of Lead, Iron or Brass, &c. is 112 th, half a hundred 56 th, and a quarter of a hundred 28 th, and is seldom weigh'd nearer than to a quarter of a Pound, therefore instead of Ounces you may set down the Halfpounds and Quarters, &c. in the same manner you did in the Farthings, &c. An Example or two is set down for the Exercise of the Learner.

| C. 2 | o makes are which being & w | c. | Qrs | . њ | 16 |
|------|-----------------------------|----|-------------------------|------|-------------|
| | 16 1 | 31 | 0 | 124 | 1 2 |
| 06 I | | 16 | . 2 | 09 : | 4 |
| | 11 2 | 07 | 0 | 03 | 4 |
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Let it be required to add three Miles six Furlongs ten Poles and 11 Feet, to forty one Miles sive Furlongs thirty three Pole and ten Feet.

Set down the Miles, &c. as in the Margin, and add them together as before, only observing that every 16 Foot and a half, which is the Length of a Pole or Perch, must be carried to the Poles, and every 40th Pole to the Furlongs, and every 8th Furlong to the Miles. Begin then and fay, 11 and 10 is 21, out of which if you take 16

Miles Furl. Poles Feet
41 5' 33' 10'
03 6 10 11

the Number of Br under the Lishes a failter your One that halver and or

Foot $\frac{1}{2}$ there remains 4 Foot $\frac{1}{4}$, which must be set down as you see in the Example, and carry 1 to the Poles and say, 1 and 10 is 11 and 33 is 44, out of which you must take 40 and set down the remainder which is 4, and carry 1 to the Furlongs and say, 1 and 6 is 7 and 5 is 12, out of which you must take 8 and set down the remainder, which is 4, then carry 1 to the Miles and say, 1 and 3 is 4 and 1 is 5, set that down and say, 4 is 4, which likewise set down, and then the Sum of both will be 45 Miles 4 Furlongs 4 Poles and 4 Foot $\frac{1}{2}$.

EXAMPLE IV.

Let it be required to add fixteen Acres three Roods and twenty seven Rods or Perches to thirty six Acres one Rood and eleven Perches.

Set down the Acres and Roods, &c. and add them together as in the other Examples, only remembring that 40 Perches or Poles makes a Rood or one quarter of an Acre, and that 4 Roods make an Acre, which must be carried to their several Denominations as before, and this is a constant Rule in all Examples of Addition of Mix'd Numbers.

Acres Roods Perches
36 1° 31°
16 3 27

53 1 18

a Number of Plant and fee down, the Remainder which and car with the Countries of the Early Anx (Duants, Co. as you have already and the presence of the whole is complement.

Let it be required to add five Years three quarters eleven Weeeks four Days seventeen Hours and fifty two Minutes, to twenty one Years and a half nine Weeks five Days twenty three Hours and thirteen Minutes.

Set down the Years and Quarters, &c. and add them together, but first be pleased to observe that every 60 Minutes must be carried to the Hours, and every 24 Hours to the Days, every 7 Days to the Weeks, every 13 Weeks to the Quarters, and every 4 Quarters to the Years; this will do well enough for

Tears Qrs. Weeks Days Hours Min.
21 2' 09' 5' 23' 13'
05 3 11 4 17 52
27 2 07 3 17 05

the common Division of the Year, tho' not exactly true, for there is 365 Days and very near one quarter of a Day in one Year, so that in four Years there is almost one Day lost, which is added every fourth or Leap Year: This however in common Practice may be sufficient; begin then and say, 52 and 13 is 65, and that in 65 Minutes there is 1 Hour and 5 Minutes, which 5 must be set down and the Hour carried to the Hours, and so on till you have sinish'd your Addition according to the Rules before observ'd.

burns) there will be a sed a remaining, for a times a for a which from as repairs, the the when the state of the state of the EX A Map L Edwyt and of a and then you are and the Sum

Let it be required to add thirty Feet eleven Inches and three quarters, to fifty feven Feet ten Inches and a half.

Feet In. Set down the Dimensions, as in the Margin, and please to say, that a 4ths 57 10 1 and one half is 5, which being divided by 4 the Number of Quarters in an 30 11. Inch there will remain one, fet down the one Quarter, and carry I Inch to the Inches, and fay 1 and 11 is 12 and 10 makes 22, which being divided by 12 the Number of Inches in a Foot, the remainder, which is 10, must be set down under the Inches and carry 1 Foot to the Feet, and fay 1 and 7 is 8 and 3 and 5 is 8, which finishes your Question; but in some Cases it may be requisite to add other Parts of Inches, then halves and quarters, &c. and therefore I will give another Example.

EXAMPLE

Let it be required to add the several under-written Dimensions together, viz, One hundred and fix Feet eleven Inches and one quarter, Forty nine Feet ten Inches and three quarters, Ninety feven Feet and feven twelfths of an Inch, One hundred and forty three Feet and eleven twelfths or parts of an Inch, and Fifty nine Feet four Inches and a half.

In this Example the Inches are supposed to be divided into twelve Parts, and that when the Dimension happens to be one quarter, or one half, or three quarters, the Parts will be 3, 6 and 9, that is to fay 3 for one quarter, 6 for one half, and 9 for three quarters.

Feet Inches Parts Set down the feveral Dimensions one under another, and add them up to-106 11 gether as before, and divide the Parts by 12, as well as the Inches. In the 049 10 Parts the Number is 36, which being divided by 12, the Quotient will be 097 00 07 3, and nothing remain, therefore fet down o underneath the Parts, and 143 10. 11. carry the 2 to the Inches, and fay 3 and 4 is 7 and 10 is 17, Gc. till the 059 04 06 whole is added up, making in all 38, which being divided by 12 the Quotient will be 3 and the Remainder 2, which must be set down, and the 3 457 carried to the Feet, and added up with them, as in Whole Numbers, Ge.

EXAMPLE VIII.

Let it be required to add fix Tons two Pipes three Hogsheads, fifty fix Gallons, three Quarts, and two Pints, of Wine or Water, &c. to eleven Ton, one Pipe, two Hogsheads, thirty nine Gallons, two Quarts, and three Pints of the same Liquor; or which is the same thing, to know the Sum total of the above-mentioned Quantities, which is, or may be disposed of in two separate Cellars or Vaults, &c.

Set down the Sums or Quantities but before you begin to add, obierve, that two Pints make one Quart, four Quarts make one Gallon, lixty three Gallons one Hogshead, two Hogsheads one Pipe, and two Pipes one Ton. Then fay 2 and 3 is 5, which must be divided by 2, the Number of Pints in a Quart, and fet down the Remainder which is 1, and carry 2 the Quotient to the next Denomination of Quarts, &c. as you have already done in the preceding Sums, till the whole is compleated.

Tons Pipes Hbd. Gall. Qrts. Pts. 11 1 2 39 2 3 06 2 3 56 3 2

03.

09

Let it be required to add free Years three quarters eleven were to have their feventeen VI. . sent the row of the court some CHAP.

SUBTRACTION of MIXT, NUMBERS.

N these Questions I shall follow the Method already gone through in relation to the several Denominations in Mixt Addition, as Money and Weight, &c. which I suppose the Learner by this time to be well acquainted with.

EX AM PILIE I

Let it be required to subtract, or take from 45 to 5 s. 6 d. 4, the Sum of 36 l. 10 s. 1 d. 1. Eventsed Hours and fifty-two Minutes, from tivetity-one Years three Quirers nine W

Set down the Sums as in the Margin, the leffer under the greater. H south Anova did ovil This must be done the same as you did in Subtraction of whole Num- from 45. 05 6 \frac{1}{4}

bers, only remembring what you have already learn'd as to the Parts take 36 10 1 \frac{1}{2}

of the Pounds, and therefore begin at the Farthings, and say, 2 from

1 cannot, but 2 from 4 (the Number of Farthings in one Penny,

which on this Occasion you borrow) there remains 2, and 1 Farthings above makes 3, which set down; then go to the Pence, and say, 1 that I borrowed and

from 6 there remains 4, which set down then say 10 from 5 I cannot but 10

1 is 2, and 2 from 6 there remains 4, which set down, then say, 10 from 5 I cannot, but 10 from 20 (the Number of Shillings in a Pound which you borrow) and there remains 10, which being added to the 5 above makes 15, fet that down and fay, 1 that I borrow'd and 6 is 7, and 7 from 5 I cannot, but 7 from 15 there remains 8, set the 8 down, and say, 1 that I borrow'd and 3 is 4, and 4 from 4 there remains o or nothing, which finishes this Sum, there remaining 81. 155. 4d. 4. or parts, from one hundred and fix Feet eleven fuches and one

Some Examples for Practice of and solution of I be some Examples for Practice of the solution of I and the solution of the sol take can lent 1234 19 11 4 paid 1195 16 10 4 remains to pay 0039 03 00 1 remains to pay 174 04 2 4

EXAMPLE II.

THE BUILD OF YOU AND CHARLES FOR THE PARTY DATE OF SECURITY OF THE

CARLOWIA TO A TO A SOLA

Let it be requir'd to take fix Pound one Quarter three Ounces, from twenty-four Pound three Quarters fixteen Ounces 1.

C. Qrs. 15 from 24 3 16 4 Set down the Sums and begin at the Quarters of Pounds, and fay, one Quarter is a Quarter, which being fet down underneath, you must say, 3 from 16 and there remains 13, which set down, remains 18 2 13 4 then fay, I from 3 and there remains 2, fet that down, and fay, 6 from 4 I cannot, but 6 from 14 and there remains 8, then fay, 1 that I borrowed and o is 1 which from 2 there remains 1, let that down, and then you will

first throughout The nesticit Some Examples for Practice.

find remaining eighteen Hundred two Quarters thirteen Pound and one quarter.

c. ors. the 10 ½ from 36 2 27 ½ 2 19 to aholise) a l'acrity take 03 1 19 1 remains c9 2 18 4 and modern remains

remains a, which for down, III E I II M A X E was to

Let it be requir'd to take fixteen Acres three Roods and thirty-feven Perches, from thirty-The tender that the state of the Acres Roods Peribes fix Acres one Rood and twenty-one Perches.

Set the Sum down and subtract in the same manner as you have from 36 1 21 done before, only allowing for the difference of the Quantities in take 16 3 37 the feveral Denominations which you must take care to remember; therefore fay, 37 from 21 I cannot, but 37 from 1 Rood or 40 Perches that I borrow, and there remains 3, which Remainremains 19 1 24 der must always be added to the upper Number.; then say, 3 and 21 makes 24, which set down and carry 1 that you borrowed to the Roods, and fay, 1 and 3 makes 4, which from I I cannot, but 4 from 1 Acre or 4 Roods that I borrow remains o or nothing, which o or nothing being added to 1 the upper Number is but 1, fet that down and carry the 1 Acre you borrow'd to the Acres and fay, 1 and 6 is 7, which from 6 you cannot, but 7 from 16 there remains 9, fet that down and fay, 1 and 1 that I borrowed is 2, and 2 from 3 remains 1, that being fet down finishes the Sum.

tion lay, whom will cannon

EXAMPLEAW.

Let it be requir'd to take or subtract five Years two Quarters eleven Weeks four Days seventeen Hours and fifty-two Minutes, from twenty-one Years three Quarters nine Weeks five Days twenty-three Hours and thirteen Minutes is migrall add ni as anne all nwob to

Set down the Sums or Quantities as usual, the from 21 03 09 05 23 13 lesser under the greater, and in subtracting observe take 05 02 11 04 17 52 the Method already shewn, which I hope is sufficient, and then you will find the Remainder to be sixteen remains 16, 00,011,05,021 Years eleven Weeks one Day five Hours and twentyout; nwob set doubter as asken avode guids t is a, and a from 6 there remains 4, which let down, then lay, to from 5 I can estuniM ano

which being added to the s above mais of chia dwarf and lay, that I borrow'd and 6 is 7, and 7 from 15 there remains 8, fet the 8 down, and fay, r

from 20 (the Number of Sailings in a Pound which you borrow) and there remains re-

Let it be requir'd to take forty-nine Feet seven Inches and three Quarters, or nine twelfths or parts, from one hundred and fix Feet eleven Inches and one Quarter, or three 12th parts, of an Inch.

The former Rules being observed, you will find the Remainder to be 57 Feet 3 Inches and is or an Inch.

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soon of the second of the second of the second

Some EXAMPLES for Practice.

Feet Inc. Feet Inc. remains 088 04 4

Set down the Suns and begin avhe and MANX, and from cot 3 far, one Quarter is a Quarter, which being ict cown underneath, rake co r

Let it be requir'd to subtract or take from eleven Ton one Pipe two Hogsheads thirty-nine Gallons two Quarts and three Pints, fix Ton two Pipes three Hogsheads fifty-fix Gallons three Quarts and two Pints.

This Example is for the Exercise of the Learner, and somewhat different from the foregoing Rules, but may with little Study be found out; however, for fear of discouraging the Learner, the Sum may be fet down the same as underneath the first Example: The greatest

difficulty is at the Hogsheads, but as 3 Hogsheads is 1 Pipe and I Hogshead, the best way is to leave the 3 Hogsheads out, and add I Pipe and I Hogshead in lieu of them to the from 6 Tons 2 Pipes, &c. as in the Example underneath, and then it will be 7 Ton 1 Pipe 1 Hogshead 56 Gallons, &c. which being fet down as in the fecond Example in the Margin, your fubtraction will then

be easy, saying 2 from 3 there Tons Pipes Hbd. Gall. Octs. Pts. remains 1, which set down, 6 2 3 56 3 2 then fay, 3 from 2 I cannot, but 3 from 4, the Number of Quarts in a Gallon, there remains and at top makes

2 3 56 3 2 I 00

II I 2 39 take 06 2 3 56 04 0 0 45 Tons Pipes Hhd. Gall. Qrts. Pts. take 07 I ah naorah sakar o 7 1 1 56 300 000 000 00 00 45 230 1 x1

Tons Pipes Hhd. Gall. Qrts. Pts.

3, which being fet down, and the t Gallon that you borrow'd carry'd to the Gallons and work'd in the same manner as before, will soon finish this Question, the Remainder being 4 Tons o Pipes o Hogsheads 45 Gallons 3 Quarts and 1 Pint. ber; therefore last, and them at I cannot, but an arrow a Rood or

der must giways besadded to the upper Number; then fay, a end an males a , which for down and carry within you borrowed to the Roods, and tay, I and a malica at which from * I cannot but I from a Acre or a Roods that I borrow remains o or nothing, which o or nothing being added to I the upper Number is but I, fet that down and carry the a Acre you corrowed to the Acres and fay, i and e is 7, which from 6 year cannot, but f from 16 there were had come that down and fay, 1 and 1 that 1 befrowed is 2, and 2 flows a remains 1, that

the Author the Sun.

EXAMPLE

(Lodshi book H X P. IIVII. I 9 M A K H

MULTIPLICATION of MIXTANUMBERS.

Let it be required to multiply twelve Feet fix Inches, by fix Feet nine Inches.

Before you begin to multiply it will be necessary for you to know, that Feet multiplied by Feet produce Feet, Feet multiplied by Inches and divided by 12 produce Feet and Inches, Inches multiplied by Inches and divided by 12 produce Inches and first parts, or first parts of Inches, the first parts of Inches multiplied by Feet and divided by 12 produce Inches and first parts, first parts multiplied by Inches and divided by 12 produce Inches and first parts, first parts multiplied by Inches and divided by 12 produce first and second

parts, and lastly first parts multiplied by first parts and divided by 12 produce second and third parts: This being well understood, the working of the Sums or Dimensions will be very easy; therefore set down the Sum or Dimension required as in the Margin, then multiply the Feet by the Feet which makes 72, set down the 72 underneath the Feet, then multiply the lower Feet by the upper Inches as you see it mark'd, and the upper Feet multiply by the lower Inches, and first multiply the lower Feet by the upper Inches, saying, 6 times 6 is 26, which being (according to the above Rule) divided by 12 makes just 3 Feet o Inches remaining, set down the 3 under the Feet and say, 9 times 12 is 108, that divided by 12 produces 9 Feet, which likewise set down under the Feet, then multiply the Inches by the Inches, saying, 6 times 9 is 54, which being divided

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by 12 makes 4 Inches and 12 or 6 parts, fet that down as in the Example, and add up the Particulars as you have already been taught in the feventh Example of MIX'D ADDITION.

EXAMPLE II.

Multiply One hundred thirty Feet nine Inches and one 4th, by Two hundred fifty one Foot fix Inches and three 4ths.

Set down the Dimensions under one another and multiply the Feet by the Feet as in common Multiplication; then multiply the lower Feet by the upper Inches and divide by 12, saying, 9 times 251 is 2259, which being divided by 12 makes 188 Feet 3 Inches, set that down as in the Example; then multiply the lower Inches by the upper Feet, saying, 6 times 130 is 780, which being divided by 12 makes 65 Feet, set that down in its proper place; then multiply the Inches by the Inches, saying 6 times 9 is 54, divide that by 12 the Quotient is

4 Inches and 6 Primes or first parts of Inches, set that down as in the Example; then multiply the upper Primes or first parts of Inches by the lower Feet and fay, 3 times 251 is 753, which divided by 12 makes 62 Inches and 9 parts, this you may if you please set down as it is, but it will be better if you divide the 62 Inches by 12; the Quotient will then be 5 Foot 2 Inches and 9 parts. which fet down as you fee in the Example; then fay, 9 times 120 is 117c, divide that by 12 twice as you did before, and then the Quotient will be 8 Foot 1 Inch and 6 Parts, which being fet down underneath the last Sum, you may proceed, and multiply the Inches by the Parts or Primes crois-ways, as you did the Feet and Inches, that is, the upper Inches by the lower Parts, and the lower Inches by the upper Parts, faying, 6 times 3 is 18, which divided by 12 makes one Part or Prime and 6 feconds, fet that down as in the Margin; then fay, 9 times 9 is 81, that being divided by 12 makes 6 Primes or first Parts and 9 seconds, that being set down under the proper Denomination of Parts and seconds, &c. we come lastly

to multiply the Parts or Primes by themselves, saying, 3 times 9 is
27, which being divided by 12 makes 2 seconds and 3 thirds, set them down, and cast or add up the several Sums to know the Sum required, which is 32897 Feet, 0 Inches, 5 Primes, 5 seconds and 3 thirds.

There are several other Ways of multiplying Feet and Inches, &c. some of which I shall endeavour to explain in as short and as easy a Method as is possible, leaving it to the Choice of the Practitioner to use which Way he likes best.

second Multiplication is the fame as the fift, observing the Rules before municald as to the

before, is much the calledt Way when the helps are in even parts, that we

Feet In. Primes

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130

650 260

tgust be let shown as in the Brample, Co.

MAKE HIgures; the third hindiplestion is the tank, only when you come to implify the vect by the Feet by the Feet, there is then no Division, but the whole quantity that they produce

Multiply fix Inches a

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CHALLET TO

EXAMPLE III. (Being the Second Method.)

Let it be required to multiply fix Foot fix Inches, by three Foot nine Inches. Set down the Dimensions as you did before, and mark with dots or pricks as many places towards the right-hand as your Dimension consists of, beginning always at the lowest Denomination, then multiply in the same manner as you do in whole Numbers; there is only this difference, which is of carrying one Denomination to another after you have divided by 12; as for example, begin then and fay, 9 times 6 is 54 and the twelves in Feet Inches 54 is 4, for 4 times 12 is 48, which from 54 there remains 6, fet down the 6 in the farthest place of Primes or Parts of an Inch, which is mark'd out 63 09 on the right-hand of the Dimension and say, 9 times 6 is 54 and 4 that I carried is 58, which being divided by 12 makes 4 Foot 10 Inches, let that down as in in the Margin and fay, 3 times 6 is 18, that being divided by 12 makes one Foot 6 Inches, fet the 6 down as in the Margin and fay, 3 times bridge soupers 6 is 18 and 1 is 19, that being fet down and the Parts added up, finishes this Question, and here be pleas'd to observe, that as in Multiplication of whole Numbers the first Figure of the second Multiplication is always put under the second Figure or Place of Tens in the first Line or Multiplication, so in this we place the first Figure of the fecond Multiplication in the fecond Place or Denomination from the first, and so likewise in the third Multiplication, when it confifts of three Places, the first Figure is placed in the third Denomination from the first Place on the right-hand, as in these Examples following, which a little Practice will make familiar. Let us now proceed to one or two Examples more in this fecond Way or Method, which I delire the Learner to practife before he proceeds to the other Ways abovemention'd, and then I hope he will find the Work to be still more pleasant and cally, ou bbs bas plomer by in makes a Indice and

MOITIGE A.M. Some EXAMPLES for Practice. Desiles and any se risinging

| Feet | Inches | Parts | | | | | | | Feet | Inches | Parts | |
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EXAMPLE IV. (Being the Third Manner.) at Inches and a Princes or first parce of Justice for that down its in

Let it be required to multiply fifteen Feet six Inches and three quarters, by 5 Feet six

In the Methods abovemention'd the greatest Difficulty is when the Feet are in two or three Numbers, which obliges you to fet down the Multiplication and Division on another Piece of Paper or in another Place, to avoid which you may divide the Feet by 12 and multiply the Inches by that Quotient and Remainder if any, and this you will find very eafy in all small Dimensions; but to be a little more particular, be pleas'd to observe, that in the fecond Example of Multiplication of Feet, Inches, &c. you said 6 times 130 was 780, and then divided by 12 in this Method, you fay only, 6 times 10 Foot 10 Inches is 65 Foot, or when the Inches are in equal Parts, as in the Example aforemention'd, 6 Inches being the half of one Foot or 12 Inches, you may fay, the half of 130 Feet is 65, and if it had been 4 Inches you must have divided the Feet by 3, 4 Inches being the third part of one Foot or 12 Inches. A few Examples will make this Method very eafy; let us proceed then and multiply the 15 Feet 6 Inches and three quarters, by 5 Feet 6 Inches and a half. 10 61 0 20min 0 War docks, argust 4

Set down the 15 Feet, 6 Inches, &c. as before, and fay, 6 times 9 is Feet In. Pts. 54, which being divided by 12 there remains 6; then fay, 5 times 6 is 36 15 6 9 and 4 that you carry is 40, that being divided by 12 there remains 4; 05 6 6 then instead of faying 6 times 15 is 90, and dividing by 12, Foot 3 In 2 and 7 9 4 10 the 15 by 12 in your Head, and keep the Quotient which is 7 Foot 3 In 2 and 7 9 4 16 ches in your mind and fay, 6 times 3 is 18 and 3 that you carried is 21; 107 which is 1 Foot 9 Inches, set down the 9 Inches and say, 6 times i is 6 77 and 1 is 7, or if you had pleas'd to say, the half of 15 is 7 Inches and 6 parts and 3 that you carried is 7 Inches and 9 parts; this, as I faid 186 2 10 10 6 before, is much the easiest Way when the Inches are in even parts, the second Multiplication is the same as the first, observing the Rules before mention'd as to the placing the Figures; the third Multiplication is the same, only when you come to multiply the Feet by the Feet, there is then no Division, but the whole quantity that they produce must be set down as in the Example, &c.

Some EXAMPLES for Practice.

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| Feet multiplied by Feet | | (1969,66 | A in | | 2172 | 0 | 0 | tion of b | 7 6. 6 5. 10 |
| The lower Inches multi- | 7 | 6 | · o - | <u>\</u> | 2715 { 135 | | | 200 | 135 9 8 9 · 9 · 2715 |
| The upper Inches multi- plied by the lower Feet } | | | ő — | 65-6 | | 0 | | | 29478 5 9 2 10 |
| The lower primes or parts of Inches multiplied by the upper Feet | 0 | 7 | 6 - | | 7 | 6 | 6. | K b | nh ne gallmotte a di nhà trea thea mais a line |
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| | 86 | 2 | 10 10 | 6 | 29478 | 5 | 9 | 2 | 10 |

The GOLDEN RULE;

Or RULE OF THREE.

THE Method to be observed in this Rule is first to state your Question, then to make your first and third Numbers of one Denomination, to multiply the second and third Numbers together and divide by the first, and the Quotient is the Answer to your Question. But, before you can proceed to work according to the above Rule, it often happens, that the first and third Numbers, tho' of one Name or Denomination, yet have different Parts, as halves or quarters of Pounds or Yards, &c. and whenever this happens, they must be reduced into the same Parts or Denomination one as the other; you must also, before you multiply your second and third Numbers together, reduce your second or middle Number into the same Denomination you care to have your Answer in: For Example, if your second or middle Number happens to be Pounds, Shillings, Pence and Farthings, it must be brought into Farthings; so likewise if you would know to a Farthing what any thing will cost (when there is no Farthings in the middle Number) you must bring the middle Number into Farthings. A few Examples will explain these Rules better than many Words, which very often consound and perplex, more than instruct the ingenious Reader.

EXAMPLE I.

If six Pounds is given for a hundred of Deal Boards, what will six cost at the same Price?

State your Question as in the Margin, and say, if 120 (the Number of Boards which is always sold for a hundred) cost 6 l. what will 6 cost; then bring your 6 l. into the lowest Denomination, as Farthings, by multiplying the Pounds by 20 to bring them into Shillings, and the Shillings by 12 to bring them into Pence, and the Pence by 4 to bring them into Farthings, as in the Margin; then multiply 5760 your middle Number in Farthings by 6 your third Number, and divide the Contents of that Multiplication, which is \$456c, by 120 your first Number; then divide 288 the Quotient by 4 to bring the Answer to your Question into Pence; and lastly divide the Pence by 12 to bring it into Shillings: The Price being thus found for the 6 Deals, you may if

you please know what one Deal will cost by dividing the Price of the 6 Deals, which is 6 Shillings by 6

the Number of Deals, and then you will find each Deal

Deals
If 120 cost 6 what will 6 cost

20

120 shillings

12

1440 pence

4

5760 farthings
6 the third Number

12'(0)34560(

4)288

12)72 pence

6)6 shillings the price of 6 Deals

ber, Gc.

This Method well observed will be of great Use in many Questions in to cost one Shilling. the Rule of Three, &c. Some Examples for Londing

EXAMPLE II.

Let it be required to know what fix Load and a half of Oak Timber will cost, when two Load and a quarter is fold for Five Pounds twelve Shillings and lix Pence.

Tond that says of If 2 f cost 5 12 6 what will 6 f cost at the same rate State your Question thus, and say, Shillings 26 Then, according to the Rule above, 12 of Inches weak place make your first and third Numbers of one Denomination by bringing them The relative for the contract of T into Quarters of Loads, and taking in the Fractions as in the Example; then farthings bring your middle Number into the 26 t de cintere en factoria de la constante de la lowest Denomination of Farthings as before, and multiply the 5400 Far-32400 and the street and the second things by your third Number, which 10800 is 26 Quarters, and divide by 9 the to parts and epical become first Number; then divide 15600 the 9)140400 Quotient by the same Numbers you the Quotient 4)15600 multiplied the middle Number, as in the Example above, which will pro-12)3900 duce the Sum required, being 16 1. 5 s. for 6 Load and a half of Oak Tim-20)325

EXAMPLE III.

Let it be required to know how many Days twenty Men can do the fame Work as fifty Men would do in fix Days ten Hours.

State your Question thus, and say, if 50 Men can do a Piece of Work in 6 Days 10 Hours.

in how many Days will 20 Men do the same Work.

The first and third Numbers being already of one Denomination, you must multiply the middle Number, which is 6 Days 10 Hours, by 24, the Number of Hours in a Day, and take in the Hours, &c. and then it you please multiply by 60, to bring them into Minutes; the middle Number being thus brought into Minutes, you must multiply them by the first Number, and divide by the third, which is contrary to the Rules before mentioned. The Reason is, because 20 Men will require more Time than 50 to do the same Work, whereas if you had multiplied the second and third Number together, and divided by the first, the Aniwer would have been but 2 Days, 13 Hours and 3ths or 36 Minutes, which is the Reverse of the Question, and the exact Time that 50 Men would have done the Work that 20 Men would do in 6 Days 10 Hours. And therefore this Rule is called the Rule of Three Reverse or Inverse; for in the Rule

of Three Direct, the Numbers are in such Proportion, that Answer 16 Days 1 Hour as the first is to the third, so is the second to the fourth or Number sought; but in this Rule the Numbers are always in fuch Proportion, that as the first is to the third, so is the fourth or Number fought to the second, as in the Example above; for if you fay,

As 50 Men the first Number is to 20 Men the third Number, so is 16 Days 1 Hour your Number fought or fourth Number to 6 Days to Hours your fecond Number; that

is, as many times as the first Number is more or less than the third, so many times more or less must the fourth Number be than the second, as the Question happens to be stared. In this Example, the first Number, which is 50, is twice and a half more than 20 the third Number; therefore the fourth Number, which is 16 Days 1 Hour, must be twice and a half more than 6 Days 10 Hours the fecond Number, as is very plain in the Margin. Another thing to be observed in this Rule is, that

| Men As 50 is | Men to 20 50 | Day is 16 | 1 to | Days He. | i n |
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if your first Number is greater than the third, the Number sought, or sourth Number, will be greater than the second Number; and that if the first Number is less than the third, the sourth Number will be less than the second; which being well observed, will make this useful Rule very easy: An Example or two more is set down for the Exercise of the Ingenious, with which I shall conclude the first Part of this Book, and proceed to the second Part, which will contain some few Problems or Questions in Geometry.

EXAMPLE IV.

If thirty Horses, Cows or Oxen, in seven Weeks five Days Time, eat up the Grass of a certain Field or Meadow, &c. in how long Time would forty five Horses, Cows or Oxen, &c. be eating the same Quantity?

EXAMPLE V.

If Two thousand seven hundred Soldiers were besieged in a fortisted Town or Camp, &c. and their Provisions of Victuals, &c. were computed to serve them but two Months, how many of those Soldiers must depart the Garrison immediately, and every Week afterwards, to make the same Victuals last six Months if there should be occasion?

Answer, 972 Men must depart out of the Town or Garrison immediately, and 72 Men every Week afterwards.

EXAMPLE VI.

If there were in a certain Meadow or Field Pasture enough to seed 900 Oxen or Sheep for six Months, how long Time would the same Pasture last, if there came into the Field every Month an equal Number of Sheep or Oxen till the whole Number amounted to 2700?

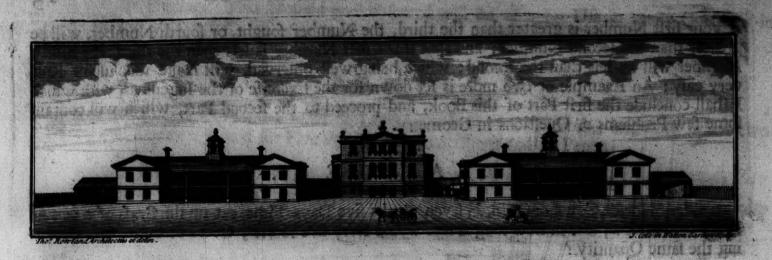
Answer, 900 must come in every Month, and the Pasture will last three Months.

EXAMPLE VII.

If there was to be put into a certain Fort 60 Men, and they were to be increased by 60 Men every Week till the whole Number amounted to 2700, how much Provisions would be necessary to provide the Fort with to maintain the Garrison till it is surnish'd with the aforesaid Number of 2700 Men?

Answer, 45 Weeks Provision for 1380 Men.





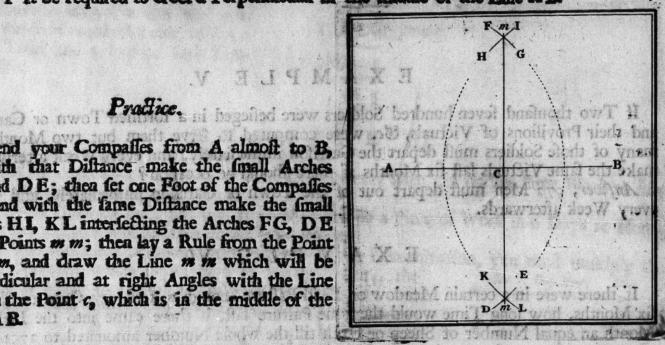
PART METRY.

PROBLEM I.

ET it be required to creek a Perpendicular in the middle of the Line AB.

tas as Hecks and the Lag

Extend your Compasses from A almost to B, and with that Distance make the small Arches FG and DE; then fet one Foot of the Compasses in B, and with the fame Distance make the small Arches HI, KL intersecting the Arches FG, DE in the Points m m; then lay a Rule from the Point m to m, and draw the Line m m which will be perpendicular and at right Angles with the Line A B in the Point c, which is in the middle of the line AB. all old offe sand



II. and the paid of the state II PROBLEM

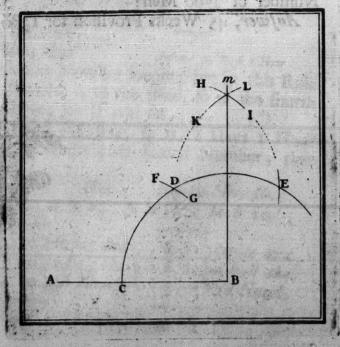
CXAMPLE

mult come in everyaldouth, and therebill no will but thee, storter.

Let it be required to erect a Perpendicular at the End of the Line AB.

Practice.

Set one Foot of your Compasses in B, and extend the other to any Distance at Pleasure, as at C, and make the Arch C D E; then with the same Distance set one Foot of the Compasses in C, and make the Arch FG intersecting the Arch CE in D; then let one Foot of the Compasses in D, and with the same Distance make the Intersection at the Point E; lastly, with the same Distance from the Points D and E make the small Arches HI, KL interfecting one another at the Point m; then lay a Rule from the Point m to B, and draw the Line MB, which will be perpendicular to the Line AB.



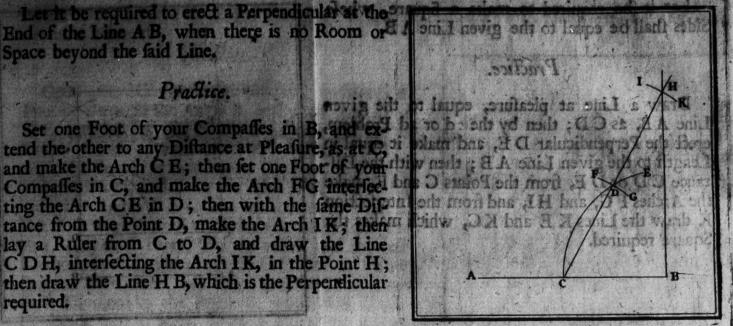
lw out his sport warm noted.

PVROBLEMATE

Let it be required to erect a Perpendicular at the End of the Line AB, when there is no Room or I mil noving out of large ad listh abi Space beyond the faid Line.

Proffice.

Compasses in C, and make the Arch FG intersect by O emotion and more at ting the Arch CE in D; then with the same Dicting and smort bins IH lans tance from the Point D, make the Arch IK; there wind and but a Z lay a Ruler from C to D, and draw the Line CDH, interfecting the Arch IK, in the Point H; then draw the Line H B, which is the Perpendicular required.

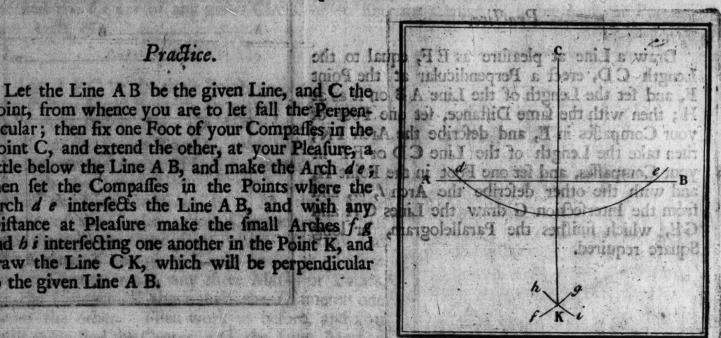


PROBLEM VIL

I et it be required to make an Vhon Mor Jon Sauce, Ande Sides that be equal to the

From a Point at Pleasure to let fall a Perpendicular on the Line AB.

Point, from whence you are to let fall the Perpent on 191 somethic small out this nadi all Point, from whence you are to let lan the terpent of dicular; then fix one Foot of your Compasses in the A characteristic formation of the Point C, and extend the other, at your Pleasure, a characteristic formation of the Points where the Arch de intersects the Line AB, and with any control of the Pleasure at Pleasure make the small Arches for a canolal and the points where the product of the Pleasure make the small Arches for a canolal and the points where the product of the points where the product of the pro Distance at Pleasure make the small Arches fig an angolailant on a string and b i intersecting one another in the Point K, and draw the Line C K, which will be perpendicular to the given Line A B.



ROBLEM VIII Let it be required to make Trisingle equal to the given Triangle ABC.

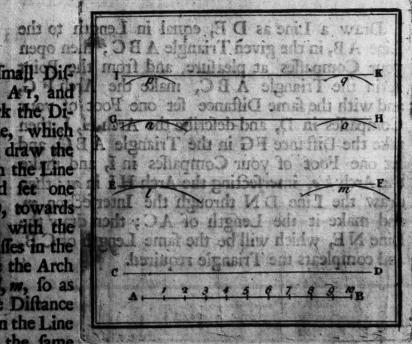
Let it be required to draw Lines parallel to one another at the Distances of 2, 3 and 4 Foot.

Practice.

Draw a Line as AB, and take any small Diff tance in your Compasses, at Pleasure, as Arr, and turn it over the Line 10 times, and mark the Divisions with Figures, as in the Example, which will make you a Scale of 10 Foot; then draw the Line CD, and take the Distance A4 (in the Line or Scale A B) which will be 4 Foot, and fet one Foot of your Compasses in the Line CD, towards the End C, and make the Arch I; then with the same Distance, set one Foot of the Compasses in the ame Line towards the Bnd D, and make the Arch draw the Line EF upon the Arches 1, m, so as just to touch the said Arches; then take the Distance A 2, and fet one Foot of the Compasses in the Line EF, and make the Arch ", likewise do the same ato, then draw the Line GH as before: Lastly,

, and from the Control I are a with the to

Take the Distance A 2, and make the Arches p, q, and draw the Line I K, then will the Lines CD, EF, GH, IK, be parallel one to the other, at the Distances required of 2, 3 and 4 Foot.

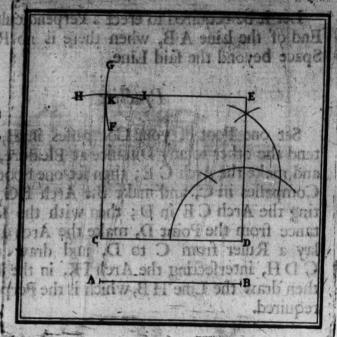


PROBLEMIVE

Let it be required to make a Square, whose Sides shall be equal to the given Line A.B.

Practice.

Draw a Line at pleasure, equal to the given Line AB, as CD; then by the ad or ad Problem, erect the Perpendicular DE, and make it equal in Length to the given Line AB; then with the Distance CD or DE, from the Points C and E, make the Arches FG, and HI, and from the Intersection K draw the Lines KE and KC, which makes the Square required.

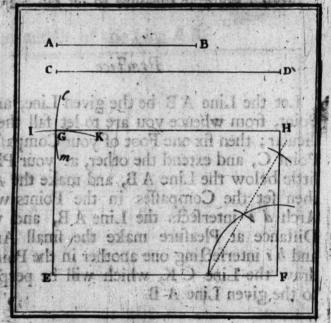


PROBLEM VII.

Let it be required to make an oblong or long Square, whose Sides shall be equal to the two given Lines A B, C.D.

Practice.

Draw a Line at pleasure as EF, equal to the Length CD, erect a Perpendicular at the Point F, and set the Length of the Line AB on it as at H; then with the same Distance, set one Foot of your Compasses in E, and describe the Arch IK; then take the Length of the Line CD or EF in your Compasses, and set one Foot in the Point H, and with the other describe the Arch 1, m, and from the Intersection G draw the Lines GH and GE, which finishes the Parallelogram, or long Square required.



PROBLEM VIII.

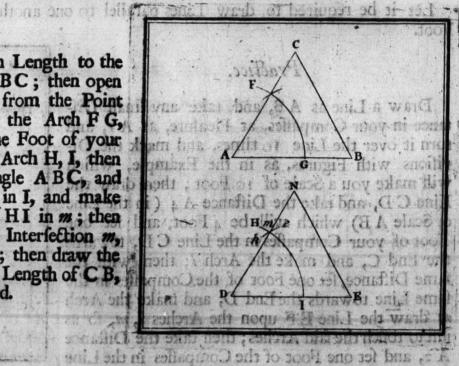
Ran draw the Line GH as before Inth,

Lancy Car, EE, GH, IK, be parallel case to she other, at the skiparces convened as

Let it be required to make a Triangle equal to the given Triangle ABC.

Practice.

Draw a Line as D E, equal in Length to the Line A B, in the given Triangle A B C; then open your Compasses at pleasure, and from the Point A in the Triangle A B C, make the Arch F G, and with the same Distance set one Foot of your Compasses in D, and describe the Arch H, I, then take the Distance F G in the Triangle A B C, and set one Foot of your Compasses in I, and make the Arch ke, intersecting the Arch H I in m; then draw the Line D N through the Intersection m, and make it the Length of A C; then draw the Line N E, which will be the same Length of C B, and compleats the Triangle required.



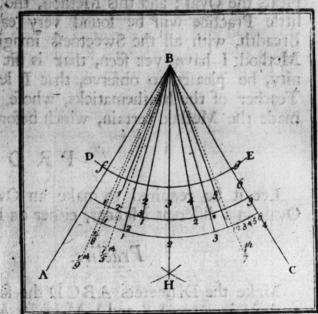
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XI M B L E M TX.

Let it be required to divide the given Angle A B C into two equal Parts, or any other bas, dignol bengilis via to the minimum of his y

Open your Compasses at pleasure, and set one Foot of them in the Angle B, and make the Arch DE, intersecting the Sides of the Angle in the Points f and g, then from the Points f and g, with the fame, or any other Distance, make the Interfection H, and draw the Line H B, which divides the Angle A B C into equal Parts as defired. But if it were defired to divide the faid Angle into 3, 4, 5 or 6 Parts, &c. the easiest and shortest Method, is to divide the Arch DE into as many Parts as is required, and then to draw Lines from those Divisions to the Point B, which will divide the Angle into 3, 4, 5, or more Parts, as was at first proposed.

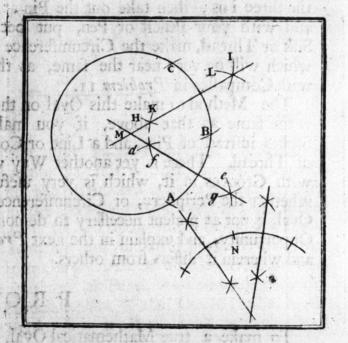


PROBLEM X.

To make a Circle, whose Circumference shall pass through three given Points, and also to find the Center of any given Circle, or to find the Center of a Segment, or Portion of any Arch, &c.

Practice.

Let ABC be the three Points given; then from the Points A and B, with above half the Distance from those Points, draw the Arches d, e, and f, g, and from the Points B and C, with the same Distance draw the Arches HI, KL; then draw Lines through the Intersections of those Arches, and where the Line interlects, as at M, there is the Center of the Circles, whose Circumserence shall pass through the three given Points. And to find the Center of any given Circle, make at pleasure in the Circumference, any three Marks or Points, at the Distance of above half the Diameter one from the other. Then work as before, and you will eafily find the Center, and the same Method must be observed to find the Center of a Segment, or Portion of any Circle, as you may fee by Infpection in the Figure marked N.

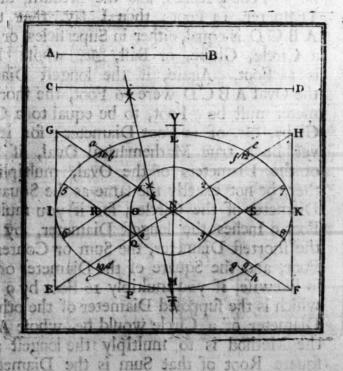


PROBLEM

To make an Oval of any Length or Breadth affigned.

Practice.

Let the Lines AB, CD, be the Length and Breadth affigned for the Oval; then draw a Line at pleasure, as E F, equal in Length to the given Line CD, then make the Perpendiculars EG and FH, equal to the given Line A B, and draw the Line G, H, which forms the Parallelogram EGHF; draw the Diagonals E H and F G, and make the Diameter I K parallel to EF, and the Diameter LM parallel to GE; then with the Distance I E, make the fmall Square IOEP, and with the Diffance O, N, make the Circle 1 2 3 4; then take the Distance OQ, where the Side of the Square OP cuts the Diagonal EH, and fet it from O to R, and make KS equal to I R; then draw Lines from the Points 1 2 3 4, through the Centers R and S, and from the Centers R and S draw the Arches 5, 6, and 7, 8, then with the Distance I E or IO, from the Points or Centers I and K, make the small Arches a b, c d, ef, gb, and from the Centers 1 2 3 4, with the Di-



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stance 4, 5, or 2, 8, make the Arches 8, 9, 10, 6, 5, 11, and 12, 7, intersecting the small Arches ab, cd, ef, and gb, in the Points 9, 10, 11, 12; and lastly, from the Points 11 L or L 12, with any Distance at pleasure, make the Intersections i and k, then draw a Line through those Intersections, till it cuts the Line L M at T, then make N V, equal to N T, and from the Centers T and V draw the Arches 11 L 12, and 9 M 10, which compleats the Oval; and this Method, tho' in Appearance something troublesome, yet with a little Practice will be sound very easy, and to form an Oval of any assigned Length and Breadth, with all the Sweetness imaginable, and in my Opinion, much beyond any other Method I have yet seen, that is sit for drawing, &c. but lest this should savour of Vanity, be pleased to observe, that I learned this Method from my Master Mr. Marshall, Teacher of the Mathematicks, whose Invention it was; I have only added to it, what has made the Method certain, which before was doubtful.

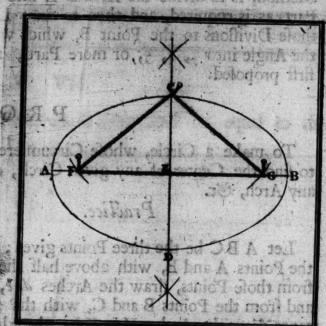
PROBLE M. XII. De Dia O B A COME DE STORE

Let it be required to make an Oval of the same Length and Breadth as the preceding Oval, in a different Manner, either on Paper or on the Ground, &c.

Practice.

Make the Diameters ABCD the same Length as the Diameters I K and L M in Problem 11. and at right Angles one with the other; then with the Distance AE or EB, from the Points C and D, make the Intersections FG, in the Line AB; then stick Pins in the Points FDG or FCG, and take a Piece of Silk or Thread, and tye it tight round the three ins; then take out the Pin at C or D, and with your Pencil or Pen, put between the Silk or Thread, make the Circumference ACBD, which will be very near the same, as that struck with Compasses in Problem 11.

The Method to make this Oval on the Ground, is the same as that above, if you make Use of Stakes instead of Pins, and a Line or Cord instead



of Thread. There is yet another Way very well known, by an Instrument, called the Cross, with Grooves in it, which is very useful in small Ovals, and is an excellent Method; but whether the Periphery, or Circumference, is exactly true, so as to form a Mathematical Oval, is not at present necessary to demonstrate; and therefore I shall leave that to another Opportunity, and explain in the next Problem, what is meant by a true Mathematical Oval, and wherein it differs from others.

from the other. Then work as before and Bolo B O R Q will eafily find the Center, and HIX or M B LOB O R Q

To make a true Mathematical Oval, that is, such an ovalar Superficies or Solid, whose Area, or solid Contents, is equal to the Area, or solid Content of a Globe, or Ball, &c.

Practice.

Let the longest Diameter of the Oval ABCD be 18 Foot 9 Inches, and the Breadth, or shortest Diameter, 12 Foot; then I say, that the Oval ABCD is equal, either in Superficies, or Solid, to a Circle, Globe, or Ball, &c. whose Diameter is 15 Foot. Again, if the longest Diameter of the Oval ABCD were 16 Foot, the shortest Diameter must be 9 Foot, to be equal to a Circle, or Globe, &c. of 12 Foot Diameter; for it can never be a true Mathematical Oval, if the Sum of the Diameters of the Oval, multiplied together, be not exactly the same as the Square of the Diameter of the Circle; for if you multiply 18 Foot 9 Inches the longest Diameter, by 12 Foot the shortest Diameter, the Sum or Content is 225



light b, and from the Centers 123 d, with the Di-

Foot, and the Square of the Diameter of the Circle, which is 15 Foot, is exactly 225 Feet; fo likewise, if you multiply 16 Foot by 9 Foot, the Sum will be exactly the Square of 12, which is the supposed Diameter of the other Circle. Now if you desire to know, what the Diameter of a Circle would be, whose Area, or Circumserence, should be equal to an Oval, the Method is to multiply the longest and shortest Diameter of the given Oval, and the square Root of that Sum is the Diameter of the Circle required; and on the contrary, to determine the Lengths and Breadths of Ovals, whose Area, Circumserence, or Solidity.

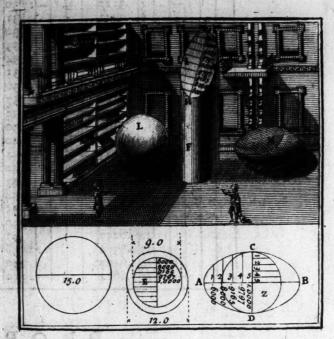
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shall be equal to the Area, Circmference, or Solidity of any given Circle, Ball, or Globe, &c. the Method is to square the Diameter of the given Circle, and divide the Product by any Number that you would have, either for the Length or Breadth of your Oval; and then if the Number you divide by be the Breadth; the Quotient is the Length; and so if the Number you divide by be the Length, the Quotient is the Breadth: As for Example; In the first Proposition, the Diameter of the Circle was supposed to be 15 Foot, the Square of which is 1225, this being divided by 12 (the shortest Diameter) you will have 18 Foot 9 Inches for the longest Diameter. So likewise in the other Example, where the Diameter of the Circle is supposed to be 12 Foot, the Square of which is 144; this being divided by 16, the longest Diameter, you will find 9 for the shortest Diameter, and this is not to be confined to those Diameters above-mentioned, but you may use any other Numbers for your Diameters, as you have Occasion.

After the Diameters of the Oval are thus found, all the difficulty is, in making the Perifery, or Circumference, of the Oval exact. The Method already taught in Problem 11, and 12, comes the nearest the Truth of any I know, or have seen; but what is to be relied on,

for Certainty, is as follows.

Make a Cylinder, whose Diameter is equal to the Circle E, of 9 Foot Diameter, then cut the faid Cylinder diagonally, fo that the Diameter GH is 16 Foot; then the Diameter IK will of necessity be 9 Foot; therefore is the Oval GIHK exactly true and equal to a Circle, Globe, or Ball, Gc. whose Diameter is 12 Foot, according to what has been faid above, and if the Cylinder Phad been 15 Foot Diameter, and the Diameter GH 18 Poot 9 Inches, the Oval GIHK would have been the fame exactly as the Oval ACDB, and equal either in Superficies, or Solidity, to a Circle, Globe, or Ball, &c. of 15 Foot Diameter, as is represented by the Solids L and M; this however is rather a Demonstration than a Method, to be put in Practice (except as a Proof of this Proposition) therefore, whenever there is Occasion to be so very curious and exact, make use of the Numbers, calculated and fent me by my ingenious Friend Mr. Marshall; in order thereto divide half the long-



est or shortest Diameters of the Oval ACBD into five equal Parts, then erect Perpendiculars upon those Divisions in the Diameters, &c. and make the Half or Semi-diameters 1.0000 in the Line of equal Parts on the Sector, then take off the Numbers from the Sector, as it is fet down in the Oval A C B D, and place them upon the Perpendiculars, &c. and trace the Periphery from those Points, with a thin Rule or Lath, &c. the same must be done for the other Parts of the Oval to finish it. But for those, who do not understand the Use of the Sector, there is two Methods very easy; the first is to make a Circle of the shortest Diameter of the Oval, and divide the Diameter into the fame Number of Parts, as you incline to divide the longest Diameter of the Oval, and set the Perpendiculars of the Circle (either with Compasses, if it is a small Oval, or with a Lath or Rule, if it is a large one) upon the Perpendiculars of the Oval, as is feen by inspection, in the Circle N, and in the Oval A B C D, for the Lines 1, 2, 3, 4, 5 in the Circle, are exactly the same Length of the Lines 1, 2, 2, 4, 5 in the Oval. The other Way, is to change the Numbers into Foot-Measure, by multiplying them by the longest or shortest Semi-diameters of the Oval, and then setting on the Lengths with your Rule, as in the Example underneath. I am afraid I have trespaied too much in this long Description, or Method, to make a true mathematical Oval; but I could not explain my felf fo as to be understood in fewer Words. And if any should think the Division, above-mentioned, not minute or nice enough, be pleased to use the Numbers in the following Table, which are for dividing the Semi-diameters of Ovals or Circles (for they will, serve for either) into 5, 10, 20, 25, 50 or 100 Parts, which will be more than sufficient to form any Oval of a moderate Size, with Truth and Exactness, for any Business whatsoever.

EXAMPLE.

Suppose the Oval A B C D of 18 Foot 9 Inches long, and 12 Foot broad; then the shortest Semi-diameter of the Oval will be 6 Foot; and if the longest Radius or Semi-diame ter be divided into 5, 10, 20, 25, 50 or 100 equal Parts; and if the Numbers in the Table opposite to those Divisions are multiplied by 6 Foot, which is half the shortest Diameter, it will bring those Numbers into Feet and decimal Parts, which decimal Parts being multiplied by 12, produce Inches and decimal Parts of Inches; these decimal Parts being again multiplied by 12, will produce Parts of Inches, which will be near enough, as may be seen by Inspection in the Work underneath, where the longest Semi-diameter is divided into 5 Parts, which is sufficient to shew the Method of bringing any of the Numbers of the Table into Feet and Inches, &c.

| The Numbers in the Table opt | cofite to 1, 2, 3, 4, 5 in the first Colu | mns (where at the | Top is | writ the Sen | ni-diamer i | n hve Parts) |
|--|---|-------------------|--------|--------------|-------------|--------------|
| | १४त्य १८ स्टब्स्ट ४ व्यवस्य १५ अस्तात | are 16000 | 8000 | 9165 | 9797 | 1,0000 |
| These Numbers being multiply'd a | s directed above, produce Feet and Inc | hes, &c. 3 6000 | 4 8000 | 5 4990 | 5 8782 | 6,000 |
| .6000 .8000 | 3 Foot 7 Inches 7 ths | 72000 | 96000 | 5 9880 | 10 5384 | |
| And for the Numbers 9165 There will be | Foot o Inches Tths Foot o Inches Tths Foot o Inches | 12 | 12 | 12 | 12 | |
| (1.0000) | 6 Foot | 2 4000 | 7 2000 | 11 8560 | 6 4608 | |

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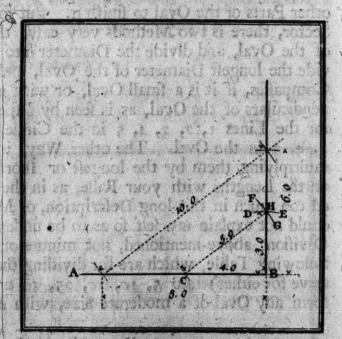
| Semi-diam. in c P | Semi-diam. in | Semi-diam. in 20 | 52000 | Semi diam. in | I he semi-diam, in 100 farts | | Semi-diam. in c P | The Semi-diam, in 20 Parts | The Semi-diam. in | The Semi-diam, in 100 Parts | .6726 | The Semi-diam, in 9 Parts | mi-diam. | The Semi-diam, in 25, Parts The Semi-diam, in 50 Parts | | The Semi diam, in c Parts | Semi-diam. in | The Semi-diam. in 25 Parts | The Semi-diam, in | The Semi-diam, in | you have to be to |
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| | | 1 | 1 | 2 | 1 2 3 4 5 6 | .1410 .1989 .2431 .2800 .3122 | | 3 | 7 | 27 14 28 29 15 30 31 | .6939 | | I1 | 27 5 27 5 14 28 5 | 2 .87 3 .88 4 .88 | 26 90 | 8 | 626 | 39 40 | 76 77 78 79 80 | .970 .973 .975 .977 .979 |
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| | | 3 | 4 | | 56789 | .5267 .5425 .5577 .5723 .5864 | 2 | 4 3 | 11 | 20 40 41 21 42 43 22 44 | .8074 .8146 .8216 | | 3 | 35 6 17 34 6 | 6 .944 7 .94 8 .94 | 4 | 9 | 29 | 46 | 90 91 92 93 94 | .994 .995 .996 .997 .998 |
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PROBLEM XIV.

To raise a Perpendicular at the End of a Line with a 5 Foot Rod, or a 16 Foot Rod, as Occasion shall require.

Practice.

Let AB be the Line required to raise a Perpendicular upon, with a 5 Foot Rod, and from the Point B towards A, make a Mark in the Line A B at the Distance of 4 Foot, as at C; then at the Point C and B, drive Stakes, if it is on the Ground, and Pins or Nails, if it is upon a Board or Floor, &c. then make the Arch DE, at the Distance of 3 Foot from the Point B, by putting one End of the Rod against the Stake at B, and with a Pencil or Nail, &c. held against the Side of the Rod at the Distance of 3 Foot, moving the Rod a little from you towards D, and bring it again towards you at E; then put one End of the Rod against the Stake or Nail at C, and with the other End, which is 5 Foot, make the Arch F'G, interfecting the Arch DE in the Point H; then draw the Line HB, which will be perpendicular to the Line AB. The same Method must be observed with the 10 Foot Rod, only instead of 3, 4 and 3 Foot, you must use 6, 8 and 10 Foot, as may be feen in the Figure by Inspection.



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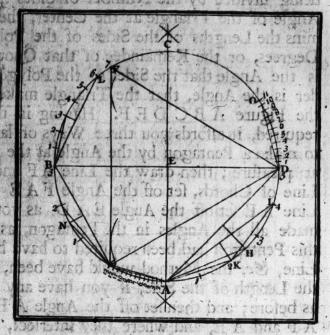
PROBLEM

To make a regular Polygon of any Number of Sides equal or unequal.

Practice.

Make the Circle ABCD, and draw the Diameters AC and BD, at right Angles one with the other, divide the Semi-diameter E B into two equal Parts, and draw the Line F G parallel to AC; then will FG be the Side of the equilateral Triangle FGD; draw the Line AD, and it will be the Side of a Square. Divide the Arch AHD into five equal Parts; four of them, as AI, will be the Side of a Pentagon or Polygon of 5 Sides. The Arch GBF being divided into two equal Parts in B, one of them, as GB, is equal to the Semi-diameters A E or E D, and is consequently the Side of a Hexagon or Polygon of 6 Sides; divide the Arch B L F into feven equal Parts, fix of them, as B L, is the Side of a Heptagon or Polygon of 7 Sides; divide the Arch A H D into two equal Parts in H, the Line A H is the Side of an Octagon or Polygon of 8 Sides; the Arch GB being divided into three equal Parts, two of them is the Side of a Nonagon or Polygon of 9 Sides, the Arch AK I being divided into two equal Parts in K, the Line AK is a Decagon or Polygon of 10 Sides; the Arch GNB being

divided into two equal Parts in N, the Line G N is a Dodecagon or Polygon of 12 Sides, and fo for all the even-fided Polygons, which will always double the Number of Sides. You having no more to do for the Polygons of 14, 16, 12, 20 Sides, Se. than to divide the Arches belonging to the Sides of the Polygons of 7, 8, 9, 10 Sides, &c. into two equal Parts as was done for the Side of the Hexagon GB, and the Sides of the Octagon A H, the Decagon I K, and for the Dodecagon GN. And so likewise for those Polygons of 13, 15, 17, 19 Sides, &c. the Method is to take the Arch of the Side of the Polygon, whose Number is less by one than what you want, and divide the faid Arch into so many equal Parts as is the Number of Sides you want the Polygon to be of, and then all those Parts but one is the exact Side required; for Example, if you take the Side of the

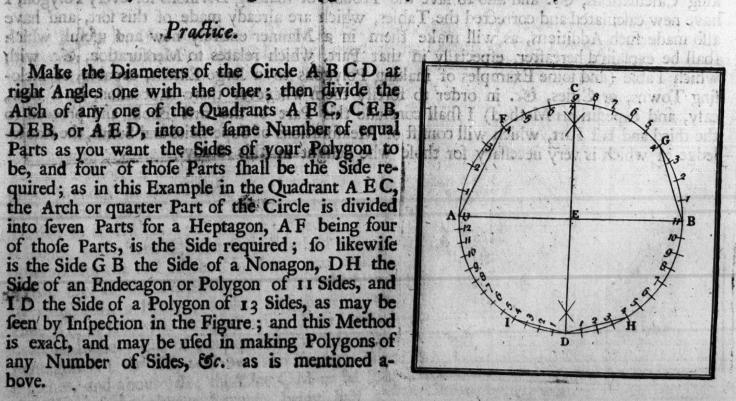


Decagon AK, and fet it from D to O (to avoid Confusion) and divide the Arch DO into 11 parts, 10 of these parts shall be the Side of a Polygon of 11 Sides; and also if you take the Side of the Dodecagon AG or GN, and divide the Arch AG or GN into 13 parts, 12 of those Parts shall be the Side of the Polygon of 13 Sides; and so on for any other Number whatsoever. The same thing, tho' in a different Manner, is in Serlio's Book of Architecture, which shall be the next Problem, for the Reader to take which Method he likes best. But this I did not see or remember, till some time after I had formed the abovesaid Problem, to which I was excited by reading Mr. Whifton's Euclid, where in Book IV. p. 97, he fays, That there hath not yet been found out the Art, by which regular Figures of 7, 9, 11, 12, 17 Sides, &c. may be inscribed in a Circle by a Pair of Compasses and a Rule only: Whether this Method, or that of Serlip's, comes up to what he means by a Rule to divide the Circumference, must be left to better Judges than, my self; for I am afraid, a mathematical Rule or Method to divide the Circumference into 7, 9, 11, 13 and 17 Parts, &c. as is defired, is for ever impossible. All that I pretend to in this, is that the Method above, and that of Serlio's, is true, and capable of mathematical Demonstration, and answers to all Intents and Purposes the exact Method of making all Sorts of regular Polygons, whether the Sides are in Number equal or unequal, which comes up, in some measure, to what Mr. Whiston fays is fo much wanted. whether they are of great the and Service, as is talk allows, in Can

of of state with the PROBLEM MANY I have all to select the property of the pro

Another Way to make a regular Polygon of any Number of Sides, &c.

right Angles one with the other; then divide the Arch of any one of the Quadrants A EC, CEB, DEB, or AED, into the same Number of equal Parts as you want the Sides of your Polygon to be, and four of those Parts shall be the Side required; as in this Example in the Quadrant A E C, the Arch or quarter Part of the Circle is divided into seven Parts for a Heptagon, AF being four of those Parts, is the Side required; so likewise is the Side G B the Side of a Nonagon, DH the Side of an Endecagon or Polygon of 11 Sides, and I D the Side of a Polygon of 13 Sides, as may be feen by Inspection in the Figure; and this Method is exact, and may be used in making Polygons of any Number of Sides, &c. as is mentioned above.



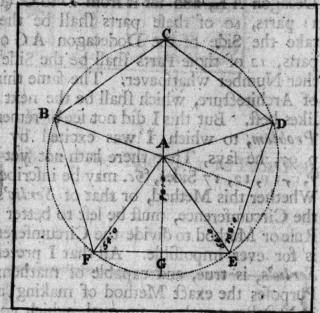
Line A.D., and it will be the Side of a Square. Divide the Arch A.H.D. into hee equal Paris, four of them, as A.I. will be thy We o'M But O'FRY B. o' e Sides. The Arch G.B.E.

Some other Ways of making regular Polygons, very necessary and useful in Gardening and Fortification, &c.

gon of a Sides; divide the Arch A 11 D into two court Parts in 11, the Line A H is the Side of an Octagon or Polytran of 8 Sides; the Arch contrary divided into three cottall at re, two of

Let the Circle (in which you are to describe the Polygon) consist of 360 Degrees, which being divided by the Number of Sides your Polygon is to be of, the Quotient will be the Angle of the Triangle at the Center, the Sides of which (where it cuts the Circle) determins the Lengths of the Sides of the Polygon. The Complement of that Quotient to 180 Degrees, or the Remainder of that Quotient out of 180 Degrees (which is the same thing) is the Angle that the Sides of the Polygon, makes with each other, and half that Remainder is the Angle, that the Triangle makes at the Angle of the Polygon, as may be feen in the Figure ABCDEF. Having in this manner the Number of Degrees at each Angle required, it affords you three Ways of laying down, or protracting the Polygons; and first, to make a Pentagon by the Angle at the Center, draw the Circle BCDEF of any Distance at pleasure; then draw the Line AF and by an Instrument called a Protractor, or by the Line of Chords, fet off the Angle FAE 72 Degrees, and draw the Line AE; then from the Line A E set off the Angle E A D, as you did before, and so continue to do, till you have made all the Angles in the Pentagon, as may be feen by Inspection in the Figure; and if this Pentagon had been required to have been made by the Angles at the Triangle or Base-Line, &c. the Method would have been, to draw a Line at pleasure, as FE, upon which set the Length of the Side, if you have any determin'd Length, otherwise ler it be at pleasure, as before; and then fet off the Angle A E F and A F E 54 Degrees each, and draw the Lines A F and A E, and where they interfect, as at A, there is the Center; then draw the Circle

BCDEF, and with the Distance FE divide the Circle into five Parts, and draw the Lines ED, DC, CB and BF, which finishes the Pentagon exactly. The third Way is by the Angles of the Sides; as for Example, draw the Line EF as before, at pleasure, upon which set the Length of your Side, and make the Angle FED, 103 Degrees; then divide the Line EF into two equal Parts in G, and draw the Line AG perpendicular to FE, and fet the Distance EG upon the Line ED, and erect the Perpendicular AH, and where the Perpendiculars interfect, as at A, there is the Center; then with the Distance A F or A E make the Circle BCDEF, and with the Distance FE divide the Circle into five equal Parts; then draw the Sides E D and D E, &c. as before. These Methods are exactly the fame for all forts of Polygons, and therefore ought to be carefully obser-



quired; as in this Example in the Omdiant A

the Aich or quarer Part of the Carde is divided into feven Parts for a Heptagon, A R being four of those Parts, is the Sida required; to likewife

is exact, and may be used in-making Polygons of any Number of Sides, Etc. as is mentioned about.

bout.

ved, for they are of great Use and Service, as is said above, in Gardening and Fortification, &c. and I have been the more careful (tho' perhaps a little tedious) in what relates to Polygons, on account of the many Mistakes and Errors propagated in the Methods to make them, by Authors of good Authority. But for the Use of those, who are not expert in making Calculations, &c. and also to save the Trouble of making Divisions for every Polygon, I have new calculated and corrected the Tables, which are already made of this fort, and have also made such Additions, as will make them in a Manner entirely new and useful, which shall be explain'd hereafter, especially in that Part, which relates to Mensuration, &c. with which Table (and some Examples of making Polygons to a large Extent, capable of inclosing Towns, or Cities, &c. in order to fortify them whenever there is occasion, in a new, easy, and expeditious Method) I shall conclude this Part of the first Book, and proceed to the third and last Part, which will consist of Mensurations of Superficies and Solids, the Knowledge of which is very necessary for those who delight in this Study.

is the Side G B the Side of a Nonagon, D H the Side of an Endecagon or Polygon of an Sides, and the Side of a Polygon of a Sides, as may be feen by Inspection in the Figure; and this Method

Breadth of the Side CE, will be 76 g. Kirds, in Front, a Inches, and about it. Thus with very little Trouble may the Pentagon, or the other Polycons, above-medicaled, by made without any other laterant the La La Badh Thoogh , which Method will be found

| The Names of Several Goo merical Figures, all of which, except the Triangl and Square, are called Po hygons. | The Num of the Sides | Angles at the Center. | Angles at the Side of the Triangle and Square, and at the Side of the Polygons D M | Angles at the | The Radii or Semi diameters of Circles is feribing the Polygon with the Sides and Perpendiculars of th Polygons, &c. | The Side, iquar- ed and multiplied by these Num- bers, gives the suggestions. | The Diameters of the Circle, fquared & mul- tiplied by thek Num. gives the | The Area of the Polygon multip by these Numb and the fg. Root extracted, given | The Area of the Pelygor when the Dia meter of the Circle is |
|--|-------------------------------|-----------------------|--|---------------|---|---|--|--|---|
| Trilagon or | 3 | 120,00 | 60.co | 30.00 | Semi-diameter p. 000 Side 1-732 Perpendicular 500 | | •32457 | rive or lit | 129907 |
| Teffaragon or | 4 | 90.00 | 90.00 | 45190 | Semi-diameter 1 000 Side 1-414 Perpendicular 4 707 | 1.00000 | 50000 | 2.00coc | 2.00000 |
| Pentagon | 5 | 72.00 | 108.00 | 54.00 | Semi-diameter 1.000 Side 1.175 Perpendicular 800 | 1.72039 | 59441 | 1.68234 | 2.37765 |
| Hexagon | 6 | 60.00 | 120.00 | 65.66 | Semi-diameter 1,000 Side 1,000 Perpendicular - 866 | 2.59800 | W.64950 | 1.53964 | 2.59800 |
| Heptagon | 7 | 51.25 | 128.3423 | 64.47 13 | Semi-diameter 1.000 Side | 3.63432 | .68407 | 1.46183 | 2.73629 |
| Odogon of vi | 8 | 45.00 | 135.00 | 67.30 | Semi-diameter 1.000 Side 1705 Perpendicular923 | | 270715 | 1.41412 | 2.82861 |
| Ennagon | 9 | 40.00 | 140.00 | 70:00 | Semi-diameter 1.000 Side .6844 Perpendicular .939 | 6.18222 | -72309 | 1.38295 | 2.89239 |
| Decagon | 10 | 36.00 | 144.00 | 72.00 | Semi-diameter 1.0000 Side .618 Perpendicular9510 | 7.69292 | -73474 | 1.36097 | 2.93906 |
| Endecagon | 11 | 32.43 | 147.16 | 73.38 | Semi-diameter 1.000 Side .5634 Perpendicular .959 | 9.36679 | -74350 | 1.34535 | 2.97320 |
| Dodecagon | 12 | 30.00 | 150.00 | 75.00 | Semi-diameter 1.000 Side .517 Perpendicular .965 | 11.19451 | -75006 | 1.33332 | 3.00027 |
| Tridecagon | 13 | 27.41 .5 | 152.18,2 | 76.09 \$ | Semi-diameter 1.0000 Side 4780 Perpendicular 9700 | 13.18606 | .75509 | 1.32434 | 3.02037 |
| Teffaredecagon | 14 | 25.42 6 | 154.17 3 | 77.08.3 | Semi-diameter 1.000 Side 445 Perpendicular 974 | 15-33555 | .75920 | 1.31713 | 3.03681 |
| Pentedecagon | 15 | 24.00 | 156.00 | 78.00 | Semi-diameter 1.000 Side | 17.64249 | 76255 | 1.31138 | 3.05020 |
| Hexadecagon | 16 | 22,30 | 157.30 | 78.45 | Semi-diameter 1.0000 Side .3902 Perpendicular .9808 | 20.10866 | .76541 | 1.30647 | 3.06166 |
| Heptadecagon | 17 | 21.10,2 | 158.49 5 | 79.24 2 | Semi-diameter 1.0000 | 22.73604 | .76766 | 1.30266 | 3.07064 |
| Octodecagon | 18 | 20.00 | 160.00 | 80.00 | Semi-diameter 1.0000 Side | 25.53212 | .76985 | 1.29898 | 3.07943 |

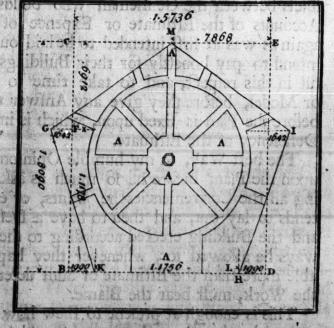
PROBLEM XVIII.

To make a Pentagon, Hexagon, Heptagon, and Octogon, capable of inclosing a Town or City, with Ease and Expedition, with a Line and ten Foot Rod only, of great Use in Fortification and Gardening, &c. work on a mindo or visites on which are as it in who and the

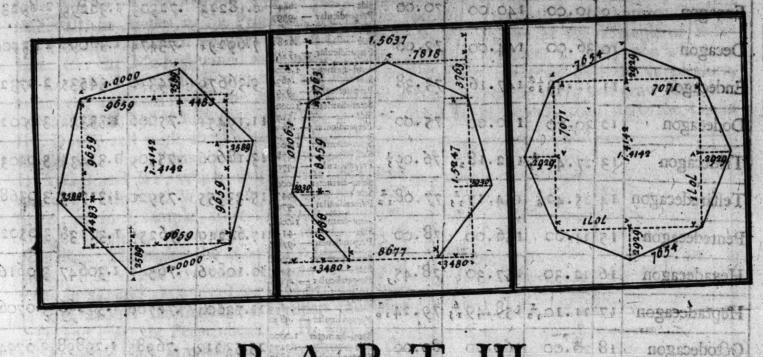
Practice. as diele anob ad or all a sail a baller

Let A A A A, &c. represent a Town or City, &c. then by Problem 14th, erect the Perpendicular BC upon the Line BD; then measure the Length of the Town or City (which

Suppose to be 1760 Yards, and by the Rule of Proportion fay, As 1.3090 the Length of the oblong Square BCDE, is to 1760 Yards, the supposed Length of the Town or City, &c. fo is 1.5736 the Breadth of the oblong Square BCDE, to 1530 Yards, 2 Foot, 4 Inches, and about 1, the suppos'd Breadth of the Town, &c. Then for the Perpendicular BF, fay as CB 1.8090 is to 1760 Yards; fo is BF 1.1178 to 1087 Yards, 1 Foot, 6 Inches, and about 12, the same Method is to be observed for the rest of the Numbers you want in Yards, &c. as the Perpendicular GF, which will be 150 Yards, 2 Foot, 2 Inches and about 1, the Line BK or LD will be 192 Yards, 1 Foot, and almost 10 Inches; and of consequence the Side of the Pentagon K L or HI, will be 1142 Yards, 1 Foot 8 Inches, and about 1th; the Line CM or ME at the Top of the oblong Square, being half the



Breadth of the Side CE, will be 765 Yards, 1 Foot, 2 Inches, and about 1.6. Thus with very little Trouble may the Pentagon, or the other Polygons above-mentioned, be made without any other Infrument than a Line and a 10 Foot Rod, which Method will be found of great Advantage to many, who do not know the Use of the proper Instruments, as well as those who do; for it may possibly happen, a regular Polygon may be required to be made, when there is no Instrument to be had, or procured at the time you want them. The Numbers fixed to the Pentagon, as well as those to the Hexagon, Heptagon, and Octogon, in the Figures underneath, are perpetual, and will ferve upon all Occasions, let the Polygons be ever so large or small; for the Proportions will always be as above; that is, as the Side of the Oblong in the Pentagon and Heptagon, or the Side of the Square in the Hexagon and Octogon, is to the real Sides of the Town or City, &c. in Perches, Yards, Feet or Inches, &c. to is any other of the Numbers in the Figures to the real Quantity of Perches, Yards, Feet or Inches required to make the Polygons, Gr. And this, I think, is sufficient for the Purposes above-mentioned, to form the grand Lines, which is the principal thing : The making of the Bastions, and other. Works of Fortification, on the Sides where they are too long to be defended by Musket-shot from the Bastions at the Angles, &c. is the Work of an Engineer, or Persons more skilled in Fortification than I am, and indeed I should not have mentioned this at all in this Treatife, were it not for the Affinity there is between the Civil and Military Architecture; for one may, I prefume, without Offence affirm, that it is hardly possible for an Architect to be skilful in one, without having fome Knowledge of the other.



PARTIII. MENSURATION.

If it will not be thought improper, I should be glad in this Place to acquaint the ingenious Reader, that the Mensuration of all Sorts of Superficies and Solids is not attempted; but only such as are absolutely necessary to obtain a competent knowledge of measuring the several Artificers Work in a Building, or to make the Estimate before the Building is erected, which ought to be done with as much Care as when the Building is finished; the Method of doing which, when I come to the the 5th Part or Section (this being only the Ground-work or Foundation) I shall endeavour to explain in as short and easy a Way as I can, because of the great Consequence that attends it; for there is nothing makes so much Uneassiness between the Gentleman who builds, and the Architect or Artificers, as the wrong Accounts of the Estimate or Expence of a Building, which sometimes comes to as much again as was at first intended to be laid out: This being a great Discouragement to those, who intend to pay honestly for their Buildings, it is the Duty of all Architects to be very careful in this respect, and to take time to make and prepare their Estimates by the Drawing or Model, before they give any Answer to those, who would oftentimes know the Expence before the Plan is fixed upon, which is impossible, and is therefore often the Cause of the Desiciency of the Estimate.

The best Way, in my humble Opinion, is for the Gentleman, who builds, to fix intirely upon the Plan, before he so much as asks for the Estimate, and then he will be sure of having all the Conveniencies he wants, or else to determine at once the Sum of Money he intends to lay out, and then to have a Design made accordingly: If these Measures are taken, and the Building erected according to the Designs, without any Alterations (which must always be allowed for, whenever they happen) and the Expense should be any thing considerable more than the Estimate or Sum determined, the Architect or Artisteers, who undertake the Work, must bear the Blame.

This is enough at present to shew how much depends upon being exact in our Calculations, and with what Care Gentlemen should proceed, who intend to Build, left they lose the Benefit

Reward for the Good they do, in employing to many Tradelmen, who are concern'd in Building, and also for the Addition of Beauty it makes to the City, Town or Country, where they happen to build; and that I may in some Measure contribute to the Advancement of the Art of Building, and to the Encouragement of such good Designs above mentioned, I have spared no Pains to make the most difficult Parts easy, delightful and profitable, both to the Builden and the Artificer, in order to which, it is my humble Request to the ingenious Practitioner to be as perfect as possible in the following Examples, which will make him proceed in the rest of the Work with Delight.

a may be feen by Inspection, which will explain this Method better than many Words.

Or to extract the Root of any square Number proposed, is to find out another Number, which, when it is multiplied by itself; produces the Number proposed, and, for the more easy Method of doing this, the following Table must be learned by heart, which is only to re-

That I is the Root of 1, 2 is the Root of 4, 3 the Root of 9, 4 the Root of 16, 5 the Root of 25, 6 the Root of 36, 7 the Root of 49, 8 the Root of 64, and 9 the Root of 81; and also, that I is the Square of the Root 1, 4 the Square of the Root 2, 9 the Square of the Root 3, 16 the Square of the Root 4, 25 the Square of the Root 5, 36 the Square of the Root 6, 49 the Square of the Root 7, 64 the Square of the Root 8, and 81 the Square of the Root 9, as may be seen in the Table underneath.

| 1 | 2 × 15 × 15 | 《新闻》 《美国》 | | | | | |
|---|-------------|------------------|------|-------|------|---------|----|
| 1 | Root | 1 2 | 3 4 | 5 6 | 1 7 | 8! 9 | Ea |
| | Square | 1 4 | 9 16 | 25 30 | 1491 | 64 81 | |

PROPOSITION I.

Let it be required to extract the Root of the whole Number 987654.

Set down the Number as in the Margin, and make a Point or Dot over the Place of Units, another over the Place of Hundreds, and so on towards the Left-hand, as in the Example, always leaving one Figure between the Dots; then make a circular Line, as you do in Divilion, and find the Root of the first Number 98, the nearest to which is 9, set down the 9 in the Quotient, and its Square 8r underneath the 98; and then substract as you do in Division, and bring down the next Number 76 to it, which makes a Dividend of 1776. and for the Divilor you must double the Root 9, by faying, twice 9 is 18, which let down towards the left Hand, as you fee in the Margin; and then, as you do in Division, say, how many times I can I have in 17, or how many times 18 in 177, which will be found 9 times; then fet the 9 in your Quotient, and also in your Divisor, which must always be observed; then multiply the Divilor by 9 and place the Product underneath the Dividend 1776 and substract as before, there remaining 75, to which bring down the next Number 54, which makes a new Dividend of 7554; then double the Figures in the Quotient, which is now 90, and fay twice 9 is 18, 8 and go 1, and twice 9 is 18 and 1 is 19, which makes 198 for the new Divifor, which fer down as in the Example, and divide as you did before, by asking how many times to there can be had in 75, this being found to be 3 times; let down the 3 in the Quotient, and also in the Divisor, and then multiply the Divisor by 3, and place the Product 5949 underneath the Dividend 7554, and substract as before, there remaining a 605, by which you may perceive, that 993 is not the exact Root of the whole Number 287654, for if it had been exact, there would have been no Remainder, whereas there is now re-

987654(998.807 81 4 Quarters

189)1776 3.228

1701 807

1983) 7554 3 Feet

5949 2.421

19868)160500 12 Inches

158944 5.052

198760) 1556000

000000 807

12 Inches

13913249 9.684

12 Parts of an

Inch

993 Yards 3 Quarters

993 Yards 2 Foot 5 Inches

993 Feet 9 Inches and 8-1 2ths

Proof of the Work.

993.807

993.807

6956649

79504560

2981421

8944263

987652353249

1646751 Remainder

maining 1605; therefore in this Case, and all others, whenever there is a Remainder, if there is a Necessity of having the Root more exact, the Method is to put two Cyphers to the right Hand of the Remainder, which makes a new Dividend; and then to work as before (as may be seen by Inspection in the Margin) till you have got two or three Places in the Decimals, which is exact enough for most Business, always remembring, that whatever Figure you have for the Quotient, the same must be put in the Divisor, that it may be multiplied with it, as has been already mentioned above. There remains one thing more, and that is, if it is required to have the Root of the same Denomination into which the whole Number to be extracted is divisible, it is requisite to bring the Decimals into such Parts as are required; for Example, if the whole Number is Yards, the Root ought to be Yards and Quarters

Quarters of Yards, or Yards, Feet and Inches, whenever there is a Remainder; lo likewife if the whole Number is Feet, the Root must be Feet, and if any Remainder, the Parts must be Inches and Parts of Inches, &c. therefore if the whole Number is Tards, multiply the De-cimals by 4, to know the Quarters of Yards, and cut off one Figure to the left Hand, as in the Example, which will be Quarters; so likewise, if the Root should be Yards, Feet and Inches, multiply the Decimals by 3, to reduce them into Feet, and cut off a Figure to the lest Hand, as before, and multiply that Product by 1:, to bring them into Inches, as may be feen in the Margin; and also, if the whole Number is Feet, the Decimals must be multiplied by 12, to bring them into Inches, and that Product again by 12, to bring them into Parts of Inches, as may be seen by Inspection, which will explain this Method better than many Words.

redenald serbons sup both of To Extract the Cube Root,

Or to extract the Cube Root of any whole Number, is to find out another Number, which being multiplied by its felf, and that Product by the same Number again, shall produce the Number proposed; and for the more easy Extraction of the Cube Root of any Num-

ber proposed, The under-written Table must also be learned by heart, which will be very easy to do, there being no great Difficulty to remember, that I is the Root of 1; 2 is the Root of 8; 3 the Root of 27; 4 the Root of 64; 5 the Root of 125, and 6 the Root of 216, &c. And allo that 1 is the Cube of 1; 8 the Cube of 2; 27 the Cube of 3; 64 the Cube of 4; 125 the Cube of 5, and 216 the Cube of 6, &c.

PROPOSITION II.

Let it be required to extract the Cube Root of the whole Number 54937601.000000

Point the Number as before, and find the nearest Cube to 54, which is 3; fet 3 in the Quotient, and fubstract its Cube 27 from 54, and augment the Re-on-10 1 27)279 Dividend no of bas about H mainder 27 by 9 the next Figure in the Refolvend, 100 54872 Cube of 28 100 100 100 which Name is here given to the whole Number which Name is here given to the whole Number 54937601; and so continue throughout the whole 4332) 656 Dividend Work; then divide the Dividend 279 by 27 the tri- 3 34872000 Cube of 380 341 ni a 311 ple Square of the Root 3, and it will give 9 times for the second Figure of the Quotient. But since the Cube of the Quotient 39, viz. 59319, would come out too great to be substracted from the Figures 54937, 43342893) 222695990 Dividend that precede the fecond Point in the Resolvend, 4334239 there must only 8 be writ in the Quotient; then the 54937005653375 Cube of 380.15 Quotient 28 being in a separate Paper (or Place) in all 1995346625 Remains multiplied by 38, and that Product again by 38, gives

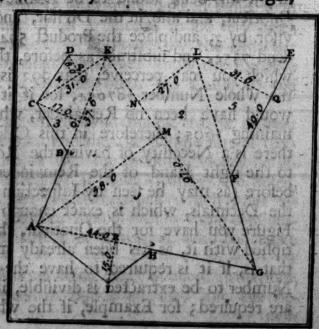
\$4937601.000000(380.15 awab 102 or Dor over the Place of wire 433200) 656010 Dividend 54915331401 Cube of 380.1

the Cube 54872, and this taken from 54937 will leave 65, which being augmented by the next Figure of the Resolvend 6, and divided by the triple Square of the Quotient, viz. by seeking how many times 4232 the triple Square is contained in 656, it gives o for the 3d Figure of the Quotient, for 4332 cannot be had in 656; then Cube the Quotient 38c, and take its Cube 54872009 out of the Refolvend 54937601, and there will remain 656010, which being again augmented by o (to bring the Root or Quotient iuto Decimals) and divided by 423200, the triple Square of the Root or Quotient 380, it gives I for the 4th Figure of the Quotient; the same Method must be continued for the 5th Figure in the Quotient, and so on, if there is more Figures required; the rest of the Work may be seen in the Margin, which will fufficiently explain this Method.

PROPOSITION III.

To find the Area or superficial Content of the irregular Piece of Ground ABCDEFGHI.

Divide the whole Piece of Ground into as few Triangles as possible; in order to which, continue the Sides AB, GF to K and L, and the Side GH to A, which forms the Trapezium AKLG and the two Triangles AIH and FLE, draw the Diagonal KG, making the two Triangles A KG and GKL, draw the Diagonal CK of the small Trapezium BCDK, which makes the two Triangles KCB and CDK. Thus is the whole Ground divided into 6 Triangles; then make all the Perpendiculars at right Angles, with their Bases as is seen in the Figure in the Margin, and find



the Content of each Triangle, by multiplying either the Base and Perpendicular together, and take half the Sum for the Content, or by multiplying the Base and half the Perpendicular of every Triangle, which will also give the Content; then add the Contents of all the Triangles together, which will give 5667 Feet for the Area of the whole Piece of Ground ABCDEFGHI.

PROPOSITION IV.

To find the Side of a Square, whose Area shall be equal to the irregular Piece of Ground above-mentioned.

Extract the square Root of the Area 5667 Foot, and the Root 75 Foot, and 2794 decimal Parts is the Side of the Square required, near enough for Business, it bringing the Contents within less then ______. Parts of a Foot.

PRROPOSITION V.

Suppose one Side of a Parallelogram to be 150 Foot, to find the other Side in order to make the Content or Area equal to the above-mentioned Piece of Ground.

Divide the Area of the Piece of Ground 5667 Foot by 150 Foot the given Length, and the Quotient 37 Foot 78 is the exact Length of the other Side.

PROPOSITION VI.

To find the Area or superficial Content of the Floor or Cieling A in the Plan of the House in Plate 22.

Multiply the Length 45 Foot by the Breadth 75 Foot, or look in the Tables of Feet and Inches at the End of the Book for those Dimensions, and you will find the Content to be 675 Foot; then deduct the Chimnies, one of which is in large as at G, and breaks into the Room 9 Inches and its Breadth is 7 Foot, which makes the Dimension 7 Foot by 9 Inches; this being multiplied together, or looked for in the Table, &c. the Area or Content will be 5 Foot 3 Inches, to which you must add the same Dimension for the other Chimney in the same Room, which will make 10 Foot 3 Inches for the Deduction, and must be taken out of 675 Foot, there remaining 664 Foot 9 Inches for the Content of the Floor or Cieling, &c.

PROPOSITION VII.

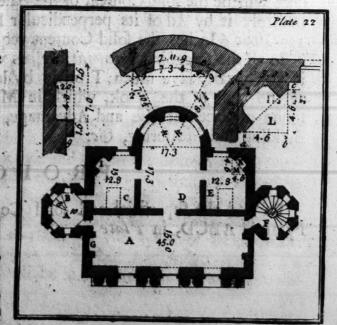
To find the Area of the Floor or Cieling of the Octagon Closet B, which is inscribed in a Square of 10 Foot, in Plate 22.

First find one of the Sides by looking into the Tables of Polygons, and, by the Rule of Three, say, as .9239 (the tabular Number for the Perpendicular of the Octagon) is to 5 Foot the Perpendicular, from the Side to the Center A of the Octogon, so is 7654 the tabular Number for the Side to 4.142 the Side of the Octogon of the Closer; this being done, multiply the Side 2.142 by 2.500 half the Perpendicular 5 Foot, and then multiply the Product by 8 (the Number of Sides in the Octogon) and it will give 82 Foot 84 decimal Parts for the Content, the Method of bringing the decimal Parts into Inches, is multiplying them by 12, &c. as has been already mention'd; and here I must take Notice, that if you have only the Side of a Polygon in Feet, Inches or Yards, &c. and want to know the Radius of the Circle in which those Polygons are inscribed, or the Perpendicular of the Polygons, &c. the Method is, as the tabular Number for the Side of the Polygon, is to the Measure of the Side in Feet, Inches, Yards, &c. so is 1.0000 the tabular Number for the Radius, to the Radius in Feet, Inches or Yards, &c. and so for the Perpendiculars, which may sometimes be of great Service when you cannot come to measure them.

PROPOSITION VIII.

To find the Area of the Floors or Cielings of the Rooms CDE. Plate 22.

Multiply the Length and Breadth of the Room C, 12 Foot 8 Inches by 15 Foot, or look for the Contents in the Table of Feet and Inches, where will be found 190 Foot for the Content, to which add 190 Foot for the Room E, which is the same as C; then measure the square Part of the Room D, 17 Foot 3 Inches by 17 Foot 2 Inches as before, either by the Tables or Multiplication, &c. and the Content will be 297 Foot 6 Inches and 12; then for the circular Part (it being half a Circle) find the Circumference of the whole Circle by multiplying the Diameter 17.3 by 3.1416, and take half the Product for the Circumference of the Semi-circle,



and multiply it by half the Radius, that will give 116 Foot to Inches and this for the Area of that Part of the Room, what remains to be done, is to deduct the Chimneys I and H for the two Rooms C and D, and the Chimney K in the Room E, which is a right-angled Triangle. The angular Chimney I forms a small Square, whose Sides are 5 Foot, the Area of which is 25 Foot, out of which the Triangle L must be deducted, therefore multiply ab the Base 4 Foot 6 Inches by 2 Foot 3 Inches, half the Perpendicular be, which makes to Foot 1 Inch and ;, this being taken out of 25 Foot, there remains 14 Foot 10 Inches ; for the Deduction, out of the Room C. The Triangle M in the Room E being the same as the Triangle K in which the Chimney stands, and also the same Dimensions as the Triangle L, which was last measur'd, the same Area, which was 10 Foot 1 Inch ; will serve for the Deduction out of the Room E; and the way to measure the Chimney H for the Deduction, is to multiply the Circumference de 7 Foot 11 Inches 12 by half the Radius bi, which is 4 Foot 2 Inches iths, and this gives the Area of the whole Segment of the Circle dkbe; then must the Area of the Segment f g k b be found in like Manner, that is by multiplying the Circumference fg 7 Foot 3 Inches , by half the Radius fb, which is 3 Foot 11 Inches ; then subtract the lesser Area from the greater, and there will remain for the Deduction of the Breast of the Chimney, &c. 5 Foot 8 Inches 1sths, &c. but as this is somewhat tedious and troublesome to find the Arch-line de when the Building is erected, it will be sufficient to measure the Arch f g with a Rule, that will bend to the circular Part, and add to it 4 Inches ;, which is the Distance from the Angle f to the Line 1.2. and is perpendicular to the Chord-line fg; then multiply that Length, which will then be 7 Foot 7 Inches; by 9 Inches, and it will produce 5 Foot 8 Inches, and is, which is near enough for any Bufiness, the difference between the true way and this being less then ; one twelfth of an Inch; then add the Contents of the Rooms CDE together, and also the Deductions by themselves, and from the total of the Rooms take the total of the Deductions, and there will be left for the Area of the Rooms CDE 763 Foot 8 Inches 1sths.

PROPOSITION IX.

To find the Area of the circular Stair-case F, whose Diameter is 10 Foot. Plate 22.

Square the Diameter 10 Foot, and multiply that Product by 7854, it will give the Area; or, if you find the Circumference by multiplying the Diameter 10 Foot, by 3.1416, and then multiply half the Circumference by 5 Foot the Radius or Semi-diameter, it will also give the Area.

PROPOSITION X.

To find the superficial and solid Content of the square Pyramid ABCD with its Base HI.

For the superficial Content, multiply the Length of the Base 5 Foot 6 Inches $\frac{2}{12}$ by 1 Foot 5 Inches the Height, and that Product by 4 for the Sides; then for the Top-part or Off-set I, measure the Length from 1 to 2, which will be 5 Foot 2 Inches $\frac{1}{12}$, and multiply it by 3 Inches $\frac{1}{12}$ the Breadth, and that Product again by 4 for all the Sides; then for the upper Part or Pyramid A B C D, multiply 16 Foot 8 Inches $\frac{1}{12}$ the Length of the Side D B C, which is the Line I D, by 10 Foot the Length of the two base Lines of the Pyramid A B, B C, and it will give the Content, or if the Length is multiply d by half the Line A B, or B C, 2 Foot 6 Inches, and that Product again by 4 for all the Sides, it will also give the Area or superficial Content required.

For the folid Content.

Square the Length of the Base H 5 Foot 6 Inches; (which is multiplying 5 Foot 6 Inches it by 5 Foot 6 Inches is and multiply the Product by 1 Foot 5 Inches the Height, and that Product will be the solid Content of the Base H; then square 5 Foot the Base of the Pyramid, and multiply it by 3d of its perpendicular Height, which is 5 Foot 6 Inches, and the Product is 137 Foot 6 Inches the solid Content required.

In all the foregoing *Propositions*, as well as those which are to come hereafter, you if you please, save much Trouble by looking for the Areas or Contents, &c. in the Tables at the End of the Book, which in Mensurations consisting of many Dimensions, will be found of excellent Use and Advantage, not only to Learners, but to all others conversant in Building and Measuring, &c.

PROPOSITION WILL SO THE CONTENT OF THE PROPERTY OF THE PROPERT

To find the superficial and solid Content of the Frustrum ABCELFG, or Piece of the Pyramid ABCD, in Plate 23.

a Circle) had the Circumstance of the winder Circle by multiplying the Danneter test by ... and the halfe take the the Cartestance of the Samu-circle.

melius and .; then for the out olar Part (ivixing balf

Part of the B. is referring

And viz: for the superficial Content, take the Side FG at the top, which is 1 Foot 8 Inches from BC; Foot, and to half the Remainder add the Side at top, which is 1 Foot 8 Inches; then multiply the Product by 11 Foot 1 Inch 2, the middle Line of the Side FGBC; then multiply that Product by 4 for the other Sides, to which if you please to add the Area of the top ELFG, it will give 148 Foot 4 Inches for the Area or superficial Content of the Frustrum ABCELFG.

For the solid Content:

Let the Sides be continued to D, which will form the Pyramid ABCD, and to know the Length of its Axis or Perpendicular D K, the Method is to use the following Proportions: As the Difference of the Sides B C, FG 3 Foot 4 Inches, is to the little Side F G 1 Foot 8 Inches; so is the Height or Axis I K, 11 Foot to 5 Foot 6 Inches the Height of the Axis KD: Or as the Difference of the Sides B C, FG 3 Foot 4 Inches is to the greater Side B C 5 Foot; so is the Height I K, or Axis of the Frustrum, 11 Foot to 16 Foot 6 Inches, the whole Height I D; from which if you take 11 Foot 6 Inches, there will remain 5 Foot 6 Inches for the Height of the small Pyramid EFLGD; then find the Content of the lesser Pyramid by the Method already taught, and take its Content 5 Foot 1 Inch 1 Part 1ths, from the solid Content of the greater Pyramid, as before, and the remainder 132 Foot 4 Inches 10 Parts and 15ths, is the solid Content of the Frustrum ABCELFG.

PROPOSITION XII.

To find the superficial and solid Content of the Pedestal and part of the Column BCDEFG, in Plate 23.

For the superficial Content; and first the Plinth G of the Base of the Pedestal, being the fame Length and Breadth as the Base of the Pyramid, the same Contents will serve; the next thing is to girt the Mouldings F with a String or piece of Tape, which suppose to be 12 Inches 7ths; and multiply it by the Length 4 Foot 9 Inches 4 (which is the Breadth of the Die of the Pedestal, and 8 Inches ; added to it for the Projection of the Mouldings, as the Line ab) then multiply that Product by 4 for the Number of the Sides, and it will give the Area of the Mouldings of the Base, &c. the same must be done for the Capital D, and for the Dado or Die of the Pedestal E, you must multiply the Height 4 Foot 10 Inches 13 by the Breadth 4 Foot 1 Inch -2ths, and that Product by 4 for the Sides, will give the Area; then for the Top of the Capital cd, 4 times 8 Inches ; its Breadth, which is 2 Foot 10 Inches by 4 Foot 9 Inches 12, the same Length that was taken to the Mouldings of the Base (because the Projections are the same) will give the Area; then for the Base of the Column, multiply the Length of the Plinth C, 4 Foot 1 Inch - by 6 Inches its Height or Breadth, this 4 times gives the Area; then girt the Members or Mouldings of the Base from C to H, which suppose to be 1 Foot 9 Inches and multiply it by the Circumference of a Circle, whose Diameter is the Diameter of the Column, and Projection of the Base together, which makes 3 Foot 7 Inches for the mean Diameter of the Base, and consequently the Circumference must be 11 Foot 3 Inches -th, these being multiplied together gives the Area of the Mouldings of the Base, with the Cin-Eture and List at the Bottom of the Column: There remains now only Part of the Column B, whose Length is 9 Foot and Diameter 2 Foot to be measured, this being a perfect Cylinder, you must multiply the Length 9 Foot by 9 Foot 5 Inches ., the Circumference, which gives the Superficies required. The top Part on which the Ball or Globe, &c. is placed need not be measured; for when the next Stone or other Part of the Column is placed on it, it will not be required

For the folid Content.

The Plinth G being the same as in the Pyramid need not be measured again; and for the Mouldings of the base Square, the Length 4 Foot 9 Inches 4, and multiply the Product by the Height & Inches ;; then for the Dado or Die of the Pedestal E, square the Breadth 4 Foot I Inch this, and multiply the Product by the Height 4 Foot 10 Inches - the Cap D of the Pedestal E, square the Length 4 Foot 9 Inches sths, and multiply that Product by the Height i Foot ithis, For the Plinth Cof the Base of the Column B, square the Length 4 Foot I Inch -, and multiply the Product by the Height 6 Inches, and for the Mouldings or Members of the Base of the Column, multiply the Area of a Circle, whose Diameter is the Diameter of the Column and Projecture of the Base (which is 3 Foot 7 Inches as before) by its perpendicular Height 1 Foot 1 Inch , including the Cincture and List at the Bottom of the Shaft of the Column; and lastly, for the Column B, multiply the Area of a Circle, whose Diameter is equal to that of the Column, by the Height 9 Foot, which finishes the whole Work; but it is necessary here to observe, that the above Method teaches to measure the exact Quantity of Stone, &c. when wrought, and that it is usual to allow for the Waste of Stone in the Mouldings, &c. cut by the Chiffel; and indeed this feems to be but reasonable, for in the Base of the Column alone, there is 11 Foot less than must be in the Stone it is wrought out of; and therefore I may venture to affirm, that whenever it is not worth the while to faw the Stone for the Mouldings, and that you are obliged to work it with the Chiffel, it must be allow'd for, either in Price or Quantity.

PROPOSITION XIII.

To find the superficial and solid Content of the Cone or round Pyramid CEF, with the Base or Plinth B, in Plate 23.

For the superficial Content of the Base or Plinth B, multiply the Length of the Side B by its Height 2 Foot, and that Product by 4 for the other Sides,; then for the Cone CEF, multiply the Circumference at Bottom 12 Foot 10 Inches - by 8 Foot 9 Inches this, half the Side CF, or CE, and the Area or Content will be 113 Foot 4 Inches.

For the folid Content.

And first of the Plinth B, square the Length of the Side B, and multiply the Product by the Height 2 Foot; then for the Cone, find the Area of the Base (which is a Circle of 4 Foot 1 Inch - Diameter) as has been already taught, and multiply it by 5 Foot 10 Inches one third of the perpendicular Height, or Axis C D, 17 Foot 6 Inches, and it will give 13 Foot 2 Inches 4 for the solid Content required.

PROPOSITION XIV.

To find the superficial and solid Content of the Frustrum of the Cone CEF, in Plate 23.

For the superficial Content, add the Circumference of the greater Base E F 12 Foot 10 Inches -1, to the Circumference of the lesser Base at the Top GH 4 Foot 3 Inches -1, this, and multiply their Sum 17 Foot 1 Inch 10 by the Side GE, 11 Foot 8 Inches 11, and half the Product is the superficial Content required.

And for the folid Content.

Of the Frustrum GHFE, take the solid Content of the lesser Cone CGH, from the solid Content of the greater Cone CEF, and the Remainder is the solid Content of the Frustrum required; in order to which say, as the Difference of the Diameters GH, EF 2 Foot 8 Inches 9 Parts 4 Seconds, is to the little Diameter GH 1 Foot 4 Parts 8 Seconds, so is 11 Foot 8 Inches, the Axis of the Frustrum GHFE to AC, 5 Foot 10 Inches the Axis of the lesser Cone CGAH; then will the Work be with the lesser Cone, the same as the greater; that is, the Area of the Diameter GH 1 Foot 5 Inches 6 Parts 11 Seconds, must be multiplied by 1 Foot 11 Inches 4 Parts, the \$\frac{1}{4}\$ d of the Axis CA, and the Product 2 Foot 10 Inches 2 Parts 1 Second, &c. will be the solid Content, and this taken from 13 Foot 2 Inches \$\frac{1}{4}\$, the solid Content of the great Cone, there will remain 10 Foot 4 Inches, &c. for the Area or solid Content of the Frustrum of the Cone required.

PROPOSITION XV.

To find the superficial and solid Content of the Globe or Ball A upon the Column B, whose Diameter is 3 Foot, in Plate 23.

For the superficial Content of the Globe or Ball A, multiply the Square of the Diameter, which is 9 Foot, by 9 Inches 5 Parts 1 Second 2 Thirds, and it will give 7 Foot 0 Inches 9 Parts 10 Seconds and 6 Thirds for the Area of a Circle, whose Diameter is equal to the Diameter of the Ball; this multiplied by 4 gives 28 Foot 3 Inches 1 for the Area of the Superficies; or if you square the Diameter, and multiply it by 3 Foot 1 Inch 8 Parts 4 Seconds, it will give the superficial Content; both these Ways are near enough for any fort of Business whatsoever, even if it were of Gold or Silver, Gr.

For the folid Content.

Square the Diameter and multiply the Product by 9 Inches 5 Parts 1 Second 2 Thirds, and that Product again by 3 Foot the Diameter, and it will give 21 Foot 2 Inches 5 Parts 7 Seconds 6 Thirds, 3ds of which is the folid Content required, or cube the Diameter and multiply it by 0.6.3.4.9, and it will give 14 Foot 1 Inch 7 ths, &c. for the folid Content.

Many more Examples of Mensurations might have been given, but these well understood will be sufficient for the Learner, and what I hope will be thankfully accepted, being the very Marrow and Essence of many learned Authors on this Subject, as well as my own Labours, which is most humbly submitted to the Publick, for the Benesit and Encouragement of all, who delight in the Study and Practice of Architecture.

BOOK

Can D of the Pedel dail found de Learth

Foot a brobert, and multiply the

Ages. It is therefore hoped that what is now produced will have the same Effect, and theet with the same Approbation, which will be the greatest Pleasure that can possibly be to me, having done my best for the Service of my Country (as far as I may be allowed that Expreffion) in endeavouring to bring this Art as near to Perfection as was possible for me to do. But before I quit this Subject, I beg leave to add one * Plate more of the Elevations of the several Forms of Temples, different from what will be found in any Author. Monfieur Perrault in his Translation of Vierwoins, has given the Elevations of five Sorts of Temples, in order to explain and illustrate what Virruvius calls the five Spaces of Buildings, which are, as has been faid before, the Pycnostile, the Systile, the Eustyle, Diastyle and Arzostyle; and in so doing, has given us a perfect Idea of those several Distances or Intercolumnations, particularly that which explains the Intercolumnation of Syftyle, which he has made of the Innick Order.

But whether he has in fo doing exactly followed the Precepts of Vitruvius, I will not take upon me to determine, for altho Vitruvius in the 2d Chapter of the 3d Book doth fay, that when the Columns are placed Syftyle, the Height should be divided into nine Parts and a half. and that one of those Parts are for the Diameter (which makes it plain that when Columns are placed Syltyle, it should be either Corinthian or Composite) yet I say there may have been Examples in the Works of Antiquity to justify this Liberty, of which we are in the Dark at

which will be a Mean between both, and is two l

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Vitruvius in his Preface to the 7th Book, mentions many fine and glorious Buildings, and also the Names of the Authors who wrote of their Proportions, yet I cannot find that he fays any more than that such and such a Temple, &c. was of this or that Order, without so much as naming any of the Sorts of their Intercolumnations, and altho? Pliny does in some Particuhars help out with this Deficiency, yet many are omitted; it is therefore very possible, that there might be Buildings of this Sort, otherwife why does Vitruous himself fay, that the Pycnostyle and Systyle were complained of as being too close for the Ladies to go to fay their Prayers in the Temples, if they held one another by the Hand, as was cuffornary in those Days.

But however, let this be as it will, I am to far from blaming Monsieur Perrault in taking this Liberty, that I do verily believe no Man ever deferved better of the Publick than himfelf, even for this Work only, of his Translation of Virruvius, which is most incomparably fine

and instructive.

I have therefore taken the Liberty to remove all these Difficulties, by making the Designs for the Plates abovemention'd, which with the Alterations of the Entablatures of the several Orders of Columns before spoken of, + will sufficiently fuit the said several Distances, so that some one or other of them, will be fure to be according to the Text of Vitravius, which is what I have incellantly laboured at, and which I hope is done to the Satisfaction of all ingenious and learned Persons, who profess the Study of Architecture. It will now be necessary to take Notice of what is very furprizing, and that is, that in all the Authors I have yet feen they have not fo much as mentioned, nor made Provision for the Current of Water from the Projections of the Cornices and Capitals, &c. in outside Works, except in the Ionick and Corintbian Pedeltals of Palladio and Scanmozzi, where there is fomething like it: Palladio has also done the fame in the Dorick, by making a great Cavetto or Hollow, including the Plinth of the Bale of the Column, which indeed carries off the Water, but the Method is not much approved, on the Account of the Appearance it makes, which is as if the Base of the Column and Capital of the Pedestal were all one, but this is only for the Projection of the Capitals of Pedeltals, the Cornices and other Projections which require it most, being without any Care taken of them, which shall be further explained hereafter.

I might here give many more Instances of several Mistakes and Omissions in several celebrated Authors, but I chuse to pass them over in Silence, and yet I cannot help wishings that Palladio and Scammozzi had been more exact in the Measures of the Ancient Buildings, and also more particular in the Description of their Designs of Modern Buildings, which would have been of great Service to young Beginners: It is therefore my Advice, that whenever their Books are read, that it should be with great Attention and Patience, for there is many Things, which will not be understood at the first reading, and to observe that there are some small Mistakes in the Minutes or Measures of the Orders, which may with a little Care and Application be

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rectified an navola of his habital One Thing more I must beg leave to explain, for it is very material, and indeed it is almost the very Life and Soul of Architecture, and what none of our most celebrated Architects, at least none that I know of, has taken any notice of, and that is, what Method is best to take in forming the Heights of Entablatures, both to outfide and infide Works, when there are no Columns or Pilatters, and also to form an Ordnance for the Columns and Pilatters, when they

are used without Pedestals.

The Method generally used by our Artificers, has constantly been to have little or no Regard to the Lofs of the Pedeftal, but to divide the Height of the Room or Place where the Columns or Pilasters were to stand into the same Number of Parts as the Column and Entablature conlifts of without a Pedestal, which makes the Height of the Entablature much larger than it fhould be, for the true Proportion of the Column and Entablature, is when the Column or Plaster bath a Pedestal. Strate welve to the divided the best of T field trans are for the flarablactic, the remaining ten Ports and a Malf is for the Column or Pis

thom is the Diamour

to I

Therefore the following Method is proposed, which is, to take the mean Height, when there is to be Columns or Pilasters; and when there is neither Columns nor Pilasters, the Height of the Entablature should be the same as when there is a Pedestal; as for Example if we would place the Corintbian Column with its Pedestal in a Room or Hall fifteen Feet high, the Method would be to divide the Height into forty-four Parts and a Half, nine of those Parts will be the Height of the Pedestal, Twenty-nine the Height of the Column, including its Base and Capital, and fix and a half will be for the Entablature either with or without the Columns or Pilasters, &c. And to place a Column or Pilaster of the Corintbian Order without a Pedestal in the same Height, the Method is usual to divide the Height into thirty-five Parts and a Half, twenty nine of which are for the Columns, and fix and a Half for the Entablature, which makes the Entablature two Feet eight Inches eleven Twelfths and a Half, as near as can be divided, which is too large; and by the first Method with the Pedestal, the Entablature is only two Feet two Inches three Twelfths and a Half, &c. (which is the Height the Entablature should have, as well when there is Columns or Pilasters with Pedestals, as when there is no Columns or Pilasters, &c. as was said before, but cannot (to prevent Miltakes) be too often repeated.) But when there is to be Columns or Pilasters without Pedestals, both Heights should be added together, which makes four Feet eleven Inches and one Quarter, the Half of which will be a Mean between both, and is two Feet five Inches seven Twelfths and a Half for the Entablature, when the Columns or Pilasters have no Pédestals.

To find the Diameter of the Column according to this new Proportion, it will be necessary to take the Height of the Entablature from the whole Height where the Column is to stand, viz. two Feet five Inches feven Twelfths and a Half from fifteen Feet, the supposed or given Height, and the Remainder twelve Feet fix Inches four Twelfths and a Half, must be divided into twenty-nine Parts, and three of those Parts will be the Diameter, which is one Foot three Inches fix Twelfths and a Half as near as can be divided, which is bigger than the Diameter would have been, if the Column had had a Pedestal by three Inches five Twelfths, and it is also four Twelfths of an Inch larger in the Diameter, than it would have been, if this Medium had not been used, but then it is higher in Proportion, and gives a fine Dimension for the Entablature suitable to the Column, &c. and to the Height of the Room or Place where

it is to stand, in lieu of that which would have been too large.

It may now perhaps be asked, why the Entablature which is for the Columns or Pilasters when they have a Pedestal (and is as it were the true Standard, Size or Dimension for Entablatures) may not serve when the Columns or Pilasters have no Pedeltals and again, why should not the Entablature have the fame Proportion to the Columns or Pilasters, when without Pedeltals, as well as when they have? To the first Question the Answer is very obvious, viz. that in this Case the Columns or Pilasters would be very large, and the Entablatures very small, in Proportion to their Bigness, and that it would have the same Appearance, as a very large Man would make with a Child's Hat on his Head; and in the other Cale, the Entablature would be too large as is already mentioned, and would look like a prodigious large Man or Giant on his Knees, both which are disproportionate, and ought to be excluded from Practice by our Connilleurs in Architecture.

This however, (as it is an Affair of great Consequence, in relation to the Beauty and fine Proportions of our Buildings, and also because many knowing and skilful Persons in the Art of Building, have different Ideas of what is beautiful) shall be left to the Discretion of the Architect, and other Builders, to put in Practice as they please; only for my own Part, I shall always make it a Rule to govern myself by, and it is what I would persuade others to do, having found

by Experience the good Effect it produces.

I shall therefore proceed to speak of what should have preceded this Digression; which is, that if any should think the above Method in calculating the Height of the Columns and Entablatures, &c. too much Trouble, I have made a new Projection for Entablatures to Columns without Pedestals, which is very near the said Medium, and will always continue the same, let the Largeness or Height of the Columns be what they will; for Example, when the Columns or Pilasters are to be in the Inside of the Building and without Pedestals, the Proportions are a follow, viz. the Mikards of Mechanistof the Olders, which have with a certain

The Tufcan without a

For the Tuscan, or the Height in which it is to stand, may be divided into eleven Parts, two of those Parts are for the Entablature, and the other nine for the Column, with its Base and Pedestal for Capital, &c. which said nine Parts, being again divided into twenty-three Parts, three of those Parts is for the Diameter. why the thing in withou you talk safe to went I safe anot first

The Dorick may be divided into eleven Parts and a Half, two of those Parts are for the En-The Dorick without a tablature, and the other nine Parts and a Half being divided into twenty-five Parts, three of Pedeftal for them is the Diameter. the Infide. The lonick may also be divided into twelve Parts, two of which are for the Entablature, and The Ionick

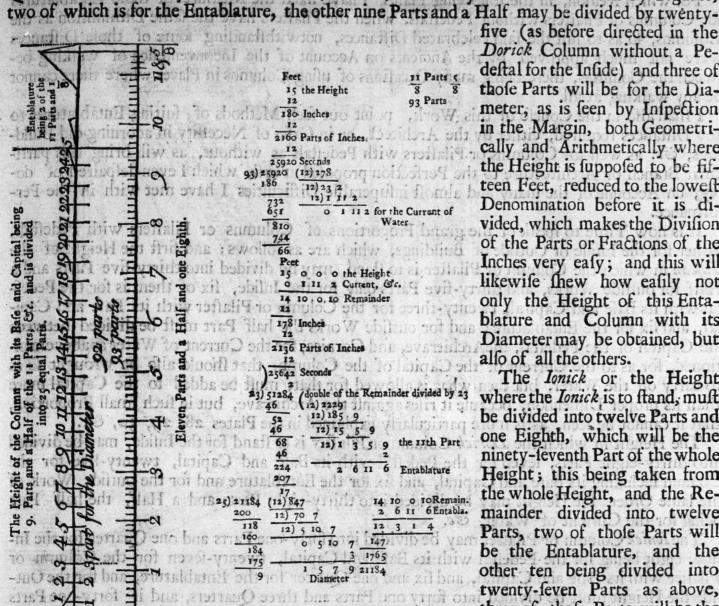
without a the other ten being divided by twenty-feven, three of those Parts are for the Diameter: And, Pedeflal for For the Corintbian, the Height may be divided into twelve Parts and one Quarter, two of the Infide. the faid Parts being for the Entablature, and the remaining ten Parts and one Quarter (which thian with. is for the Column) being divided into twenty-nine Parts, three of them will be the Diameter.

The Composite Column or Pilaster may be divided into twelve Parts and a Half, two of the out a Pedestal for the faid Parts are for the Entablature, the remaining ten Parts and a Half is for the Column or Pi-The Compo- laster, which being divided into thirty equal Parts, three of them is for the Diameter.

When the Columns or Pilasters are without Pedestals and to be placed on the outside, there Pedestal for ought to be one eighth of those Parts abovementioned allowed for the Current of the Projecthe Infide.

tions of the Cornices, &c. that is to fay, that the Columns or Pilasters on the Outside without Pedestals, should be divided in the following Manner; and first for the Tuscan, the Height The Tuscan should be divided into eleven Parts and one Eighth, to do which, divide the whole Height into Column for the Outfide eighty-nine Parts, one of those Parts will be the one Eighth, for the Current of Water as without a above; and this being taken from the Height where the Column, &c. is to stand, the Remain-Pedestal. der must be divided into eleven Parts, and disposed of as directed in the Projection of the Tuscan Order, without a Pedestal for the Inside; that is to say, two of those Parts must be for the Entablature, and the other nine for the Column, which faid nine Parts, being again divided by twenty-three, three of those Parts is for the Diameter.

The Dorick Column, &c. or the Height wherein it is to stand, must be divided into eleven The Dorick Parts and a Half and one Eighth, which is eleven Parts and five Eighths, and divides the whole Column for Height into ninety-three Parts, one of which being taken from the Height where the Column without a or Pilaster is to stand, for the Current of Water, &c. as before, leaves the Remainder to be di-Pedestal. vided into eleven Parts and a Half, which is easily done, by dividing the double of the said Remainder by twenty-three, (the Number of half Parts, in eleven Parts and a Half), and the Quotient will be exactly the eleventh Part; that is, as exactly as can be divided by Figures,



five (as before directed in the Dorick Column without a Pedestal for the Inside) and three of those Parts will be for the Diameter, as is feen by Inspection in the Margin, both Geometrically and Arithmetically where the Height is supposed to be fifteen Feet, reduced to the lowest Denomination before it is divided, which makes the Division of the Parts or Fractions of the Inches very eafy; and this will likewise shew how easily not only the Height of this Entablature and Column with its Diameter may be obtained, but allo of all the others.

The Ionick or the Height The Ionick where the Ionick is to stand, must Column for be divided into twelve Parts and the Outside without a one Eighth, which will be the Pedestal. ninety-leventh Part of the whole Height; this being taken from the whole Height, and the Remainder divided into twelve Parts, two of those Parts will be the Entablature, and the other ten being divided into twenty-seven Parts as above,

three of those Parts will be the Diameter.

The Corintbian Column or Pilasters on the Outside, or the Height where they are to stand, The Corinmust be divided into twelve Parts and a Quarter and one Eighth, which is twelve Parts and thian Cothree Eighths, and divides the whole Height into ninety-nine Parts, one of which being taken Outfide from the Height, the Remainder must be divided into twelve Parts and one Quarter, which without may easily be done by multiplying the said Remainder by four, and dividing by forty-nine, and Pedestal. the Quotient will be one of the twelve Parts, &c. two of which is for the Entablature, and the other ten Parts and one Quarter being divided into twenty-nine equal Parts, three of them will be the Diameter. Laftly,

is taken from it, the

The Composite Columns or Pilasters on the Outside may be divided into twelve Parts and a The Composite Half and one Eighth, or into twelve Parts five Eighths, which is the fame Thing, and divides fite Column the whole Height into one hundred and one Parts, one of these Parts is the one Eighth allowed for the Outfor the Current of the Cornices, &c. which must be taken from the whole Height, and the a Pedestal. Remainder divided into twelve Parts and a Half, which is done by dividing twice the faid Remainder into twenty-five Parts, two of those Parts being for the Entablature, the remaining ten Parts and a Half must be divided into thirty equal Parts, and three of them will be the Diameter.

I have been very explicite (tho' I hope not tedious) in the Directions above, relating to the several Heights of the Entablatures, &c. because a small Matter not well understood, often discourages the Practitioner from proceeding with that Pleasure and Satisfaction I most heartily wish him to have, in the Study of this fine and most noble Art (which comprehends many others unnecessary to mention here) but if in the Course of this Work, any such Thing should

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happen, fo as not to be well understood by the Learner (which I shall endeavour to avoid as much as it is possible) let not this discourage our young Practitioner, but let him remember the old Proverb, that a faint Heart never won a fair Lady (which I hope will meet with a favourable Construction) and also to take the Advice of that great Master in Deligning and Perspective Andrea Pozzo; which is, to begin his Work chearfully, with a Refolution to draw all the Lines thereof to the true Point, the Glory of God, and I dust promise him good Success in fo

honourable an Undertaking.

What has been faid in Relation to Entablatures, &c. for Columns or Pilasters without Pedestals, has been only in Relation to the several grand Divisions of the several Orders, &c. we should now come to the smaller Divisions of the Entablatures, and also to the particular Members of each Division, which would be endless to describe in Words, further than to acquain the kind and generous Reader that the Measures abovementioned will, of Necessity, make fuch Alterations in the feveral Members of the Entablatures and Diameters, &c. of Columns that have no Pedestals, that they will not furt any of the Distances mentioned by Vitruvius, which is very often required, as well as other Diffances that Necessity or Choice leads one to.

For which Reafon, in the following Plates, I have fixed the Measures of those Entablatures for Columns or Pilasters without Pedestals, when the Pilasters have the same Diminution as the Columns, fo as to fuit the faid celebrated Distances, notwithstanding some of those Distances were not much approved by the Ancients on Account of the Inconvenience of walking between the Columns, there being many Occasions of using Columns in Places where there cannot

be any walking at all.

I shall also in the Course of this Work, point out such Methods of suiting Entablatures to any Distances required, either by the Architect, or in Cases of Necessity in adorning old Buildings, &c. as well for Columns or Pilasters with Pedestals as without, as will bring this particular Branch of Architecture to the Perfection proposed at first, which I even despaired of doing, on Account of the many and almost insuperable Difficulties I have met with in the Performance.

The Tuscan for Infide Works.

It is now Time to speak of the grand Proportions of Columns or Pilasters with Pedestals, Column, &c. either for the Inside or Outside of Buildings, which are as follows; and first the Height of the with the Pe- Tuscan in which the Column or Pilaster is to stand, may be divided into thirty-live Parts and a Half for outfide Works, and thirty-five Parts only for the Infide, fix of them is for the Pedefand Outside tal with its Base and Capital, twenty-three for the Column or Pilaster with its Base and Capital, and fix for the Entablature; and for outfide Works the half Part must be divided between the Capital of the Pedestal, the Architrave, and Cornice, for the Current of Water as abovementioned, for as to the Current of the Capital of the Column, that should also be wrought so as to carry off the Water, but then what is allowed for that, must be added to the Capital more than its proper Dimension, because it rises against the Architrave, but in such small Proportion, that it cannot be seen, as is more particularly explained in the Plates 28, 29, 30, &c.

The Height in which the Dorick Column or Pilaster is to stand for the Inside, may be divided The Dorick with the Pe- into thirty-eight Parts, seven for the Pedestal with its Base and Capital, twenty-live for the Column including its Base and Capital, and six for the Entablature and for the outside Work of the same Order, the Height may be divided into thirty-eight Parts and a Half, the half Part

being for the Current of Water, &c.

The Ionick Column or Pilaster may be divided into forty-one Parts and one Quarter for the In-Column, &c. side, eight being for the Pedestal with its Base and Capital, twenty-seven for the Column or Pilaster with its Base and Capital, and six and one Quarter for the Entablature, and for the Outfide the Height must be divided into forty one Parts and three Quarters, and if forty-one Parts and Outside and a Quarter the Height of the Column, &c. is taken from it, the remaining half Part will be for the Current of the Projections, &c.

The Corintbian Column or Pilaster may be divided into forty-four Parts and a Half for the thian with Infide, nine being for the Pedestal, including its Base and Capital, twenty-nine for the Column the Pedestal or Pilaster, including also its Base and Capital, and fix and a Half for the Entablature, and for fide and Out. the outside Work of the same Order, the Height must be divided in forty-five Parts, the half fide Works. Part more than is in the Column or Pilaster with its Entablature for the Inside, &c. as above,

being for the Current of Water, &c. And Lastly,

the Quotient will be one of, the the The Roman or Composite Column or Pilaster may be divided into forty-fix Parts and a Half for the Infide, and forty-seven for the Outside, ten being for the Pedestal including its Base and Capital, and fix and a half for the Entablature, the remaining half Part being for the Uses alfideandOut ready mentioned, and it must always be remembered that three of the above Parts is for the fide Works. Diameter in all the Orders.

I should now describe the particular Parts of each Division of each Order, but that is already so well explained in the Plates 28, 29, 30, 31, 32, &c. and made to suit the several Distances before fpoken of, that it will be unnecessary to say any thing more about it here. It will be unnecessary to say any thing more about it here.

From all the foregoing Particulars, I hope every one who has gone thus far with me, will with a very little Application foon be Masters of this most difficult Part in Architecture; but least there should be any thing wanting to satisfy even the most Curious, the following Geometrical Method will be very easy and exact in enlarging the Entablatures of all the Orders, to any Dimension or Size required, and also to suit the several Distances observed by Virruvius, &c. as well when the Entablature is for Columns, &c. with Pedestals as when without which is what is so much wanted and was never done before, that I know of, or at least never published First by any Author.

destal both for Infide and Outfide Works. The Ionick

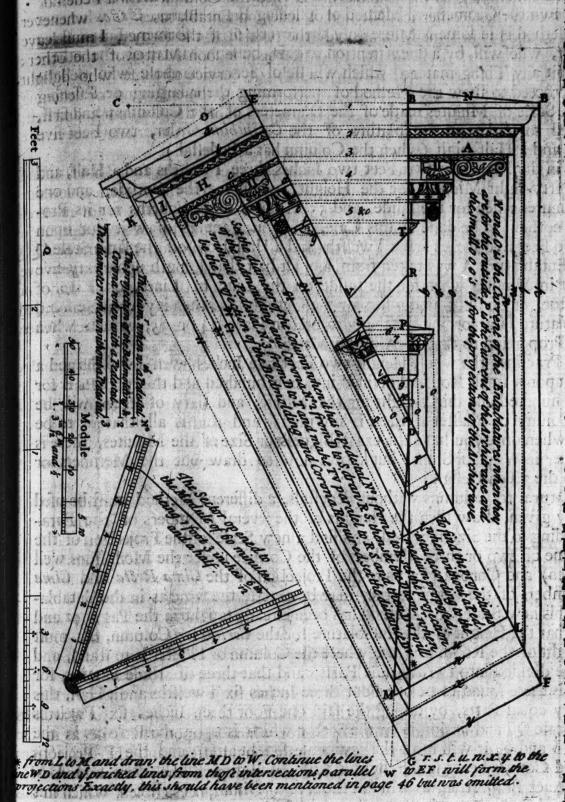
with the Pedestal both for Infide Works.

The Corin-

The Compofite with

First draw out the Entablature of the Order you fix on, according to the Proportions it has when the Column or Pilaster stands upon a Pedestal, and if any particular Distance or Distances is required for the Columns or Pilasters to stand, such Entablatures as will suit those Distances must be made use of, and as we have chose the Corinthian * to explain the different Heights of Entablatures, it will not be improper to fix on the Sort which may be Eustyle, and Diastyle; the Entablature A being drawn as in the Margin, according to the fixed Measures of Eustyle, and Diastyle in Plate 34, &c. continue the Lines BB to C at plea-

Book dl



fure, and by the fame Scale as you drew out the Entablature A, take the new or given Height of the Entablature to be enlarged as before spoken of in Page 42, which is two Feet five Inches feven Twelfths and a Half, and fet it from D till it interfects the Line BBC in E, then draw the Lines 1, 2, 3, 4, 5, &c. parallel to the Line BE, draw also the Lines 6, 7, 8, 9, 10, &c. and at right Angles from DE draw the Lines abcdef g b i, &c. which will form the Height of the feveral Members of the Entablature in exact Proportion to the first at A. Continue the Line ED to F, and also the Line BD to G, then let fall the Perpendiculars k l m n o p q, from the Cornice A to the Line DF, and draw the Lines rst uwxy to the Line DG at right Angles to DF, lastly draw the Lines 11, 12, 13, 14, 15, 16, 17 parallel to the Line EDF, and where they interfect the Lines abcdefgbi, &c. there the Projections

confidence that under circle accounts of the second many than that can be a second of the confidence o will be in exact Proportion to the first Entablature A.

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Column

But when the Entablature is for the Columns, &c. without Pedestals in the same Height, the Diameters will always be larger than those with Pedestals, and in this Case the middle of the Dentel, will not answer exactly to the Center of the Column, neither will the Space between the Modillions be exactly square, altho' in either of these Cases, several Examples in the Remains of Antiquity are to be found; but for those who would be more exact, and would make the Entablature answer all the difficult Cases, both as to the Dentels, and Spaces between the Modillions, as well when the Entablature runs straight, as when it breaks forward over the Columns in that Manner Vitruvius calls Scamilli impares, and also to suit the Distances proposed, there will be a Necessity of enlarging the Projection of the Bedmolding, Modillions, and Corona, to make the Middle of the Dentel stand exactly over the Center of the Column, and to make the Spaces between the Modillions as much more as the Difference is between the Projection in Minutes of the Scale, to the small Diameter, and the Projection in Minutes, according to the largest Scale; that is, if the Projection of the Bedmolding is 18 Minutes, and the Modillion, and Corona, in the Entablature A, is 26 our young Architecter our Page 42. On Placing in placing the

Minutes 1, according to the Scale of Minutes when the Column stands upon a Pedestal, so the Projection of the Bedmolding; the Modillions, and Corona in the Entablature HIK must be 18 Minutes, and 20 Minutes 1 according to the Scale of Minutes made from the Diameter of the Column when it stands without a Pedestal, so that the Entablature HIK will project something more than the exact Proportion of the Entablature A, and the Reason of this is, because the Entablature HIK cannot be (according to the proposed Medium) of the same Number of Minutes, or which is the same Thing, cannot be in the same Proportion to the Column without a Pedestal, as the Entablature A is to the Column with a Pedestal.

I might also have shewn the Geometrical Method of lessening Entablatures, &c. whenever required, but as the Method is in some Measure only the reverse of the former, I must leave that to the Practitioner, who will, by a due Attention to this, be soon Master of the other: But that I may not omit any Thing material which will be of Service to those who delight in this Study, I shall proceed to shew the Method of performing the enlarging or lessening of Entablatures by the Scale of Minutes made of the Diameters of the Columns; and first, suppose it was required to make an Entablature of the Corintbian Order, two Feet sive

Inches feven Twelfths and a Half high (when the Column has a Pedestal)

The Entablature A in the Margin is two Feet two Inches three Twelfths and a Half, and has one hundred and thirty-eight Minutes for the Height, when for the Outlide, and one hundred and thirty Minutes when for the Infide, and 55 Minutes three Fourths for its Projection: Now there is nothing to be done in this Case, if you want to draw it out upon Paper, but to take two Feet five Inches seven Twelsths and a Half from off the same Scale Q in the Margin, as the Entablature A was taken from, and set half that Length upon sixty-five the half of the Height in Minutes when for the Inside on the Line of Lines, or Line of equal Parts on the Sector, or on sixty-nine when for the Outlide, and then is your Scale sitted to draw out the Entablature H according to the Measures in Plate 34 or 35, which when done will be in exact Proportion to that of A in the Margin.

But if it is for real Practice, the whole Height two Feet five Inches seven Twelfths and a Half, may be mark'd upon a small Rod and divided into one hundred and thirty Parts if for the Inside, or into one hundred and thirty-eight for the Outside, and sixty of them will be the Diameter of the Column or Pilaster if there is any used; and this is all that is to be done in this Case, for when once you have the exact Bigness or Size of the Minutes, there is scarce a Workman either in Wood or Stone, but knows how to draw out the Members or

Moldings according to the given Defign.

Several &

Now for the Entablatures to Columns without Pedestals, a different Method must be used for the Reasons already given, draw then the Heights of the several Members of the Entablature as before according to the Size required, and find a new Scale for the Projection of the Bedmolding, (the Name of two or three Members of the Cornice under the Modillions well known to our Workmen) and Corona, for as to the Projection of the Cima Recta and Cima Reversa the upper Members of the Cornice, they may be exactly the same as in the Entablature H; now to find this new Scale, the Method has been already taught in the Pages 42 and 43, where it is faid, that the Height of the Entablature for the Corintbian Column, &c. must be taken from the Height of the Room or Place where the Column or Pilaster is to stand, and the Remainder must be divided into twenty-nine Parts, and that three of those Parts is for the Diameter, which is there found to be one Foot three Inches fix Twelfths and a Half, this being divided into fixty equal Parts, by taking the faid one Foot three Inches fix Twelfths and a Half from the Scale Q, and fetting it on the Sector which is upon the Rule as in the Margin on the Points 6 and 6, it will form the new Scale fought after; and the Projections of the Bedmolding and Corona being fet off by this Scale, will give the Dentels and Modillions, &c. in such exact Proportion, as will suit the several Distances chosen, which in this Cafe was the Eustyle and Diastyle, notwithstanding the Disserence of the Diameters of Columns when with a Pedestal or when without one.

The Method of lessening Entablatures by the Scale of Minutes is no more than making the Scale Q smaller according to the given Height, and is so very obvious to every intelligent Reader, that it would be supersluous to describe it in Words; only for the Entablature of Columns, &c. without Pedestals, it must always be remembred that the Projections are different from the Entablatures of Columns, &c. with Pedestals, as has been already mentioned, and that the Projections of the Bedmolding and Corona must be taken off from the Scale of Minutes when altered, according to the Method above, of enlarging Entablatures. But what will greatly facilitate this Work will be, to make the Measures or Minutes of the several Members of the Entablatures for Columns without Pedestals, of the same Size and Proportion as the Minutes are for the Diameters of the Columns when without a Pedestal; which are set down in the Plates 39, 40, 41, &c. which I think together with what has been said before, accomplishes this Proposition of enlarging or lessening the Entablatures, and is what has taken me up more Time and Trouble than I at first imagined, and what I am assaid has been a little too tedious, though absolutely necessary to have a thorough Knowledge of

The Rules abovementioned are exactly true, and will always be the same for all Sorts of Entablatures which are first fixed to any Sort of Distances whatever, the Method of doing which, is what I have already hinted at, and will come in its due Place; but first I must beg leave to desire our young Architects, not to be too busy or over hasty in placing their

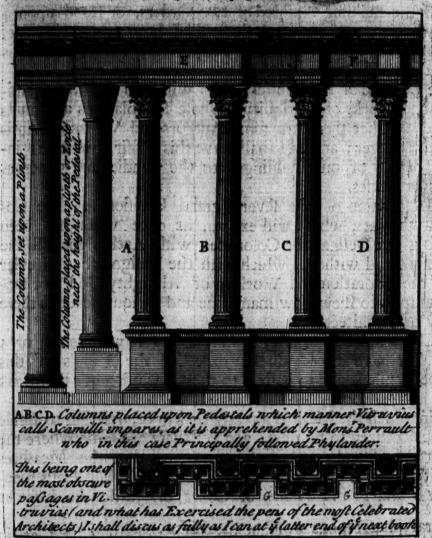
Columns

Columns of Pilasters, in Places where there is no Occasion either for Solidity, or Strength, or Beauty, which is too often done, either through depravity of Taffe or Ignorance of fome Workmen, who no fooner having executed a Piece of Work, according to fome good Debut immediately fancy themselves to be the Authors of the Work, and capable of designing any Sort of Building whatever.

I speak not this of all Workmen in general, for some I know there are who have great Knowledge and Skill in Building, and have withal a great deal of Modesty; but I speak only of those bold and ignorant Pretenders, who have no real, nor true Knowledge in Architecture, nor even of their own Trades, whereof they make Profession; and I could here be content to forgive these unthinking People, if what I have now said would give a Check to their Presumption, and that before they set themselves up for Architects, (in Opposition to those who really are so, which is very often the Case in Building) they would produce something of their own Drawing and Deligning, worthy the Esteem of those who are proper Tudges.

But to proceed, we must also be careful not to place our Columns or Pilasters either for the Infide or Outfide Work, at too great and unreasonable Distances, but at such only where there is a femblance of Strength and Reason for their being placed there, which will add very much to the Beauty and Elegancy of our Defigns: For although we have obtained the Method of fuiting the Entablatures to any Distance whatever, yet if we run into Licenti-

ouinels, we shall never gain any great Reputation for our Skill in Architecture.



There is one Thing I had almost forgot, and that is, the fetting of the Columns upon a Plinth, as in the Margin, instead of a Pedestal, and not upon the Floor as they are fometimes; in this Case the Height of the Entablature of Columns without Pedestals, should be calculated from the Height there is from the Top of the faid Plinth to the Top of the Entablature, unless the faid Plinth is made near the Height of the Pedestal on some particular Account (for otherwife it should never be done) and in that Case it may be reckoned as a Pedestal, and the Height taken from the Floor, &c. as was before directed in the Case of Columns with Pedestals; but in this as in many other Things the Discretion of the Architect must be used.

The Divisions of the several Parts of a Column or Pilaster as already mentioned and explained in the feveral foregoing Plates, are what I take to be very good

Proportions, having fearched into all the Remainders of the Works of ancient Greece and Rome, as well as those of the Moderns for the last Century, in Order to make the most perfect Models of the Orders of Columns, &c. which is however with great Humility submitted to the learned and judicious Architect, who will foon perceive in what I have differ'd

from other Authors.

gel:

But although this is done (and I hope to very good Purpose) yet here I must beg leave to be understood, for I do not by these Alterations in the Entablatures, &c. pretend to establish or lay down new Rules to the Orders of Columns, &c. as mentioned in the Preface: For what I have done in this Respect, has been only to gain the Liberty of giving the Columns or Pilasters such proper Intercolumnations or Distances as may render them Beautiful and Useful; all other Alterations consequential thereto being as nothing in respect of any new Rule: For all the Orders have the same Divisions they have had for many Ages; that is, they are divided into three Parts, one for the Pedeltal, one for the Column, and one for the Entablature; the Pedestal being again divided into three Parts, one for the Base, another for the Dado of Dye of the Pedestal, and the other for the Cimasium or Capital: The Column is also again divided into three Parts, one for the Base, the other for the Body or Shaft, and the other for the Capital; so likewise the Entablature is divided into three Parts, one for the Architrave, one for the Freese, and the other for the Cornice.

These are what I meant by the Rules so well established as not to admit of any Variations for as to the small Alterations made in the Cornices, &c. it is no more than what is absolutely necessary; and if Comparisons are allowed from Architecture to that of human Species, (which is frequently done by Vitruoius and other celebrated Authors) we shall find it to be the same as a fine proportioned Man or Woman a little differently dress d actording to the several Occasions in Life, where the fine Proportions of the Man of Woman still subsist. So it is with the Columns, &c. for the fine Proportions of the principal Parts remain, although a little differently accommodated to the several Designs of private and publick Buildings.

One of these Alterations, if it may be so called, is in the Corinthian and Composite Entablatures which I have made ten Minutes higher than some Authors have done, on Account of their being fo much elevated above the other Orders when the Columns are placed one upon the other, as is done with very good Judgment by feveral Authors, notwithit anding what is faid to the contrary by some others; for it is evident to Sense and Reason, that the higher the Cornice or upper Moldings are placed in a Building, the larger they should be, otherwise they would look mean and trifling. There is nothing, that I know of, that feems to contradict this Doctrine but the Attick Story, (which is composed of small Pilasters, over the Order of Columns or Pilasters, &c. but it is in Comparison of the ancient Buildings, no more than a modern Invention) and when the whole Building confifts of one intire Order of Columns without an Attick over it; for as to the Cornice of the Attick, if it did not bear some Proportion to the smallness of the Pilasters, it would appear very ridiculous; and as for the Entablature when it consists of one Order of Columns or Pilasters (although it is in that Case much larger than it would be if the Building consisted of two Orders, or stood upon a grand Rustick Basement, &...) yet whoever considers it nicely, will I hope agree with me, that it is much better to have an Entablature of a handsome Proportion, than one that is too large or too little for the Height where it stands.

This however is submitted to the Censure of the Publick, who will soon find by examining, that there are several Authors and Works of Antiquity, whose Entablatures are much less than the above Proportions, and also that there are more Authors and Works of Antiquity of great Repute, which are much larger; and so I shall leave this Affair, which is indeed of Moment, in respect of the Beauty of our Buildings, to the candid and generous

Reader, to put in Practice or not as he pleases.

The following Plates, &c. are a Description of the several grand Divisions of the Columns, &c. both with Pedestals and without; which will explain at once what has been treated of in this Book. I have also given Designs for Colonades with Arches for all the Orders of Columns both with Pedestals and without, which with the Design of a circular Church or Temple in Plate 27, for the Adoration and Worship of Almighty God not spoken of before, will be sufficient Examples to shew how many fine and various Beauties there are, and may be found in the Study of Architecture.

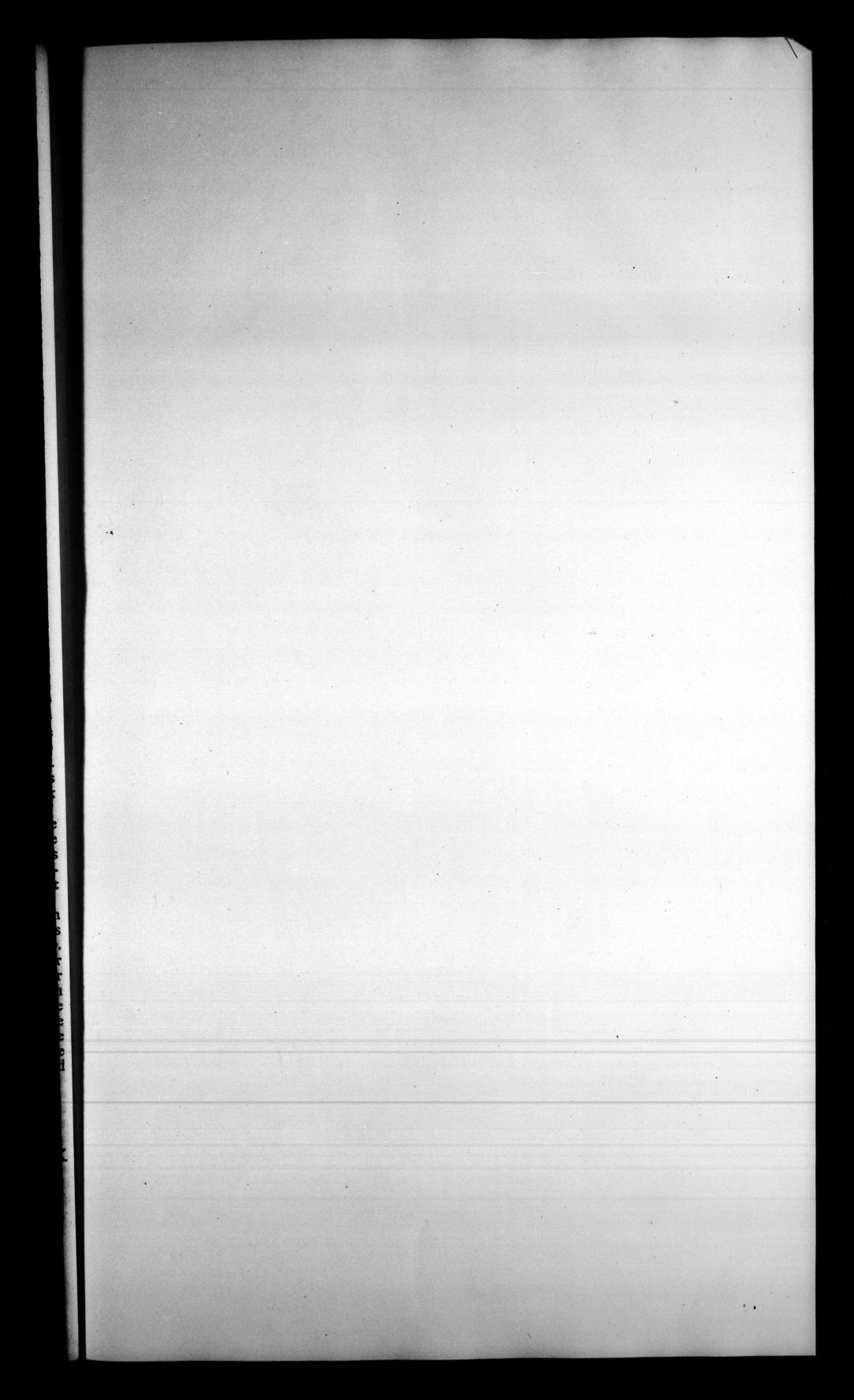
I once designed to have put this Church in Perspective, and also to have given 3 or 4 Plates in large of the same Design, but have already so far exceeded the Bounds of this Chapter, that I must beg leave to be excused, and to hasten to the Conclusion of this Book

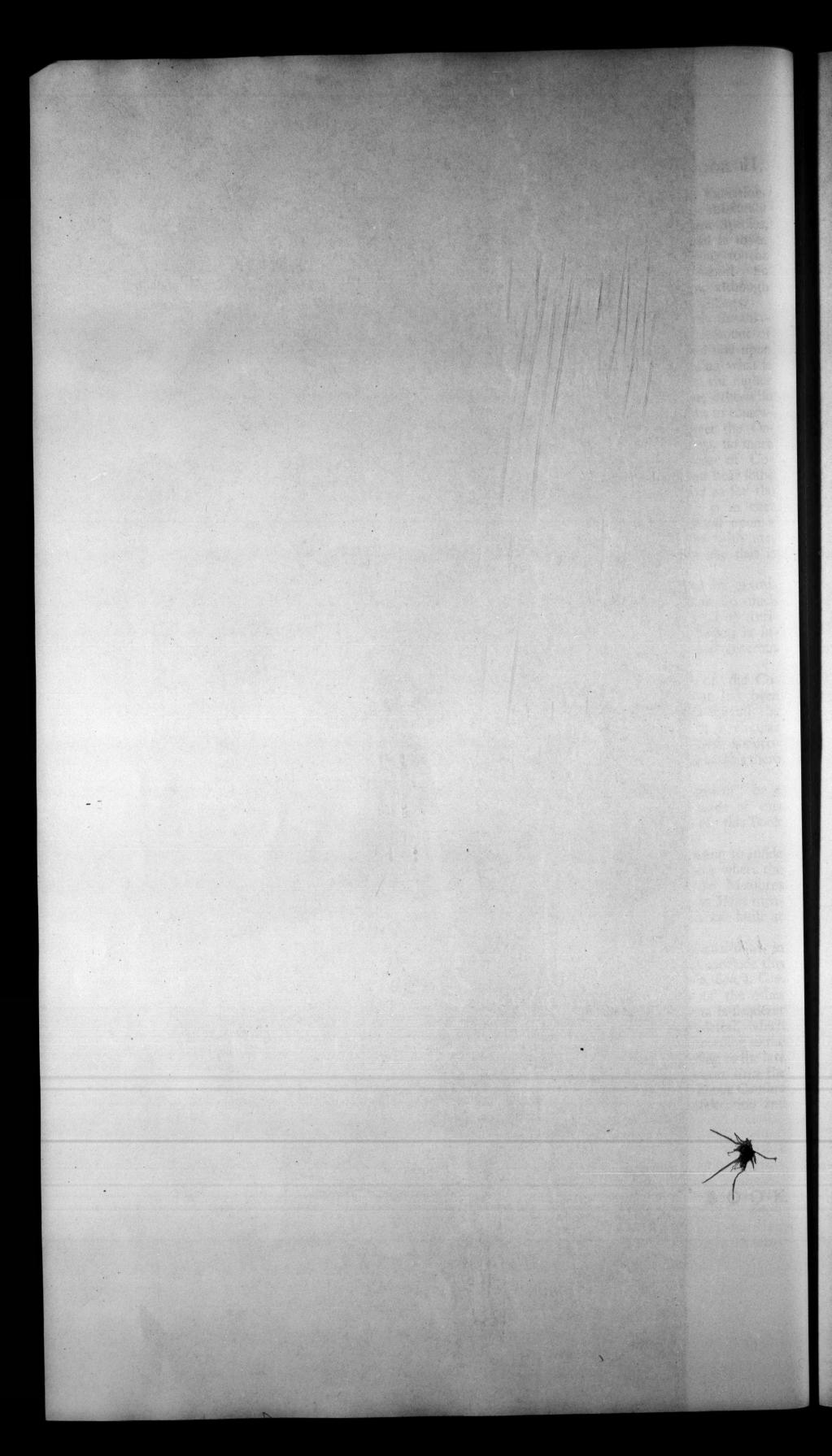
as fast as possible, and to observe,

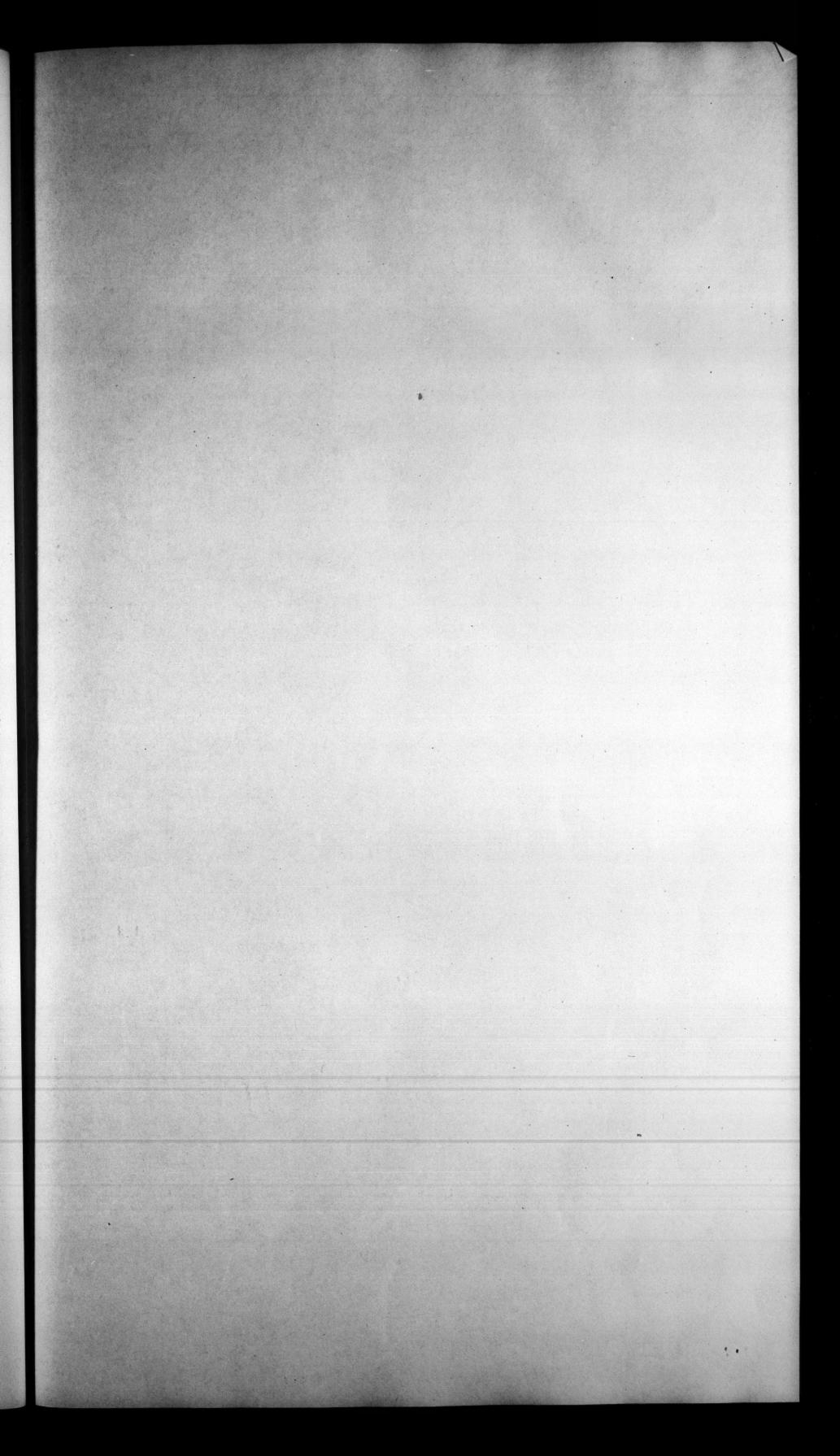
That there are but few Deligns in which the Method already spoken of, relating to Inside and Outside Works, but what will be necessary to be used; and yet there are some where the Inside and Outside Works have such Correspondence one with the other, that the Measures of the Outside and Inside are exactly alike, as may be observed in the Corintbian Halls mentioned by Vitruvius, Cap. 5. Lib. VI. and in the Basilick or Court of Justice he built at Fano.

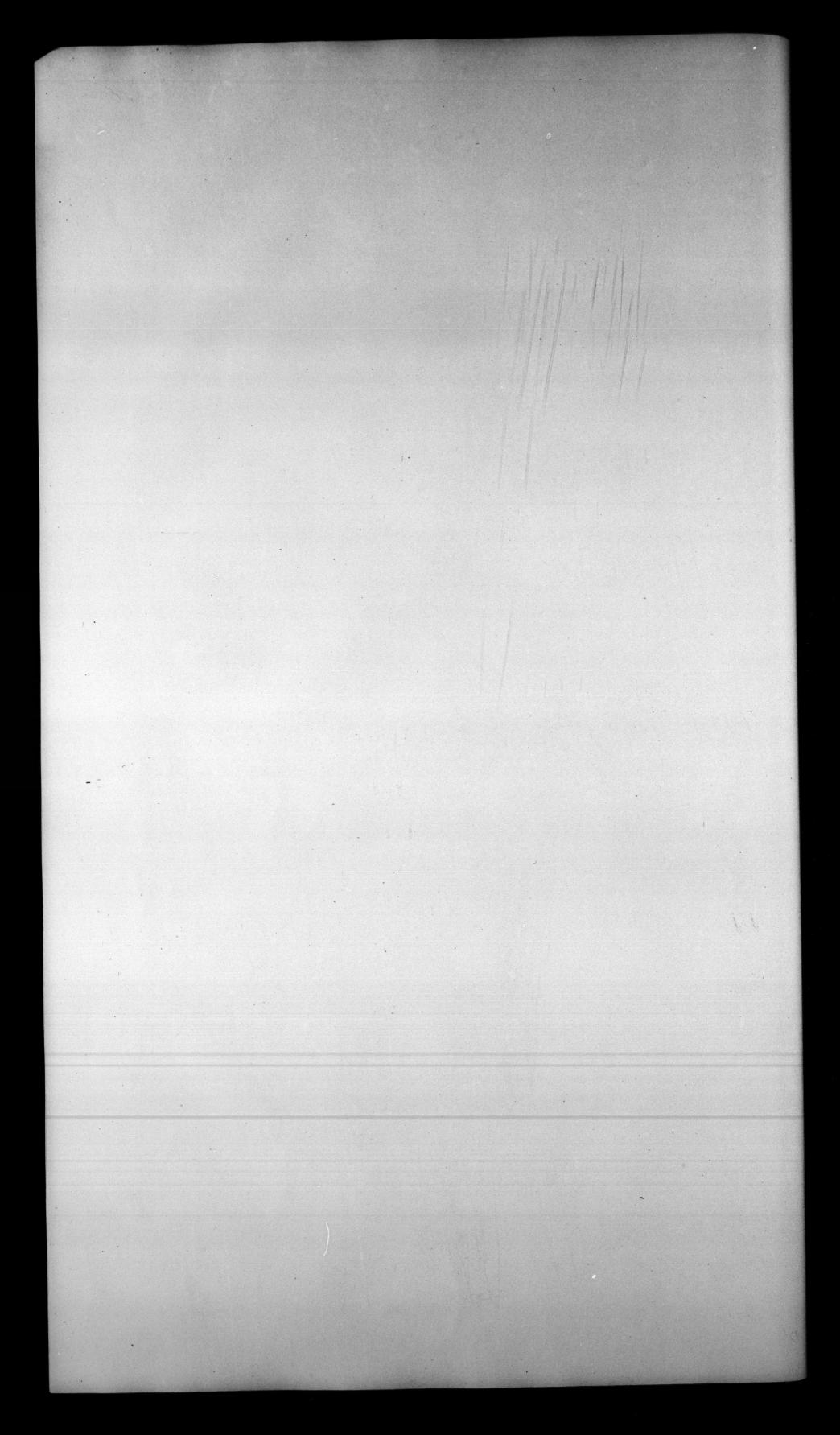
I might now proceed to shew several other Things which are rather to be wonder'd at in several Authors than approved; but I shall decline that invidious Task, and conclude this Chapter, which sinishes the 2d Book, with one Remark; which is, that Palladio, Lib. I. Cap. 18. makes the Pedestal of the Composite or Roman Order, higher than in any of the other Orders, and gives this Reason for it, that it should be so, because that Column is slenderer than the others; and yet he has not observed this Method in the Corinthian Pedestal, which is shorter by nine Minutes and above three Fourths than the Ionick Pedestal, according to the Italian Edition of 1570, and twenty-four Minutes and above one Sixth according to the late Edition of Mr. James Leoni, although the Corinthian Column is always slenderer than the Ionick, which I think is a Demonstration that, in many Things, we may without Censure deviate from those celebrated Authors, provided it be done with mature Consideration and Judgment:

Rule to it all the Orders have the fante Divisors they have had for many deet in the same divided into the Gartes conston the Policifical conston the Cotoma, and on the state that blattages the Pedellot being again divided into three Parts, one for the B. let another the blattages the Pedellot being again divided into the entertor the Cimatans of Capital. The Caluma is alto again divided into the effects, one for the Bale. The locker for the Bale of birds are the other for the Capital to the effect the Entablishes as divided into three Parts, one the the Architecture versions for the Frederic and the divided into three Parts, one the the Architecture we consider the Frederic and the Carolic









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MENSURATION

OF

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BY

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CHIEFLY

Applied to the feveral Artificers Works in Building, but may be used on other Occasions; such as GAUGING, &c.

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THE

PREFACE.

HESE Tables being designed to be added to a general Treatise of Architecture now publishing, may notwithstanding be used separately by Measurers and others concerned in Building, it has therefore been thought proper to publish them before the Book above mention'd, there being a sufficient Number reserved to be added to the Book when published; it is therefore hoped that the Usefulness and Universality of these Tables (there being none like them ever yet calculated that I know of) will be their Recommendation, and excite both Gentlemen and Artificers to encourage not only this Work, but that abovemention'd, which it is presumed will be more useful than any thing of the kind bitherto made publick, at least in our own Language, especially since these Tables will serve in all Countries alike, where their Foot is divided into twelve Parts, &c. I am humbly of opinion to say much more in Recommendation of them will be unnecessary, except that I may safely venture to affirm, that when any Person is a little used to them, he may find the Contents of 3 or 4 Dimensions (taking the whole Measurement together) sooner than most People can work or square one by their Pen. I am therefore in great Hopes, that all sorts of Persons, of all Countries, as well as our own, who are used to Measuring and Building, &c. will find much of their Time and Labour saved; and that if any should despise them in the Working or Squaring their Dimensions, yet the Satisfaction they will find afterwards in proving their Work by the Tables, will be to them a sufficient Compensation for the Purchasing of them.

. Moft obedient Serving

dra recommende



To the READER.

Otwithstanding what has been said in the Preface, I find myself obliged to mention, that the Mensuration of the superficial and solid Contents of some of the Bodies in Plate 23 (altho' the faid Plate belongs to the Book mention'd in the Preface) will be sufficient for instructing any Person to find the Dimensions in the Tables, &c. which

is chiefly aimed at in this Work; however, for the Sake of those who are not well acquainted with measuring Artificers Works, I have drawn up a fort Specimen of each, only desiring the Practitioner to observe when he cannot find any of the Dimensions exactly in the Tables, that he would divide them by 2, 3, 4, 5 or 6, &c. as there is Occasion to bring them within the Compass of the Tables. and then the Contents found in the Tables, multiplied by those Numbers again, will be exact enough for Bufiness of any sort; but this will seldom happen, for in a whole Day's Measurement, there sometimes may not be above 20 or 20 Dimensions to be divided in that Manner, which is nothing in comparison of the remaining Part of the Day's Work; and again, if it should be necessary to divide both the Dimensions, that is, the Length and Breadth of any thing, you must multiply the Contents by the Square of the Number you divide by; as for Example Suppose you divide by 2, then the Contents found in the Tables must be multiplied either by 2 twice, or by the Square of that Number, viz. 4, and if they had been divided by 3, the Contents must have been multiplied either by 3 twice, or by 9, which is the Square of 3, which with a little Practice will become very easy. All that I shall trouble the kind and generous Reader further. with, on this Occasion, is to desire bim not to disuse the Tables at the first or second Trial of them, whenever he meets with any little Difficulty, but to he confant in the Use of them for 5 or 6 Measurements, and then I will venture to assure him that he will find the Benefit and Advantage of the Tables; which that he may do, and that God would be pleased to prosper all his bonest Endeavours, is the fincere and hearty Wish of,

Med wring and Breader, Woft courteous Reader, Time of their Time. Labour Javed; and that if any floated despile them in the Working

of Persons, of all Countries, as well as our com, who are wied to

or Squaring their Dimensions, yet the Satissaction they will find

Windfor, April 10, 1739. sufficient Compensation for the Purchasting of them.

Most obedient Servant,

The Use of the TABLES. EXAMPLEIL

but in the above Limenton, when made into a bill or littimate, Cit. it is only called

Containing the Use of the Tables in measuring of Superficies.

EXAMPLE I.

To find the superficial Content of the square Pyramid ABCD, with its Base HI, in Plate 23.

First set down the Dimensions as you would do in a Book of Measurement, as follows:

a very

Ft. In. Pts.

St. In. Pts.

St

4)5 03 11 3 the four Offlets of 3 Top of the Base

Then look in the Tables for the first Dimension 5 Foot, 6 Inches, 2 Parts, by 1 Foot 5 Inches four times, viz. at the Top of Page 28, for 1 Foot 5 Inches, and in the Index or first Column on the Left-hand downwards for 5 Foot, 6 Inches, 2 Parts, but the Parts being less than i of an Inch need not be regarded, therefore opposite to 5 Foot 6 Inches, and under 1 Foot 5 Inches you will find 7 Foot 9 Inches and a 1, then as that Dimension is four times, to save the multiplying by 4, you may in Page 38 find 7 Foot 9 Inches and a ; in the first Column or Index, and opposite thereto and underneath 4 Foot, you will find 31 Foot 2 Inches, which is the Product of 5 Foot 6 Inches by 1 Foot 5 Inches four times; now to those who are more expert in fquaring Dimensions, it would have been more easy to have multiplied the lesser Sum 1 Foot 5 Inches by 4 in your Mind, which makes 5 Foot 8 Inches, and this being fought for at once in the Tables, will be found in the Index of the Table of the lower Part of Page 41, and opposite thereto and underneath 5 Foot 6 Inches, at the Top is 31 Foot 2 Inches as before for the Contents: We will now, according to this last Method, proceed with the other Dimensions, viz. 5 Foot, 3 Inches, 1 Part, by 3 Inches 1 Part four times, multiply the 3 Inches and 1 in your Mind by 4, it produces I Foot 4 Parts, which being very near I Foot and 4 of an Inch, look for 1 Foot at the Top of the Table of Page 23, and opposite to 5 Foot 3 Inches in the Index, is found 5 Foot, 4 Inches, 3 Parts, and 2ths of a Part, which being fet down as above, you may proceed to the third Dimension of 16 Foot, 8 Inches, 3 Parts, by 5 Foot two times, where at first Sight you may perceive that 16 Foot, 8 Inches, 3 Parts, is more than is contained in the engraved Tables, which do not exceed 12 Foot 6 Inches, therefore halve that Sum, which makes 8 Foot, 4 Inches, and 12, and 1; but those minute Parts we shall lay aside, and look for 8 Foot 4 Inches in the Index of Page 40, opposite to which and underneath 5 Foot, will be found 41 Foot 8 Inches; that being doubled or multiplied by 2, because you divided by 2, produces 83 Foot 4 Inches, which being multiplied again by 2 for the Sides of the Pyramid, makes 166 Foot 8 Inches, to which if you add the other Sums, it will make 203 Foot 2 Inches and 1 whereas in truth it should be 203 Foot, 5 Inches, 3 Parts, 4 Seconds, and 4 Thirds, which Difference is so small, that it is never regarded by the Workmen; and as this is occasioned by the Parts being less than tof an Inch, so if when the Parts are this, you call it tof an Inch, and likewise if when the Parts are iths, you call it half an Inch; and lastly, when the Parts are sths, you will call it this of an Inch, it will ballance the Loss of Parts under 12ths, 15ths and sths; but this indeed is a meer Nicety, which neither the Master nor Workmen need ever give themselves any Sort of Trouble about, and is what I would not have mention'd but for the Satisfaction of the Curious. Sme Lockes Plan, or the real Quantity, the'I think it is

EXAMPLE II. To find the superficial Content of a Boarded-stoor or Roof, &c. whose Dimensions are 20 Foot 6 Inches I shivib bis soldal s tollor by 15 Foot 6 Inches.

Foots or 12 Inches, the Dislerence of those two Sims! First set down the Dimensions 20 Foot 6 Inches by 15 Hoot 6 Inches, then halve them thus. faying, the half of 20 Foot 6 Inches is 10 Foot 3 Inches, and the half of 15 Foot 6 Inches is 7 Foot 9 Inches, then look in the Tables at the Top of Page 45, for 7 Foot 9 Inches, and in the Index or fiest Column for 10 Foot 3 Inches, opposite to which and under 7 Foot 9 Inches, you will find 79 Foot 5 Inches, which multiplied by 2 twice, or by the Square of two, which is 4, because both the Dimensions were divided by 2, makes the Sum 317 Foot 8 Inches, which in truth should have been 317 9 Inches, but the Difference of one Inch in so large a Quantity is - Difference is the by Infpedign only in the Tables, which

not minded by the Workmen, nor indeed any of the Inches in the Totals or Contents, unless a great many Dimensions are to be added together, and then the Inches being added makes Feet: but in the above Dimension, when made into a Bill or Estimate, &c. it is only called 3 Square 17 Foot, without any regard had to the Inches at all, and this I believe will be fufficient to account for any minute Difference in any Example hereafter mentioned, so that I shall not have Occasion to say the same Thing over again.

EXAMPLE III.

To find the superficial Content of a Room of 15 Foot 6 Inches by 12 Foot 4 Inches and a 1, and 12 Foot 6 Inches high in Girt, either for Wainscotting or Painting, &c. and also to know the Number of Yards in the faid Wainscotting or Painting, &c.

First find the Girt of the Sides of the Room, which may be done by adding all the Sides together, which will make 55 Foot 9 Inches, and this being multiplied by the Girt of the Height 12 Foot 6 Inches, by looking in the Tables at the Top of Page 47, for 9 Foot, 3 Inches, 6 Parts, the 5th of 55 Foot 9 Inches, where opposite to 12 Foot 6 Inches in the Index, and underneath 9 Foot, 3 Inches, 6 Parts, is found 116 Foot 2 Inches; this being multiplied by 6 makes 679 Feet; now to bring this into Yards, no more is to be done, but to divide 679 Feet by 9 (which I suppose every one able to do) and the Quotient will be 77 Yards 4 Foot.

Conclusion of the first Chapter.

It would be endless to enumerate the Examples for small Dimensions, such as Boards, Glass. Doors, Window-shutters, &c. which are seen at once by Inspection with the greatest Ease imaginable; I have therefore chose the most difficult, that the Practitioner might not be difcouraged. It remains for me to obviate an Objection that may possibly be made to the Tables. and to shew with what Ease, and to how great a Length they may be carried by any Person a little conversant in Measuring; and first it may possibly be objected, that there is in some of the Dimensions some very minute Parts more than the exact Truth, but in others there is also some minute Parts less, the Reason of which is, that it would have been infinite Trouble to have fet down all the remote Parts, and have made the Work fo expensive, that no one could have had it with Advantage; and indeed it is the Practice of all Measurers to call 3 Foot, 6 Inches, 9 Parts, 3 Foot 7 Inches, and for 4 Foot 7 Inches, and 7 Parts, or 4 Foot 7 Inches, and 11 Parts, 4 Foot 8 Inches, which shortens the Work very much, and is as near the Truth as can be defired, for I have tried in very large Meafurements where the Contents have been fet down as above, and also according to the exact Measure, and have found not above 4 or 5 Inches, either more or less than the Truth, which in my humble Opinion is not to be regarded. But if. notwithstanding this, some should still be unsatisfied, the printed Sheet at the End of the Ta-

The common Way of multiplying Feet, Inches, &c.

| 149 6 149 6 | 6 |
|--|---------|
| 1341 596 159 74 6 74 6 3 6 2 6 2 | 6 3 3 3 |
| 22362 8 | 6 3 |
| By the Ta | bles. |
| 1863 0 | |
| 22356 0 | Total. |

| Foot In. Pts. Foot In. Pts. Foot In. Product of 12 5 6 by 12 5 6 is 155 3 Product of 12 6 0 by 12 6 0 is 156 3 The Difference divided by | By the Tables the Jecond | way. | | |
|---|-----------------------------|-------|---|---|
| The Difference divided by ——————————————————————————————————— | Foot In. Pts. Foot In. | Pts. | Foot | In. |
| The Difference divided by ——————————————————————————————————— | Product of 12 5 6 by 12 5 | 6 is | 155 | 3 |
| Makes 1 Inch, half of this — — — 0 1 Ft. In. Foot In. Pt. Added to 155 3 makes — 155 3 6 Which multiplied by 12 — 1863 6 0 And this multiplied by 12 — 12 | 110duct 01 12 0 0 by 12 0 | 0 15 | 150 | 3 |
| Ft. In. Added to 155 3 makes — 155 3 6 Which multiplied by 12 — 1863 6 0 And this multiplied by 12 — 12 | The Difference divided by - | - 12 | 001 | 0 |
| Added to 155 3 makes 155 3 6 Which multiplied by 12 1863 6 0 And this multiplied by 12 12 | | | 100 (01 (01 (01 (01 (01 (01 (01 (01 (01 | 1 |
| Mhich multiplied by 12 1863 6 o And this multiplied by 12 12 | | | | CONTRACTOR OF THE PARTY OF THE |
| And this multiplied by 12———————————————————————————————————— | Which multiplied by a | 155 | 3 | |
| And this multiplied by 12———————————————————————————————————— | which multiplied by 12 | 18.7 | | 12 |
| | | 1863 | 6 | 0 |
| again makes — 22362 0 0 | And this multiplied by 12 | | | 12 |
| | again makes — | 22362 | 0 | 0 |

bles is according to the Truth, and will square any Dimension that can possibly happen in any Building with a very little Trouble; but now I am to shew to how great a Length the engraved Tables will answer, viz. to 22362 Feet, for suppose 149 Foot, 6 Inches and 1, was to be multiplied by 149 Foot, 6 Inches and 1, the common Way of fuch Multiplication is as in the Margin, but by the Tables there needs no more then to divide 149 Foot,

6 Inches and ; by 12, as for Example 12) 149 6 6 the Quotient being 12 Foot, 5 Inches, 6 Parts and 6 Seconds, may be called 12 Foot, 5 Inches, 7 Parts, which being fought for in the Tables, the nearest that can be found is in the upper Part of the lower Table, Page 48, and is 12 Foot, 5 Inches and 6 Parts, under which, and opposite to 12 Foot, 5 Inches and 6 Parts in the Index is 155 Foot 3 Inches, which being multiplied by 12, and that Product again by 12 (because both the Dimensions were divided) produce 122356 Feet; but as this is 6 Feet some Inches short of the real Quantity, tho' I think it is no great Matter in such a large Number, yet to make it more exact, take the Contents of 12 Foot 6 Inches by 12 Foot 6 Inches, which is 156 Foot 3 Inches, and divide 1 Foot, or 12 Inches, the Difference of those two Sums by 12, which will give you one Inch, half this Inch added to 155 Foot 3 Inches, makes it 155 Foot, 3 Inches and a half; this being multiplied by 12, and that Product again by 12, produces 22362 Feet, which I think is near enough for the most Curious; and altho' this Description seems long and tedious, yet in Practice it is nothing for the Difference of the two Numbers, as also the Divisions of that Difference is done by Inspection only in the Tables, which

a very

a very little Practice will make easy; but these large Dimensions so seldom happen, that I hope it will not discourage any Persons from using this Method whenever they have Occasion. It remains now for me to speak of the Use of the printed Sheet at the End of the Tables, which I shall do in as sew Words as possible; and first, in the working of large Dimensions, there is also a great Difficulty when the Dimensions consist of Feet, Inches and Parts, as in the Dimension in the Margin, where you must either divide the Feet by 12, to multiply by Inches, or else the Inches must be mutiplied by the Feet, and then divided by 12, and sometimes two Divisions must be made before the Product can be set down, which cannot be done without burthening

| Foot In. Pts. 12 | 2)139 Feet by 11 Inches. |
|---|-----------------------------------|
| 35 11 19 | one of the observation of the |
| 695 1417 28 6 | 127 5 139 9 Feet by 11 Inches. |
| 7 4 8 9 | |
| 2 9 | 139 139 |
| 5031 0 0 11 3 | 1529 |
| 35 Foot by 8 Inc | thes. 12)35 Foot by 8 Inches. |
| 12)280 | |
| 23 4 | 23 4 |
| In. 35 Foot 8 Inches. | 139 Foot by 9 Inches. |
| 4 is \(\frac{4}{3}\)d 11 8 4 is \(\frac{1}{3}\)d 11 8 | 12)1251 |
| 139 Foot by 11 Inc | 12) 104 3 hes. 8 8 3 |
| 6 is 1 69 6 | 139 Foot by 9 Inches. |
| 4 is 1 46 4 1 is 12 17 | 6 is ½ 69 6 3 is 4 34 9 |
| 127 5 | 12)104 3 |
| 35 Foot by 3 Inches | 8 8 3 |
| 12)105 | |

the Memory too much, and is besides liable to many Mistakes, for when you are to multiply 139 Foot by 11 Inches, one of the Ways above-mentioned must be used, or what is still longer about, you must divide the 11 Inches into aliquot Parts, as 6 is one half, 4 is one third, and 1 is one twelfth, which is very tedious; all these Methods are fet down in the Margin, where they may be feen by Inspection, to avoid which look in the first Column for 139 Foot, and opposite to it under 11 Inches, which is found at the Top of the Tables, you will find 127 Foot 5 Inches almost in an Instant, so likewise of any other by Feet and Inches; and as for the Parts multiplied by Feet, or Inches, look for the Number of Feet or Inches, &c. in the Index, and opposite thereto in the second Column, under 6 Parts, or \frac{1}{2} an Inch, you will find the Contents, for that Number of Feet or Inches multiplied by 6 Parts, or 1 an Inch, and therefore if you want to multiply by 3 Parts or ½ of an Inch, half the faid Sum is the Product, or if you multiply by 9 Parts or 4ths of an Inch, half the Product added to the Product of 6 Parts, or an Inch, is the Contents; and this I hope is fo plain, that no one can miss it, for if you look in the fecond Column opposite to 139 Foot, you will find 5 Foot, 9 Inches, 6 Parts, the half of which is 2 Foot, 10 Inches, 9 Parts; this being added to the other, makes the Content 8 Foot, 8 Inches, 3 Parts, for 139 Foot by 9 Parts, as above in the Margin;

and if it had been 139 Foot by 3 Parts, or $\frac{1}{4}$ of an Inch, then the 2 Foot, 10 Inches, 9 Parts, had been the Contents; and as for the Multiplication of Parts by Parts, I have omitted it, they being never regarded by the Workmen; but if any should have the Curiosity to set them down, they must be multiplied together, and divided by 12 as above. Where 9 Parts is to be multiplied by 3, which makes 27, that divided by 12, makes 2 Primes and 3 Seconds, for the Primes must always be in the third place, from the Feet and the Seconds in the fourth, as above.

CHAP. II.

Containing the Use of the Tables in measuring Solids.

EXAMPLE I.

To find the solid Content of the square Pyramid ABCD, with its Base HI, in Plate 23.

First set down the Dimensions as you would do in a Book of Mensuration.

| Ft. In. Pts. | 100 10 10 10 10 10 10 10 10 10 10 10 10 | Ft. | In. | Pts. | | |
|--------------|--|-----|-----|------|---|---|
| 5 6 2 30 3 | of the Pyramid. 3 the Height of the Base | 5 | 0 | 0} | 0 | the Square of the Bottom of the Pyramid. the \(\frac{1}{4}d \) Part of the perpendicular Height of the Pyramid. |

Then find the Square of the Base 5 Foot, 6 Inches $\frac{1}{12}$, by 5 Foot, 6 Inches $\frac{1}{12}$, by looking in the Tables as has already been taught, which you will find to be 30 Foot 3 Inches, which is to be multiplied by the Height of the Base 1 Foot 5 Inches; to do which you must divide the 30 Foot 3 Inches by 3, and the Product 10 Foot 1 Inch being looked for in the Index of Page

30, opposite thereto, and under i Foot 5 Inches, at the Top you will find 14 Foot, 3 Inches, and 5 Parts, which being multiplied in your Mind by 3 as you fet the Figures down produces 42 Foot, 10 Inches, 3 Parts, for the folid Content of the Bale of the Pyramid; the other Dimenfion is fo easy, that no one need to look in the Tables, it being only 5 Foot by 5 Foot, which is 25 Foot; but that being to be multiplied by 5 Foot 6 Inches, it will be necessary to take half that Quantity, which will be 12 Foot 6 Inches, then in the Index of the upper Table, Page 43, opposite to 12 Foot 6 Inches, and underneath 5 Foot 6 Inches, you have 68 Foot 9 Inches, which being doubled or multiplied by 2, because it was divided by 2, makes 137 Foot 6 Inches for the folid Content of the Pyramid, which being added to 42 Foot, 10 Inches, 3 Parts, the folid Content of the Plinth or Base, makes 180 Foot, 4 Inches, 3 Parts, for the solid Content of the square Pyramid as desired, the Mensuration of the other Solids in the said Place 23, are to be measured in the same Manner; but as the Measuring those and other Things relating to Superficies and Solids is more particularly described in the Book now publishing, I must refer to that, what having been said already being sufficient to shew the Use of the Tables, which is all that is intended in this Essay; however, I shall for the sake of Learners explain two or three Examples more, which I hope will be fufficient.

EXAMPLE II.

To find the Contents of a Wall of Brickwork of several Thicknesses one upon the other, the lower Part of the Wall being 12 Foot 6 Inches long, and 6 Foot 6 Inches bigh, 3 Bricks thick; the middle Part being the same length, but 10 Foot 6 Inches bigh, and only 2 Bricks and a ! thick; and the upper Part being the same length, and 8 Foot 3 Inches bigh, two Bricks thick.

Set down the Dimensions as before, and they will be as under-written.

In Page 44, opposite to 12 Foot 6 Inches in the Index, and under 6 Foot 6 Inches at the Top, you will find 8 1 Foot 9 Inches; again, in Page 48, opposite to 12 Foot 6 Inches in the Index, and under 10 Foot 6 Inches is found 13 1 Foot 3 Inches; and again, in Page 46, opposite to 12 Foot 6 Inches in the Index, and under 8 Foot 3 Inches, is found 103 Foot 1 Inch; now to bring this Work into Rods, which altho' this is not a proper Place for it, yet some may be desirous to know the Method, therefore you are to understand, that all Thicknesses of Brickwork are first brought to one Brick and a half thick, and then the several Quantities being added

4 of a Rod 68 247 4 of a Rod 204 204

43

together, and divided by 272 Foot 3 Inches, the Quotient is Rods, and the Remainder is Feet, and is as follows; the Contents of the first Dimension is 81 Foot 9 Inches, which being multiplied by 2, because it is three Bricks thick, which is twice one Brick and a half, makes 163 Foot 6 Inches, the fecond being 131 Foot 3 Inches, two Bricks and a half thick, you may divide by 3, the Number of half Bricks in a Brick and a half, and that Quotient being only half a Brick, must be set down twice under 131 Foot 3 Inches, as in the Margin, which reduces that Dimention to one Brick and a half, and is 218 Foot 9 Inches; the third Dimention being 103 Foot 1 Inch, and two Bricks thick, it must be divided by 3 as before, and the Quotient being only half a Brick thick, must be added to the Dimension, which is always three half Bricks, or one Brick and a half, which will make it four half Bricks, that is, two whole Bricks, and contains 137 Foot 5 Inches; these several Sums or Quantities being added together, and divided by 272 Foot as above (for the 3 Inches is never regarded) it produces 1 Rod 4 and 43 Foot.

EXAMPLE III.

To find the folid Contents of several Pieces of Timber, whose Lengths and Sides are as underwritten.

| Foot In. | zd. Foot In. | Foot In. | |
|------------------------|-----------------|--------------------------|------------------------|
| 34 6 long 1 6 Sides 60 | 24 6 long | 12 6 | long 7 |
| i 2 Sides S | Sides | \\ 26 2 5 0 8\\ 0 4\\ \\ | Sides $\int_{0}^{2} 9$ |

First divide 34 Foot 6 Inches by 3, saying, the threes in 3 is 1, which set down as in the Margin, then say, the threes in 4 is 1, and there remains 1, which also set 3)34 6 down, and the Remainder being brought into Inches, and added to the 6 Inches, makes 18 Inches, and the threes in 18 Inches is just 6, which also set down as in the Margin, where you find the 3d of 34 Foot 6 Inches is 11 Foot 6 Inches, then look for 11 Foot 6 Inches in the Index of Page 30, where you will find 17 Foot 3 Inches; this being also divided by 2, or taking the half of it, which may be done at Sight, without

Without putting Pen to Paper is 8 Foot, 7 Inches and a i, and carrying it to the Index of Page 24, where underneath I Foot 2 Inches, and opposite to the said 8 Foot, 7 Inches and 1, is found to Foot 9 Parts, and this being multiplied by 6 produces 60 Foot, 4 Inches, 6 Parts, for the folid Content. The Reason of multiplying by 6 is, because of the two Divisions above-mention'd, which must always be multiplied together, and as the first Division was by 3, and the last by 2, so you may say, twice 3 is 6, and as the multiplication of these Divisions may always be made equal, fo whenever they are above 12, you may halve the Number and fer the Sum down twice; and here I must desire the Favour to be understood, whenever I say, fuch and fuch a Sum or Quantity must be multiplied by 6, or any other Number of equal Parts under 12, I always mean, that such Number may be multiplied (if the Practitioner pleases) by the Tables, as in the last Example, for if you look for 10 Foot 9 Parts in the Index of Page 42, you will find the nearest to it is 10 Foot and i an Inch, opposite thereto under 6 Foot, you will find 60 Foot 3 Inches; but as this is less than it should be by one Inch and half, take the Difference between that and the next Dimension of 10 Foot 1 Inch by 6 Foot, which being 3 Inches, the half of which being 1 Inch and 1, must be added to it, and this Rule in this Case when you come to such minute Parts, which seldom happens, will always be true. There are several other ways of finding the Contents of Dimensions by the Tables, which will be found in Practice, and therefore I leave them for the Exercise of the Ingenious, tho' I think none are easier than those already mention'd. For the second Dimension of 24 Foot 6 Inches, by 1 Foot 2 Inches, take the half of 24 Foot 6 Inches, which is 12 Foot 3 Inches, and opposite to it, under 1 Foot 2 Inches in the Table, Page 26, you will find 14 Foot, 3 Inches, 6 Parts, the half of which is 7 Foot, 1 Inch, 9 Parts, with which you enter the Table, Page 19, where opposite to 7 Foot, 1 Inch, 9 Parts, and under 11 Inches you will find 6 Foot, 6 Inches, 7 Parts, 3 Seconds, which multiplied by 4, for the Reasons before-mentioned, will give the folid Contents of the faid Piece of Timber, which will be 26 Foot, 2 Inches, 5 Parts, and for the last Dimension of 12 Foot 6 Inches by 8 Inches, &c. look in the Table of Page 16, where opposite to 12 Foot 6 Inches, and under 8 Inches, you will find 8 Foot 3 Inches and 10 Parts; which if you carry to the Table of Page 10, you will find opposite thereto 8 Foot, 3 Inches and (which is the nearest to it) and under 4 Inches, 2 Foot 9 Inches and 1 for the folid Content of the faid Piece of Timber.

It having been mention'd in the Title-page, that these Tables may be used on other Occasions, fuch as Gauging, &c. I then thought those Things would of Course occur to the Practitioner, but for fear any Omission might be made an Objection, I have ventured to explain one or two Problems more, tho' it is not pretended to be in these Cases of the same Use and Expedition as

in Building, but possibly may serve where better Helps are wanting.

But before I explain the Method of working any more Problems or Examples, I must desire the Learner to work the Dimensions in the Tables as follows, which will be to the utmost Nicety, and to apply the faid Method whenever there is Occasion. Suppose I was to multiply 12 Foot 3 Inches, by 9 Inches and 5 Twelfths, by the Tables in Page 21, there is no Dimension there nearer than $\frac{1}{4}$, $\frac{1}{2}$, or $\frac{1}{4}$ of an Inch, which is 3 Twelfths, 6 Twelfths, and 9 Twelfths. Therefore always in these Cases when required, take the Contents of the next Dimension more, and the next Dimension less than that demanded, and take the Difference of those Contents, and divide them by 3, if it is among the Quarters of Inches, and by 6, if among the half Inches, the Quotient of either being I twelfth Part of the Dimension; and so many twelth Parts as you want above the Dimensions in the Tables, so many must be added to your Work, as in the Example above, of 12 Foot 3 Inches, by 9 Inches 5 Twelfths; for 5 Twelfths being more than \frac{1}{4} of an Inch by 2 Twelfths, take the Contents of 12 Foot 3 Inches by 9 Inches 4, which is the nearest Dimension less than demanded, and is 9 Foot, 5 Inches, 3 Parts, 9 Seconds; then take the Contents of the next Dimension, 12 Foot 3 Inches by 9 Inches 1, which is the nearest Dimension more than demanded, and is 9 Foot, 8 Inches, 4 Parts and 6 Seconds, and divide the Difference 3 Inches and 9 Seconds by 3, it being $\frac{1}{4}$ of an Inch Difference in the Dimension, and it will be 1 Inch and 3 Seconds for 1 Twelfth of an Inch; and as you wanted 2 Twelfths to the least Dimension, twice that Quantity must be added to it, which 12 will make 9 Foot, 5 Inches, 3 Parts, 9 Seconds, to be 9 Foot, 7 Inches, 4 Parts, 3 Seconds, which is the exact Quantity of 12 Foot 3 Inches by 9 Inches, 5 Twelfths, and this Rule is certain, and may always be applied when any Thing very exact is required.

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The USE of the TABLES in GAUGING, &c.

EXAMPLE L

To find the Quantity of Gallons in a Back or Cooler or other Vessel 8 Foot long, 4 Foot 6 Inches broad, and 8 Inches deep.

Look in the Tables as before taught for the Contents of 4 Foot 6 Inches by 8 Inches, which you will find to be 3 Foot, then multiply that by 8 Foot which makes 24 Foot; that Sum multiplied by 1728, the Number of Cubical Inches in a Foot square, or when there are Feet, Inches and Parts, to be multiplied by that Number, it will be much easier to multiply the Product by 12 three times, as if 5 Foot, 6 Inches, 9 Parts, were the solid Content of any Vessel to be brought into solid Inches, multiply the said 5 Foot, 6 Inches and 9 Parts by 12, the Product 66 Foot 9 Inches multiplied by 12, produces 801, which being multiplied again by 12, makes 9612 solid Inches, so likewise the abovesaid Sum of 24 Foot, there being no Inches or Parts, may be multiplied by 1728, which makes 41472 solid Inches; this being divided by 268.8 for dry Measure, and by 231 for Wine, and by 282 for Beer or Ale, the Quotient will be 154 Gallons, 1 Quart and 9 Inches, which is less than a Pint, for dry Measure, and 179 Gallons, 2 Quarts and 7 Inches and a ½ for Wine Measure, and 147 Gallons 18 Inches, which is about half a Pint for Beer or Ale Measure.

EXAMPLE II.

To find the Quantity of Gallons in a Spheroid or Vessel like a Hogshead, the Diameter at the Head being 3 Foot, and the Diameter at the Bung or Middle 3 Foot 9 Inches, and the Height 4 Foot, all in the Clear of the said Vessel.

Take the one Third of the Square of the Diameter at the Head in Feet, Inches and Parts, &c. and to it two Thirds of the Diameter in the Middle, also in Feet, Inches and Parts, &c. and multiply that Product by the Height; and this Product being multiplied by 9 Inches, 5 Parts, 1 Second, 2 Thirds, gives the solid Content in Feet, Inches, and Parts, which being multiplied by 12 three times successively, brings the said Product into solid Inches, which being divided by the several Inches in a Gallon of Beer, Wine, or Corn Measure, produces the Gallons accordingly. Or if to the \frac{1}{2}d of the Square of the Diameter at the Head, you add \frac{1}{2}ds of the Square of the Diameter in the Middle, and multiply the Product by 9 Inches, 5 Parts, 1 Second, 2 Thirds, which gives the Area of the mean Diameter, if the Dimensions are in Feet and Inches, otherwise if in Cubical Inches by 7854, which also gives the Area of the mean Diameter, and then that Product multiplied by the Height in Inches, gives the solid Content in Cubical Inches, as also the Area of the mean Diameter in Feet, Inches and Parts, multiplied by the Height in Feet, Inches and Parts, which must be multiplied by 12 three times as before, which will bring them into solid Inches, which must be multiplied by 12 three times as before, which will bring them into solid Inches,

as for Example:

Square 3 Foot the Diameter at the Head, which is 9 Foot, one Third of which, is 3 Foot; then square 3 Foot 9 Inches the Diameter in the Middle, which is 14 Foot, 9 Parts, the two Thirds of which is 9 Foot, 4 Inches, 6 Parts, which added to the 3 Foot, the 1d of the Headdiameter, makes 12 Foot, 4 Inches, 6 Parts; this being multiplied by 9 Inches, 5 Parts, 1 Second, 2 Thirds, by the Tables, as I suppose the rest of the Work to be done, will make 9 Foot, 8 Inches, 6 Parts, 4 Seconds, 6 Thirds. This also being multiplied by 4 Foot for the Height, will give 38 Foot, 10 Inches, 1 Part and 6 Seconds, for the folid Contents of the faid Veffel in Feet, Inches and Parts; and to bring it into folid Inches, in order to know the Number of Gallons, you must, as has been said above, multiply the said Sum of 38 Foot, 10 Inches, 1 Part, 6 Seconds, by 12, and the Product 466 Foot, 1 Inch, 6 Parts, by 12 again, which produces 5593 Foot, 6 Inches; this also multiplied by 12 produces 67 122 solid Inches, which being divided by any of the Numbers for the feveral Gallons of Wine, Beer, or dry Measure, as above, will produce the Gallons required very near the Truth, for if it was Beer or Ale Gallons, there would be 238 Gallons, 6 Inches, whereas according to the Truth of the Rule above faid, there would be 238 Gallons, one Pint, 27 Inches and 1, which makes the Difference but a little more than a Pint in fo many Gallons, which small Difference is owing to the want of the minute Parts in the Tables, which is not regarded in other Works; but if any should work this Proposition by the Pen in Vulgar Arithmetick, the Quantity above-mention'd would be exactly true, according to the aforesaid Method, which whether exactly true or not (so much depending upon the Curvature of the Sides) is what I shall not take upon me to determine, it being the same Method as is taught by Sir Jonas Moor, Mr. Oughtred, &c. and is to be sure near enough for common Practice, my Intention being only to explain the Use of the Tables in all forts of Measurements of Superficies and Solids; but if any should think the Difference above-mentioned to be of any Consequence, the Work may be performed by the Tables as near to the Truth as can be defired, much easier than by the Pen, when the Method is understood, which the Pactitioner will soon find by a little Practice; and I have for that Purpose let down the whole Operation several Ways, one by Decimals, one by Vulgar Arithmetick, and the other two by the Tables as follows. First

| First Method Decimally: | By the Pen vulgarly. |
|---|---|
| Diam at the head 3 o or 36 Diam at the bung 3 9 or 45 Height ———————————————————————————————————— | 3)9 0 9 |
| 36. 45. 36. 45. | 3 0 2 3 6 9 |
| 216 180 3)1296. 3)2025: the Sqrs. of the Diam. 675. The \(\frac{1}{3}\)ds. 432. the \(\frac{1}{3}\)d of the Head. 1782. the Sq. of the .7854 mean Diam. | 3)14 0 9 The 2 Thirds of the Sq. 74 8 3 of the Diameter in the 4 8 3 1 Third of the Sq. of the 5 3 0 0 Diameter at Top — 3 2 4 6 0 0 9 5 1 2 2 0 9 0 0 0 1 0 4 6 0 0 9 3 4 6 0 0 |
| 7128 8910 14256 12474 | Aea of the mean of the multip. By the height 4 Foot |
| 1399.5828 the Area of the 48. the height. | 38 10 6 3 9 0 |
| 111966624 55983312 | 466 6 3 9 0 and by 12 three times. |
| 67 17-9744 | 5598 3 9 0 0 12 |
| | 67179 9 1 0 0] |

The Second Way by the Tables.

| | Foo | t I | 1. P | . S. | T | | |
|--|-----|-----|------|------|---|---|---|
| The Square of the mean Diameter — — Multiplied by — — — — | 12 | 4 | 6 | 0 | 0 | | |
| Multiplied by — — — — | _ | 9 | 5 | 1 | 2 | | |
| These distant Parts, as has been mention'd, is not to be found immediately by the Tables, therefore take 12 Foot, 4 Inches, 6 Parts by o Foot, 9 Inches, 3 Parts, which is the nearest in the Tables to o Foot, 9 Inches, 5 Parts, 1 Second, 2 Thirds, and | }, | | • | , | | | |
| which is — — — — — — — — Then for the $\frac{2}{13}$ ths, which is wanting of the Parts, use the same Method as is taught in the 3d Example of Solids, where you will find the Difference for $\frac{1}{13}$ th, to be — | }, | | | | | | |
| Therefore that must be twice | -0 | 1 | 0 | 4 | 6 | | |
| Then for the 1 Second set down the same Difference one place lower, thus | }0 | 0 | I | 0 | 4 | 6 | |
| And for the 3ds the same Difference mult | 0 | 0 | 0 | 1 | 0 | 4 | 6 |
| And for the 3ds the same Difference must be set down twice, one Place lower or more to the Right-hand thus | ° | 0 | 0 | 1 | 0 | 4 | 6 |

which produces — 9 8 7 6 11 3 0 for the Area of the mean Diameter, which being multiplied as before by the Height, and then by 12 three times, as in the fecond Example above, will produce 67179 folid Inche, or 238 Gallons, 1 Pint, 27 Inches, 4 of Beer or Ale.

By the Tables as in the Example above.

Prod. 67122 0000 according to what has been faid in the 2d Example of Gauging. These several Numbers of solid Inches being divided by 282, makes as has been faid before, 238 Gallons and 6 Inches, and 238 Gallons, one Pint and 27 Inches 1, which is but little more than one Pint difference, which in fo large a Quantity is as nothing, and what can never be determined nearer by the Methods now in use with the Sliding-Rule, which is at best but Guess-work, when you come to very minute Parts.

EXAMPLE III.

First M. thed Decimally. | By the Few wigarly. | By the Tables as in the Edwample

To find the Number of Loads of Gravel to make a Walk 250 long, 24 Foot 8 Inches broad, and I Foot 3 Inches deep; or, which is the same Thing, to know the Number of Loads of Earth, which must be moved to level a Piece of Ground of the same Dimensions.

Take the half of 24 Foot, 8 Inches, which is 12 Foot, 4 Inches, and look in the Index of the upper Part of Page 26, for 12 Foot, 4 Inches, opposite to which, and under 1 Foot, 3 Inches, is 15 Foot, 3 Inches; that doubled or multiplied by 2 (which may be done in your Mind without any farther Trouble) makes 30 Foot, 10 Inches; then look in the printed Tables for 30 Foot by 250 Foot, and you will find 7500; to which if you add 208 Foot, 4 Inches (which is 250 Foot by 10 Inches, as may be feen at once in the faid Tables) the whole Sum will be 7708 Foot, 4 Inches; which to bring into Loads, must be divided by 27, and then the Quotient will be 100 Load and 8 Foot.

one is corden to see to tend of C L USION.

From what has been faid, I may reasonably conclude, that any the least knowing Person may find out the Use of the Tables, which has been a work of infinite Labour and Care, and I am in great Hopes there is not one Error in the whole Calculation; but if there should appear to be any, the generous Artist will forgive it, since he may be assured it was not designed, and that all the Care that was possible has been taken by the Engraver and Printer, as well as myself, in making them correct.

according to what has been hid in the 2d Harangle of Gazana. 1 6 0 0 1 6 65160 to Their leveral Numbers of folid Inches being divided by a 2, makes as Ivo from fuld before, of Wallots and O laches, and Westlow, one Pun and 27 more than one I int difference, Thefe office form, as his been i determined nearer by the is not to be found immediately ? edit dia olu di wor abodishi Lables, therefore takes to Peor, a live Siding Rule, which is at hift o Paris by o Poor, 9 Inches; 3 Pers, which but Guels-work, when you is the nearly fin the Tables, to or our extraketorior reventante. Inches, glads, affected, a Thinks, and Then for the littles, which is wanting o the Party of the fame Method as is taught in the ad Lample or Solids, where you will find the Differenced or a th, to be - J Therefore that must be twice --- one of 6 Then fir the a Second fee down the fame Difference one place lowery this -- - --And for the three tours of the color of had 1000 0 2 6 be fet down twice, one Place lower or more 1000 to the Right hand thus which produces --- o 8 7 6 11 7 o for the Area of the mean Diameter, which being multiplied as before by the Height, and then by in three times, as in the second Figurale above, will produce (as o tale I cles, or age

Gallons, a First, at Idelices 1 of Bear on Ale.

| F.I.Parts F.I.Parts F. | Parts F.I. Parts | F.I.Parts | I.Parts | F.I.Parts | F.1.Parts | ME I Par | F.I. Parts | three inci | hes. | |
|---|---|--|-------------------------------------|---|--|--|--|--------------------------------------|---|------------------------------------|
| 0.0.0 0.0.0.0 | | 0.1.0 | 20.4 | 0.1.5 | 0.1.3 | 0.2.0 | 6.1.Parts | F.1.Part | 6.1.Parts | F.I.P. |
| 0.1.0. 0.0.0.3.0 0. | 0.0.4.6 0.0.0.6.0 | 9.1.2.0 | | | | | | | | |
| 0.0.0.4.0 0. | 0.0.9.0 0.0.1.1.6 0 | 0.1.5.0 0 | .O.1 20.6 | 0.0.2.3.0 | 0.0,3,0,0 | | | | | |
| 3,000.7.6 | 0.1.1.6 0.0.1.8.3 0. | 0.2.3.0 0. | 0.2.0.0 | 0.0.3.0.0 | 0.0.3.6.0 | 0.0.4.0.0 | 0.0.5.0.0 | 0.0.6.2 | | |
| 30.0.0.11.3 0.0 | 1.9.0 0.0.2.7.6 0. | 0.3.6.0 0. | 0.4.4.6 | 0.530 | 2.0.3.8.3 | 0.0.6.6.0 | 0.0.7.3.0 | 0.0.8.1.6 | 0.0.8.3.0 | 0.0.9. |
| 4.0, 0.0.1.0.0 0.0 | 2.1.6 0.0.3 0.0 0.0 2.1.6 0.0.3 2.3 0.0 2.4.6 0.0.3 6.9 0.0 2.4.6 0.0.3 6.9 0.0 2.7.6 0.0.3 11.3 0.0 | 0.4.0.0 0 | 0.4.8.3 0 0.5.0.0 0 0.5.3.9 0 | 0.5.7.6 | 0.0.7.0.0 | 0.0.7.6.0 | 0.0.3.5.3 | 0.0.8,9.0 | 0.0.10.3.9 | 0.0.10. |
| .5.0, 0.0.1.3.0 0.0 0.0.1.3.0 0.0 5 0.0.1.4.6 0.0 | 2.6.0 0.0.3.9.0 0.0 2.7.6 0.0.3.11.3 0.0 2.9.0 0.0.4.1.6 0.0 | 0.4.9.0 0.0 0.5.0.0 0.0 0.5.3.0 0.0 | 0.3.11.3 0 | 0.7.6.0 | 0.8.3.9 | 0.0.9.0.0 | 0.0.10.1.6 | 0.0.11.3.0 | 0.1.0.4.6 | 0.1.1. |
| 6.0 0.0.1.6.0 0.0. 0.0.1.6.0 0.0. | 2.6.0 0.0.3 9.0 0.0 2.7.0 0.0.3 11.3 0.0 2.9.0 0.0.4 1.6 0.0 2.10.6 0.0.4 3.9 0.0 3.0.0 0.0.4 8.3 0.0 | .5.9.0 0.0 .6.0.0 0.0 | 0.7.6.0 | 0.8.7.6 | 0.0.0.0 | 0.0.11.0.0 | 0.1.0.11.3 | 2.1.1.6 | 0.1.2.5.3 0 | 1.4.6 |
| 10.0.1.8.3 0.0. | 3.4.6 00.4.10.6 0.0 | .6:6.0 0.0 | .8.1.6 0 | 0.0.0.0 | 01146 | .1.0.6.0 | 1.1.2.0.9 0 | 1.3.7.6 | 0.1.5.2.3 | 1.6.0 |
| 2, 0.0.1.10.0 0.0. | 9.0 0.0.3.7.6 0.0 | 7.6.0 0.0 | 9.4.6 0. | 0.10.10.0 | 1.0.8.3 | 1.2.6.0 0 | 1.4.3.9 0 | 1.6.1.6 | 2.1.7.11.3 | 1.9.0 |
| 2 0.0.2.7.0 0.0.4 | 3.0 0.0.6.4.6 0.0. | 8.6.0 0.0. | 10.7.6 0. | 0.0.0.0 | 1.2.5.3 0 | 1.4.6 0 0 | 1.6.6.9 0. | 1.8.7.6 | 0.1-10.8.3 0. | 2.0.0 |
| \$ 0.0.2.4.6 0.0.4 | 9.0 0.0.7.1.6 0.0. | 9.6.0 0.0. | 11.10.6 0.1 | .2.3.0 0. | 1.4.2.3 0. | 16600 | 1.8.9.9 0. | 1.11.1.6 | 2.0.9.0 0. | 2.3.0. 2.3.9. |
| 0.0.2.6.0.0.0.5 0.0.2.6.9 0.0.5 0.0.2.7.6.0.0.5 0.0.2.8.3 0.0.5 | .0.0 0.0.7.6.0 0.0. 1.6 0.0.7.8.3 0.0. 3.0 0.0.7.10.6 0.0. 4.6 0.0.8.0.9 0.0. | 10.0.0 0.1. 10.3.0 0.1. 10.6.0 0.1. | 0.6.0 0.1 | 30.0 0. | 1.5.6.0 0. 1.5.11.3 0: 1.6.4.6 0. | 1.8.0.0 0. | 1.10.6.0 0. 1.11.0.9 0. | 2.1.0.0 0 2.1.7.6 0 | 2.2.9.9 0.1 2.3.6.0 0.1 2.4.2.3 0.1 | 2.5.3. 2.6.0. 2.6.9. |
| 5 00 2 10 6 000 | .6.0 0.0.8.3.0 0.0.1 .7.6 0.0.8.3.3 0.0.1 9.0 0.0.8.7.6 0.0.1 0.6 0.0.8.9.9 0.0.1 | 1.3.0 0.1. | 1.9.0 0.1 2.0.9 0.1 2.4.6 0.1 | 4.1.6 0.1 4.6.0 0.1 4.0.6 0.1 5.3.0 0.1 | 1.7.3.0 0.1 1.7.8.3 0.1 | . 10.0.0.0 | 2.1.3.9 0 | 2.3.6.0 0. | 2.6.3.0 0.2 | 2.7.6. 2.8.3. 2.9.0. |
| 0, 0.0.3.0.0 0.0.6. 0.0.3.0.0 0.0.6. 2, 0.0.3.1.6 0.0.6. | 0.0 0.0.9.0.0 0.1.0 1.6 0.0.9.2.3 0.1.0 3.0 0.0.0.4.6 0.1.0 | 0.0.0 0.1.3 | 2.8.3 0.1 | 6.4 6 0 1 | .0.0.0 0.2 | .0.0.0 0. | 2.2.5.3 0.0 2.3.0.0 0.0 | 2.4.9.0 0. 2.5.4.6 0. | 2.7.7.6 0.2 2.8.3.9. 0.2 2.9.0.0 0.3 | .10.6. |
| 0.0.3.3.0 0.0.0. | 6.0 0.0.9.9.0 0.1.1 7.6 0.0.9.11.3 0.1.1 | 0.0 0.1.3 | .3.0 0.1 | 7.1.6 0.1 | 10.3.9 0.2 | 2.0.0 0.2 | .4.1.6 0.2 .4.8.3 0.2 | 7.3.0 0. 7.10.6 0. | 2.9.8.3 0.3 2.10.4.6 0.3 2.11.0.9 0.3 2.11.9.0 0.3 | .0.9.0 |
| 0.0.3.5.3 0.0.6: | 0.0 0.0.10.3.9 0.1.1 | 9.0 0.1.5 | .2.3 0.1. | 7.10.6 0.1 8.3.0 0.1 8.7.6 0.2 9.0.0 0.2 | 06.0 02 | 3.0.0 0.2 3.6.0 0.2 | 7.6.0 0.2 | 9.1.6 0. | 3.0.5.3 0.3 3.1.1.6 0.3 3.1.9.0 0.3 | 3.9.0 4.6.0 5.3.0 |
| 3 0.0.3.8.3 0.0.4. | 6 0 0 0 0 0 0 | 9.0 0.1.0. | 0.0 0.1 | 0.1,0.0.2. | 1.4.6 0.2. 1.9.9 0.2. | 4.6.0 0.2 5.0.0 0.2 5.6.0 0.2 | .8.0.9 0.2 .8.7.6 0.3 .9.2.3 0.3 | 0.3.0 0.3 | . 3.10.0 0.3. | |
| 4, 0.0.3.9.9 0.0.7. 0.0.3.10.6 0.0.7.3 0.0.3.11.3 0.0.7.3 | | AND RESIDENCE OF THE PARTY OF T | 8.3 0.1.1 | 10.10.0 0.2. 11.3.0 0.2. 11.7.6 0.2. | 2.8.3 0.2 3.1.6 0.2 3.6.9 0.2 | 7.0.0 0.2 7.6.0 0.2 7.6.0 0.2 | 10.3.9 0.3: 10.10.6 0.3: 11.5.3 0.3. | 3.7.0 | .5.7.6 0.3. | 9.0.0 9.9.0 10.6.0 11.3.0 |
| 3 0.0.4.1.6 0.0.8.3 0.0.4.2.3 0.0.8.4 | 0.1.0.2.3 0.1.4. | 9.0 0.1.8. | 3.9 0.2.0 7.6 0.2.0 | 0.0.0 0.4.6 0.9.0 0.2. 0.9.0 0.2. | 4.0.0 0.2. 4.5.3 0.2. 4.500 0.2. 5.3.9 0.2. | 9.0.0 0.3 | 0.0.0 0.3. 0.6.0 0.3. 1.1.0 0.3. 1.8.3 0.3. | 4.0.0 0.3 | .8.0.0 0.4.0 .8.8.3 0.4.0 .9.4.6 0.4.1 | 0.0.0 |
| 3 0.0.4.4.6 0.0.8.9 | 0 0.1.1.3 0 0 1 6 | 0.0.0.1.9.1 5.0 0.1.9.1 | 3.0 0.2.1 0.9 0.2.1 0.6 0.2.2 | .6.0 0.2.6 .10.6 0.2.6 .3.0 0.2.6 | 5.0.0 0.2. 5.2.3 0.2. 5.7.6 0.2 | 10.0.0 0.3. 10.6.0 0.3. | 2.3.0 0.3.1 2.9.9 0.3.1 | 6.6.0 0.3 7.1.6 0.3 7.9.0 0.4 | 11.5.3 0.4.3 | 3.9.0 |
| 0.0.4.6.0 0.0.9.0 0.0.4.6.9 0.0.9.1 0.0.4.7.6 0.0.9.3 1 0.0.4.8.3 0.0.9.4 | 0001166000 | 0.0 0.1.10.0 | 0.0 0.2.3 0.0 0.2.3 0.0 0.2.3 | 0.0 0.2.7 4.0 0.2.7 9.0 0.2.8 | .6.0 0.3.6 .11.3 0.3.6 .4.6 0.3 | 0.0.0 0.3. | 3.11.3 0.3. 4.6.0 0.3.5 5.0.9 0.3.6 5.7.6 0.3.1 | 0.0.0 0.4 | 1.6.0 0.4.6 2.2.3 0.4.6 | .0.0 |
| 0.0.4.9.0 0.0.9.7. | 0.1.2.3.0 0.1.7.0 | 0 0.1.11.9 | 9 02.4 | 60 000 | 0.9 0.3.1 | .6.0 0.3. | 5.2.3 0.3.10 | 0.10.6 0.4. | 3.0.9 0.4.8 4.3.0 0.4.9 | .0.0 |
| 0.0.5.0.0 0.0.0.0.0 0.0.5.0.0 0.0.0.0.0 0.0.5.0.0 0.0.0.0.1 | 0 0.1.2.9.9 0.1.7.9 | .0 0.2.0.8 | 0.2.5. | 0.0 10 9 11 | 00000 | .0.0 0.3.6 .0.0 0.3.6 .0.0 0.3.6 | Charles and I won to the same of | 0.0 0.4. | 5.7.6 0.4.10. | 0.0 |
| 10.0.3.2.3 0.0.10.4. | 6 0.1.3.6.9 0.1.8.9 0.1.3.9.0 0.1.9.0 0.1.3.11.3 0.1.9.3 0.1.4.1.6 0.1.9.6 | 0 10.2.1.11 | 0.2.7. | 9.0 0.2.11. 1.0 0.3.0. 6.0 0.3.0. | 0.5 0.3 5 3.9 0.3 5 9.0 0.3 6 2.3 0.3 6 | 6.0 0.3.10 | 0.4.3. | 10.6 0.4.6 | 0.0.9 0.5.2. | 6.0 3.0 |
| 0.0.5.6.0 0.0.11.0.0 | 0.1.4.6.0 0.1.10.0. | 0 0.2.3.2. | 0.2.8. | 3.0 0.3.1. 7.6 0.3.2. | 5 0 12 2 0 | 6.0 0.4.0 | 9.9 0.4.5. 4.6 0.4.5. 11.3 0.4.6. | 1.6 0.4.1 9.0 0.4.1 4.6 0.4.1 | 0.5.3. 0.5.3. 0.5.4. | 3.0 |
| 0.0.3.9.0 0.0.11.3.0 | 0.1.4.10.6 0.1.10.6. | 0.2.3.9. | 0 2 9 3 | 0.3.3.4 | 0.3.8. | 6.0 0.4.2. 0.0 0.4.2. 6.0 0.4.3. | 0.9 0.4.7. 7.6 0.4.8. 2.3 0.4.8. | 7.6 0.5.1 3.0 0.5.1 0.6 0.5.2 | 2.3 0.5.6. 10.6 0.5.7. 6.9 0.5.8. | 9.0 6.0 |
| 0.0.5.10.6 0.0.11.9.0 | 0.1.5.5.3 0.1.11.3. 0.1.5.7.6 0.1.11.6.0 0.1.5.9.9 0.1.11.9.0 | 0.2.5.0. | 0.2.10.16 0.2.11.3 0.2.11.7 | 0.3.5.6 | 0.3.10. | 6.0 0.4.4. 0.0 0.4.4. 6.0 0.4.5. | 9.0 0.4.9.0 3.9 0.4.10.1 10.6 0.4.10.6 5.3 0.4.11.4 | 0.5.3 0.5.3 0.5.3 0.5.4 | 3.0 0.5.9.6 11.3 0.5.9.6 7.6 0.5.10.6 3.9 0.5.11.3 | 5.0 |
| 0.0.6.2.3 0.1.0.4.6 0.0.6.2.3 | 0.1.6.2.3 0.2.0.3.0 0.1.6.4.6 0.2.0.6.0 0.1.6.6.9 0.2.0.9.0 | 0.2.6.3.6 | 03.0.4 | 0.3.6.5 | 04.0.0 | 0.4.6.0 | 0.5.0.0 | 0.5.6. | 0.0 0.6.0.0 8.3 0.6.0.9 4.6 0.6.1.6 | .0 |
| 0.0.6.4.6 0.0.6.5.3 | 0.1.6.11.3 0.2.1.3.0 0.1.7.1.6 0.2.1.6.0 0.1.7.3.9 0.2.1.0.0 | 0.2.7.6.6 | 0.3.1.10 | 03.8.2 | 0.4.2.6 | 0 0.4.8.3 | 0.5.2.6 | 0 0.5.8. | 0.6.2.3 0.0 0.6.3.0 0.6.3.9 | .0 |
| 0.0.6.6.0 0:1:1.0.0 0.0.6.6.0 0:1:1.1.6 0.0.6.7.6 0:1:1.3.0 0.0.6.8.3 0:1:1.4.6 | 0.1. 7.6.0 0.2.2.0.0 0.1. 748.3 0.2.2.3.0 0.1. 7.0.6 0.2.2.6.0 | 0.2.8.6.0 | 0.3.3.0. | 0 0 3 9 6 . 6 0 3 . 9 . 11 . 9 | 0 0.4.4.0 0 0.4.4.6 0 0.4.5 | 0.4.9.11 | | | | |
| 0.0.6.9.0 0.1.1.6.0 0.0.6.9.9 0.1.1.7.6 0.0.6.10.6 0.1.1.9.0 0.0.6.10.6 0.1.1.1.60 | 0.1.8.3.0 0.2.3.0.0 | 0.2.0.5.3 | 0.3.4.6. | 0 3.10.9. | 0.4.5.6 | 0 0.3.0.0 | 0.5.6.10 | 0.6.0.k 0.6.1.6 0 0.6.2.3 | 0 0.6.0.0 | 0 |
| 0.0.7.0.0 0.1.2.0.0 | 0.1. 9. 0.0 0.2. 3. 0.0 0.1. 9. 0.0 0.2. 4.0.0 0.1. 9. 2. 3 0.2. 4. 3.0 | 0.2.10.0.0 | 03.5.3 | 0.4.0.6 | 0.4.7.6 | 0 0.5.3.0. | 0.5.8.9.4. | 6 0.6.2.11 0 0.6.3.7 6 0.6.4.3 | 9 0.6.11.3. | 0 |
| 0.0.7 0.0 0.1 2.1 0 | 0.1.9.9.0 0.2.5.0.0 | 0.3.0.3.0 | 0.3.7.6.0 | 0.4.2.0.0 | 04.10.0 | 0 0 6 6 3 | | EU. U. 10. | 0 0.7.0.0. 3 0.7.0.g. 6 0.7.1.6. 9 0.7.2,3.6 | |
| 07.3.9 0 1 2.7.6 | 0.1.9.11.3 0.2.5.3.0 0.1.10.1.6 0.2.5.6.0 0.1.10.3.0 0.2.5.9:0 | 0.3.0.0.9 | 0.3.7.0.6 | 0.4.3.2.3 | 0.4.10.6 | 0.5.5.9.0 | 0.6.0.6. | 0.6.8.5. | 0.7.3.0.0 3 0.7.3.9.0 6 0.7.4.6.0 | 7 1 |

| | -from to | vo footsix i | nches by or | PARTY NAMED IN THE PARTY NAMED IN | 网络阿拉拉斯 | THE REPORT OF THE PERSON NAMED IN | IP TO THE | E I Parta | F.I. Parts | F.I.Parts | F.I.Parts | F.I.Parts |
|-----------|---|--|--|--|--|---|---|---|--|---|---|--|
| F.I.Parts | F.I.Parts | F.I.Parts | F.I.Parts | F.I.Parts | F.I Parts | F.I.Parts | ON A | 0.2:0 | 0.2 4 | 0.2 \$ | 0.2.7 | 0.3.0 |
| 2.0.0 | 0.0.7.6.0 | 21200 | 0.1.10.6.0 0.1.10.8.3 | 0.2.6 0.0 0.2.6 3.0 0.2.6 6.0 0.2.6 9.0 | 0.3.1.9.9 | 0.3.0.00 | 0.4.4.6.0 0.4.4.11.3 0.4.5.4.6 0.4.5.9.9 | 0.5.0.0.0 | | 0.6.3.0.0 | 0.6 11.10.6 | 0.7.0.0.0 0.7.7.6.0 0.7.8.3.0 |
| 2.7.0 | 0.0.7.9.0 | 0.1.3.6.0 0.1.3.7.6 0.1.3.9.0 0.1.3.10.6 | 0.1.11.3.0 | 0.2.7.0.0 | 0.3.3.0.0 | 0.3.10.0.0 0.3.10.10.0 0.3.11.3.0 0.3.11.7.0 | 0.4.6.8.3 0.4.7.1.6 0.4.7.6.9 | 0.3.2.6.0 | 0.5.10.3.0 0.5.10.10.0 0.5.11.5.3 | 0.6.7.4.6 | 0.7.2.7.6 | 0.7.10.6.0 |
| 2.0.0 | 0.0.7.113 | 0.1.4.0.0 | 0.1.11.9.9 0.2.0.0.0 0.2.0.2.3 0.2.0.4.6 0.2.0.6.9 | 0.2.8.0.0 0.2.8.3.0 0.2.8.6.0 0.2.8.9.0 | 0.3.4.0.0 | 0.4.0.0.0 0.4.0.4.0 0.4.0.9.0 0.4.1.1.0 | 0.4.8.0.6 0.4.8.5.3 0.4.8.0.6 0.4.9.3.9 | 0.5.4.0.0 | 0.6.0.0.0 0.6.0.6.0 0.6.1:1.6 0.6.1:8.3 | 0.6.8.7.6 | 0.7.4.0.0 | 0.8.0.0.0 0.8.0:9.0 0.8.1.6.0 0.8.2.3.0 |
| 2.9.0 | 0.0.8.2.3 0.0.8.3.0 0.0.8.3.9 0.0.8.4.0 0.0.8.5.3 | | 0.2:0.9.0 | 0.2.9.0.0 | 0.3.5.3.0 | 0.4.1.6.0 0.4.1.10.0 0.4.2.3.0 0.4.2.7.0 | 0.4.10.7.6 0.4.10.7.6 0.4.11.0.9 | 0.5.6.6.0 | 0.6.3.11.3 | 0.6.11.1.6 0.6.11.1.6 0.6.11.9.0 0.7.1.0.0 | 0.7.7.5.3 0.7.8.1.6 0.7.8.9.9 | 0.8.3.0.0 0.8.4.6.0 0.8.5.3.0 |
| 2.10.0 | | 0.1.5.0.0 | 0.2.1.0.0 | 0.2.10.0.0 | 0.3.6.9.9 | 0.4.3.4.6 0.4.3.9.0 0.4.4.1.6 | 0.4 11.0.0 0.4.11.11.3 0.5.0.4.6 0.5.0.9.9 | 0.5.8.0.0 0.5.8.6.0 0.5.9.0.0 0.5.9.6.0 | 0.6.5.0.9 0.6.5.7.6 0.6.6.2.3 | 0.7.1.7.6 | 0.7.10.2.3 | 0.8.6.9.0 0.8.7.6.0 0.8.8.3.0 |
| 2.11.0 | 0.0.8.9.0 | | 10.2.2.3.0 | 0.2.11.0.0 | 0.3.7.9.0 | 0.4.4.0.0 | 0.5.1.3.0 0.5.1.8.3 0.5.2.1.6 0.5.2.6.9 | 0.3.11.6.0 | 0.6.8.5.3 | 0.7.3.6.0 0.7.4.1.6 0.7.4.9.0 0.7.5.4.6 | 0.8, 2.3.9 | 0.0.11.3.0 |
| 3.0.0 | 0.0.0.1.0 | 0.1.6.0.0 | 0.2.3.0.0 | 0.3.00.0 | 0.3.9.7.6 | 0.4.6.0.0 | 0.5.3.0.0 | 0.6.0.6.0 | 0.6.9.0.0 | 0.7.6.7.6 | | 0.9.0.9.0 |
| 3.1.0 | 0.0.9.2.3 | 0.1.6.9.0 | 0.2.3.11.3 | 0.3.1.3.0 | 0.3.10 3 0 | 0.4.7.6.0 0.4.7.0.0 0.4.8.3.0 0.4.8.7.0 | 0.5.4.9.0 | 0.6.2.0.0 | 0.6.11.9.9 | 0.7.9.9.0 0.7.10.4.6 | 0.6.5.9.6 | 0.9.5.3.0 |
| 3.2.0, | 0.0.9.5.3 | 0.1.7.0.0 | 0.2.4.0.0 | 1 | 0.4.0. | 0.4.9.0.0 | 0.5.6.6.0 0.5.6.11.3 0.5.7.4.6 0.5.7.9.9 | 0.6.4.6.0 | 0.7.1.0.0 | 0.7.11.0.0 0.7.11.7.6 0.8.0.3.0 0.6.0.10.6 | 0.8.9.10. | 0.9.6.9.0 0.9.7.6.0 0.9.8.3.0 |
| 313.0 | 0.0.9.83 | | 0.2.5.3.0 | 0.3.3.3.0.0 | 0.4.0.9.0 | 0.4.10.6:0 | 06830 | 0 6 .6 .0 .0 | 0.7.3.9.0 | 0.8.2.1.6 | 0,8.11.3.0 0.8.11.11. 0.9.0.7.1 0.9.1.3. | 0.9.9.9.0.0 0.9.9.9.0.6.0 0.9.11.3.0 |
| 3.4.0 | 0.0.9.11.3 | 0.1.8.0.0 | 0.2.5.9.9 0.2.6.0.0 0.2.6.2.3 0.2.6.4.6 | 0.3.4.0.0 | 0.4.2.3.6 | 0.5.0.4.0 | 05.10.00 | 06.8.0.0 | 0.7,6.0,0 0.7,6.0,9 0.7,7.1,6 0.7,7.8,3 | 0.8.4.0.0 | 0.9.2.0. 0.9.2.8. 0.9.3.4. 0.9.4.0. | 0.10.0.0.0 0.10.0.9.0 0.10.1.6.0 0.10.2.3.0 |
| 3.5.0 | 0.0.10.7.3 | 0.1.8.6.0 | 0.2.6.0.6 | | | | 0.5.11.9.6 0.6.0.2.3 0.6.0.7.6 | 0 6 10.0.0 0 6 10.6.0 0 6 11.0.0 0 6 11.6.0 | 0.7.8.3.0 0.7.8.9.9 0.7.9.4.6 0.7.9.11.3 | 0.6.7.1.6 | 0.9.4.9.0.9.5.5. | 0.10.3.0.0 0.10.4.6.0 0.10.5.3.0 |
| 3.6.0 | 0.0.10.6.0 | 0.1.9.0.4 | | | | 0.5.3.4 | 0.6.1.11.5 | 07.0.6.0 | 0.7.11.0.9 | 0.8.0.7.0 | 0.9.8.10. | 9 0.10.8.3.0 |
| 3.7.0 | 0.0.10.9.0 | 0.1.9.6.4 | 0.2.8 3.6 | 0.3.7.0 | 0.4.5.9.0 | 0.5.4.6. | 0.6.3.3.0 | 0.7.2.0.0 0.7.2.6.0 0.7.3.0.0 0.7.3.6.0 | 0.8.0.9.0 | 0,8.11.6.0 | 0.9.10.3. | 0 0.10.9.0.0 3 0.10.9.0.0 6 0.10.10.0.0 9 0.10.11.3.0 |
| 3.6.0 | 0.0.11.0.0 | 0.1.9.10.0 | 0.2.8.9 | 9 0.3.7.9.0 | 0.4.0.0. | 2 0 5 6 0. | 0100.5.00 | 0 0.7.4.0.0 0 0.7.4.6.0 0 0.7.5,0.0 0 0.7.5.6.0 | 0.8.3.0.0 | 0.9.2.0.4 | 21218 | 2 0 11.0.0.0 |
| 3.9.0 | 0.0.11.3.6 | 0.1.10.4. | 0.2.9.9. | 0 03.90. | 0.4.8.3. | 0.5.7.0. | 0.6.7.2. | 0 0,7.6.0.0 3 0.7.6.6.0 6 0.7.7.0.0 9 0.7.7.6.0 | 0.8.5.9.9 | 0.9.5.1.6 | 0.10.4.5 | |
| 3.10.0 | 0.0.11.5. | 0 0.1.11.0. | 0 0.2.10.3. 0 0.2.10.6. 6 0.2.10.8. | 0 0.3.10.0. | 0 0.4.9.6. | 0.5.9.0 | 0 0.6.8.6. | 0 0,7.8.0.0 | 0.8.7.6.0 | | 0.10.0.0. | 0.11.7.6.0 |
| 3.11.0 | 0.0.11.9 | 3 0.1.11.4. | 0 0.2.11.0. 0 0.2.11.3. 0 0.2.11.5. | 0 0.3.11.0. | 0 0.4.10.9. | 0.5.10.0. | 0.6.11.1. | 0 0.7.10.0.0 | 100000 | 100060 | 0 10 0.3 | 3 0.11.9.9.0 6 0.11.10.0.0 |
| 4.0.0 | 0.1.0.0. | 3 0.1.11.10. 0 0.2.0.0. 9 0.2.0.1. 6 0.2.0.3. | 0 0.3.0.0. 0 0.3.0.0. 0 0.3.0.2. | 0 0.4.0.0. | 0 0.5.0.0. | 0 0.6.0.0. | 0 0.7.0.0 6 0.7.0.5 0 0.7.0.10 | 0.8.0.0.0 | 0.9.0.0.0 | 0.10.0.0. | 0.11.0.0 | 0 1.0.0.0.0 3 1.0.0.9.0 6 1.0.1.5.0 9 1.0.2.3.0 |
| 4.1.0, | 0.1.0.2. | 0 0.2.0.6. | 0.3.0.0. | 0 0.4.1.0. | 0 0.5.1.3. | 0 0.6.1.6 | 0 0.7.1.9 6 0.7.2.2 0 0.7.2.7 | 0 0.8.2.0. | 0.0.2.3. | 0.10.2.6. | 0.11.2.9 | .0 1.0.3.0.0 3 1.0.3.0.0 6 1.0.4.0.0 9 1.0.5.3.0 |
| 4.2.0 | 4 0.1.0.5. | 3 0.2.0.10. | 0 0.3.1.3. | 9 0.4 .1 .9 | 0 0.5.2.6 | 0.0.6.3.0 | | A . | 2 0 0 4 6. | 0 0.10.5.0. | 0.11.6.10 | 6 1.0.7.00 |
| 4.3.0 | 0.1.0.9 | 0 0.2.1.6 | 0.3.2.3 0.3.2.5 0 0.3.2.7 | .0 0.4.3.0 .3 0.4.3.3 .6 0.4.3.6 | 0 0.5.3.9 | 0 0.0.4.6 | 0 0.7 5.3 6 0.7 5.8 0 0.7 6.1 6 0.7 6.6 | 0 0.8.6.0 3 0.8.6.6.6.6.6.6. | 0 0 0 0 0 9 . 7 . 3 . 9 . 0 . 0 . 9 . 7 . 10 . 0 . 9 . 8 . 5 . | 0.10.7.0. | 0.11.8.11 | 0 1.0.9.00 3 1.0.9.00 6 1.0.10.00 9 1.0.11.30 |
| 4.4.0 | 0.1 .1.0 0.1 .1.0 0.1 .1.0 | 0 0.2.2.0. | 0 0.3.3.0 6 0.3.3.2 | .0 0.4.4.0 .3 0.4.4.3 .6 0.4.4.6 | 0 0.5.5.0 | 0 0.6.6.0 | .0 0.7.7.0 .6 0.7.7.5 .0 0.7.7.10 | 0.8.8.0 | 0 0,9,9.0. | | 6 0.11.11.8 | 0 1.1.0.00 3 1.1.0.00 6 1.1.1.00 9 1.1.2.31 |
| 4.5.0 | 0.1.1.2 | .3 0.2.2.4 ,0 0.2.2.6 .9 0.2.2.7 6 0.2.2.9 | 0 0.3.3.11 | .6 0.4.5.6 | 0 0.5.6.3 0 0.5.6.6 0 0.5.6.0 | .0 0.6 .7.6 .0 0.6 .7.6 .6 0.6 .8 .3 | 0 0.7.8.9 | 0.8.11.0. | 0 0 10.0 .4 | 3 0.11.2.4. | 0 1.0.1.9 0 1.0.2.5 0 1.0.3.1 0 1.0.3.9 | 3 1.1.3.0 6 1.1.4.0 9 1.1.5.3 |
| 4.6.0 | 0.1.1.6 | .3 0.2.2.10 .0 0.2.3.0 .9 0.2.3.1 .6 0.2.3.3 | 0 0.3.4.6 | 0.4 6 3 | 0.5.7.0 | .6 0.6.9.4 | 0.7.10.11 | 3 09.0.6 | 0 0.10.2.0. | 9 0.11.3.7. 6 0.11.4.3. 3 0.11.4.10. | 0 1.0.5.4 | 0.6 1.1.7.60 |
| 4.7.0 | 0.1.1.8 | 0.2.3.7 | 0.3.5.5 | 3 04.7.3 | 0.5.9.4 | .6 0.6.10.16 .6 0.6.11.3 | 0.8.0.8 | 09.2.6 | 0 0.10.4.3 | 9 0.11.6.1. 6 0.11.6.9. 3 0.11.7.4. | 0 1.0.8. | 9 1.1.10.0 |
| 4.8.0 | 0,1, 2,0 | 0 0.2.4.0 | 0.3.6.0 | 0.4.8.3 | 0.5.10.0 | 0.7.0.9 | 0.8.2.5 | 3 09 4 0 | 0 0.10.6.6. | 0.11.8.7. 6 0.11.9.3. 0.11.9.10 | 6 1.0.10.1 | 1.2.1.6 |
| 4.9.0 | 0.1.2.3 | .0 0.2.4.4 .0 0.2.4.6 .9 0.2.4.7 | 0.3.6. | 0.4.9. | 0.5.11.6 | 0 0.7.1.4 | 0 0 0 8 4 7 | 3 09 6.6 | 0 0 10 8 9 | 0.11.11.0 | 6 1.1.2. | 1.2.4 |
| 4.10.0 | 0.1.2.5 0.1.2.6 0.1.2.6 0.1.2.7 | 0.2.4.16 0.0.2.5.0 0.2.5.1 0.0.2.5.3 | 0.0 0.3.7.6 6 0.3.7.6 0.0 0.3.7.6 | 0.0 0.4.10.1 0.0 0.4.10.1 0.0 0.4.10.1 | 0.0 0.6.0.6 3.0 0.6.0.6 5.0 0.6.1.1 | 0 0.7.3.6 | 0.0 0.8.5.6 | 9 0.9.7.6 9 0.9.8.0 1.3 0.9.8.6 1.0 0.9.9.0 1.0 0.9.9.0 1.0 0.9.9.0 1.0 0.9.9.0 | 0 0 10 10 6 | 0 1 0.1.0 9 1.0.1.7 .6 1.0.2.3 .3 1.0.2.10 | 0 1.1.3.6 0 1.1.4.6 0 1.1.4.6 1.1.5.6 | 1.2.6.8 1.2.6.8 1.2.7.6 1.2.7.6 1.2.8.3 |
| 4.11.0 | 0.1.2.9 0.1.2.9 0.1.2.1 | 0.2.5.0 | 0.3.8. 0.0 0.3.8. 0.0 0.3.8. 0.0 0.3.8. 0.0 0.3.8. | 3.0 0.4.11.0 5.3 0.4.11. 7.6 0.4.11.1 | 0.0 0.6.1.9 3.0 0.6.2.0 6.0 0.6.2.4 9.0 0.6.2.4 | 0.0 0.7.4.6 | 0.8.7.3 0.6 0.8.7.6 0.8.8.1 0.8.8.1 | 3.0 0.9.10.0 3.3 0.9.10.0 1.6 0.9.11.0 5.9 0.9.11.0 | 0 011 0.9 | 0 1.0.3.6 | 0 1.1.6. | 1.2.9.1 1.2.9.1 7.6 1.2.10 1.3 1.2.10 |
| لينا ا | 4 0.1.2.1 | 1.340.2.5.10 | , U W. 3. 0.3 | W III | | | | | | | | |

5.7.

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6.

| | Gyrm. f | A five fact by | TAB one quarte | r of an inc | h to sever | n foot five u | nenes and | i un ee yu | arters by | three inch | es . | |
|---|--|--|---|--|---|---|--|---|---|--|--|---|
| Parts | P.I.Parts | F.I.Parts | | F.I.Parts | F.I.Parts | F. I. Parts | F. L.Parts | F.I.Parts | F. 1. Parts | F.1.Parts | F. I. Parts | F. I. Parts |
| .Palls | 0.0.7 | 0.0.2 | 0.0.3 | 0.1.0 | 0.6.3.0.0 | 0.1.2 | 0.1.3 | 0.10.0.0.0 | 011300 | 1.0.6.0.0 | 1.1.9.0.0 | 1.3.0.0.0 |
| 5.0.0 | 01.3.0.0 | 0.2.6.0.0 | 0.3.9.0.0 0.3.9.4.6 0.3.9.6.9 | 0.3.0.3.0 | 0.6.3.3.9 | 0.7.6.9.0 | 0.8.9.5.3 | 0.10.1.6.0 | 0.11.3.6.0 0.11.4.1.6 0.11.4.8.3 | 1.0.7.10.6 | 1.1.11.0.9 | 1.3.2.3.0 |
| 5.1.0 | 01339 01339 01353 | | | 0.5.1.0.0 | 0.6.4.3.0 0.6.4.6.9 0.6.4.10.6 0.6.5.2.3 | 0.7.7.6.0 0.7.7.10.6 0.7.8.3.0 0.7.8.7.6 | 0.8.10 9.0 0.8.11.2.3 0.8.11.7.0 0.9.0.0.9 | 0.10.2.6.0 0.10.2.6.0 0.10.3.0.0 0.10.3.6.0 | 0.11.5.3.0 0.11.5.9.9 0.11.6.4.6 0.11.6.11.3 | 1.0.9.1.6 | 1.2.1.1.6 | 1.3.3.0.0 1.3.3.9.0 1.3.4.6.0 1.3.5.3.0 |
| 5, 2.0 | 0.1.3.5.3 | | 0.3.10.0.0 | 0.5.2.0.0 | 0.6.5.6.0 | 102000 | | 0.10.4.0.0 | 0.11.7.6.0 0.11.8.0.9 0.11.8.7.6 | 1.0.11.0.0 1.0.11.7.6 1.1.0.3.0 1.1.0.10.6 | 1.2.2.6.0 1.2.3.2.3 1.2.3.10.6 1.2.4.6.9 | 1.3.6.9.0 1.3.7.6.0 1.3.8.3.0 |
| T. S. | 0.1.3.6.9 | 0.2.7.4.6 | 0.3.11.0.9 | 0.5.2.9.0 | 0.0.0.5.3 | 0.7.10.1.6 | 0.9.1.9.9 | 0.10.5.0.0 | 0.11.9.2.3 0.11.9.9.0 0.11.10.3.9 0.11.10.10.6 | | 1.2.5.11.3 | 1.3.9.0.0 |
| 5,3.0 | 01390 | | | | 0.6.7.0.9 0.6.7.4.6 0.6.7.8.3 | 0.7.11.7.6 | 0.9.2.8.3.0.9.3.6.9 | 0.10.7.0.0 | 1.0.0.0.0 | 1.1.4.0.0 | 1.2.7.3.9 | 1.4.0.0.0 |
| 5. 4.0 | 0.1.4.0.0 | 0.2.8.0.0 | 0.4.0.0.0 | 0.5.4.3.0 | | 0.8.0.4.6 | 0.9.4.0.0 0.9.4.5.3 0.9.4.0.6 0.9.5.3.9 | 0.10.8.6.0 | 1.0.0.6.9 | 1.1.5.3.0 | 1.2.10.0.9 | 1.4.2.3.0 |
| 5.5.0 | 0.1.4.3.9 | 0.2.8.7.6 | 7 11 0.4.0.11.2 | 0.5.5.0.0 | 0.6.9.3.0 0.6.9.0.6 0.6.9.0.6 0.6.10.2.3 | 0.8.1.0.0 | 0.9.5.9.0 | 0.10.10.0.0.0 0.10.10.6.0 0.10.11.0.0 0.10.11.6.0 | 1.0.3.4.0 | 1.1.0.4.0 | 1.3.0.9.9 | 1.4.0.00 |
| 5.6.0 | 0.1.4.2.0 | | 0.4.1.3.9 0.4.1.6.0 0.4.1.8.3 0.4.1.8.3 | | 0.6.10.6.0 | 0.8.3.0.0 0.8.3.4.0 6 0.8.3.9.1 3 0.8.4.1 | 0.0.7.6.6 0.9.7.11. 0.9.8.4.6 0.9.8.9. | | 1.0.5.7. | 5 1.1.10.3.6 | 1.3.1.6.0 1.3.2.2.3 1.3.2.10.0 1.3.3.6.9 | 1.4.6.9.0 |
| 5.7.0 | 0.1.4.6.9 | 0.2.9.6 | 6 0.4.2.00 | 0.5.0.9.0 | - | 0 0.8.4.6. | 0 0.9.9.3 6 0.9.9.8 0 0.9.10.1 6 0.9.10.6 | | 1.0.6.9. | | 0 1.3.4.3.0 | 1.4.9.9.0 1.4.9.9.0 1.4.10.6.0 1.4.11.3.0 |
| 300 | 0.1.4.9.5 0.1.4.9.5 0.1.4.10.6 | 7 0.2.9 | 0110.4.2.9 | 9 10.2.1.2.0 | 0.7.0.8. | 0.8.5.7. | | 0 0.11.4.0.0 | 1.0.9.0 | 3 1.2.1.4. 0 1.2.2.0. 9 1.2.2.7. | 6 1.3.7.8 | 1.5.0.0.0 |
| 5.8.0 | 0.1.5.0.0 0.1.5.0.0 0.1.5.1.0 0.1.5.2.0 | 6 0.2.10.3 | 6 0.4.3.2. 0 0.4.3.4 6 0.4.3.6. | 0.5.8.0.0 0.5.8.3.0 0.5.8.0.0 0.5.8.0.0 | 0.7.1.3. 0.7.1.7. 0.7.1.11. | 3 6.0.1. | 0 1000 | 0.11.5.0. | 0 1.0.10.8. | The state of the s | 0 1.3.9.0. | 9 1.5.2.3.0 |
| 5.9.0 | - | | 0 0.4.3.9. | 0.5.9.0.0 | 0.7.2.6. | 0.8.7.6. 0.8.7.10. 6 0.8.8.3. 3 0.8.8.7. | 0 0.10.1.2. | 6 0.11.7.0. | 0 1.1.0.11 | 3 1.2.6.4. | 0 1.3.9.9. 0 1.3.10.5. 0 1.3.11.1 6 1.3.11.9. | 0 1.5.6.0.0 |
| 5.10.0 | 0.1. 5.6. | 0 0.2.11.0. | 0 0.4.4.6. | 3 0.5.10.3.6 | 0 73.9 | 9 0.8.9.4 | 0.10.2.6 | 0 0.11.8.0. 3 0.11.8.6. 6 0.11.9.0. 9 0.11.9.6. | 0 1.1.2.0 0 1.1.2.7 0 1.1.3 2 | 9 1.2.7.7. 1.2.8.3. 1.2.8.10. | 6 1.4.1.2. 0 1.4.1.10. 6 1.4.2.6. | 3 1.5.6.9.0 6 1.5.7.6.0 9 1.5.8.3.0 |
| 5,11,0 | 01 6.0 | 0 0.2.11.6 | 0 0,4.5.0 | 9 0.5.109. | 0.7.4.9. | | 0.10.4.3 | 0 0.11.10.0. | 0 1.1.3.9 | 9 1.2.10.1 | 0 1.4.3.3. 6 1.4.3.11. 0 1.4.4.7. 6 1.4.5.3. | 0 1.5.9.0.0 3 1.5.9.9.0 6 1.5.10.6.0 0 1.5.11.3.0 |
| 5.11.0 | \$ 0.1.5.10. 3 0.1.5.11. | 3 0.2.11.10 | 6 0.4.5.9. | 3 0.5.11.3. 0.5.11.6. 9 0.5.11.9. 0 0.6.0.0 | 0 0.7.6.0 | 6 0.8.11.3 0.8.11.7 0 0.9.0.0 0 0.9.0.4 | 0.10.6.0 | 0 1.0.0.0. | | 2 2 2 2 2 | 2 1.4.6.0. | 0 1.6.0.0.0 3 1.6.0.9.0 6 1.6.1.6.0 |
| 6.0.0 | 0.1.6.0. 2 0.1.6.1. 3 0.1.6.2. | 9 0.3.0.1 6 0.3.0.3 3 0.3.0.4 | 0.4.6.0. 0.4.6.2. 0.4.6.4. 0.4.6.4. 0.4.6.6. | 3 0.6.0.3. 6 0.6.0.6. 9 0.6.0.9. | 0.7.6.0 0.7.6.3 0.7.6.7 0.7.6.11 | | 0.10.7.3 | 0 1.0.1.0. | 0 1.1.8.3 | .9 | 6 1.4.8.0. 0 1.4.8.9 6 1.4.9.5 | 0 1.6.3.0.0 |
| 6.1.0 | 0.1.6.3 0.1.6.3 0.1.6.4 0.1.6.5 | 0 0.3.0.0 | 0 0.4.6.9 .6 0.4.6.11 0 0.4.7.1 0 0.4.7.3 | 3 0.6.1.3. 0.6.1.6. 9 0.6.1.9. | 0 0.7.7.3 0 0.7.7.6 0 0.7.7.6 0 0.7.8.2 | 0.9.2.3 | 0.10.8.7 | 9 1.0.3.6 | .0 1.1.9.11 | .3 1.3.4.7 | 0 1.4.10.1 .6 1.4.10.9 | 9 1.6.5.3.0 |
| 6.2.0 | | 0 0.3 1.0 | 0.4.7.6 0.4.7.8 0.4.7.8 0.4.7.0 0.4.8.0 | 0.6.2.0. 0.6.2.3. 0.6.2.6. 0.6.2.6. | 0 0.7.8.6 0 0.7.8.9 0 0.7.9.1 0 0.7.9.5 | 0.9.3.0 0.9.3.4 6 0.9.3.9 5.3 0.9.4 | 0.0 0.10.9.0 0.0 0.10.9.1 0.0 0.10.10.4 1.6 0.10.10.9 | 1.3 1.0.4.6 | 0 1.1.11.0 | .9 .3.6.3 .3.6.4 | 6 1.5.0.2 0 1.5.0.10 0 1.5.1.6 | |
| 6.3.0 | 0.1.6.8 | 3 0.3.1.6 .0 0.3.1.6 .0 0.3.1.6 .0 0.3.1.6 | 5.0 0.4.8.3 1.6 0.4.8.3 5.0 0.4.8.3 0.0 0.4.8.7 0.0 0.4.8.9 | | 0 0.7.9.9 | 0.0 0.9.4.6 0.0 0.9.4.6 4.6 0.9.5.3 8.3 0.9.5. | 6.0 0.10.11.3 0.6 0.10.11.3 3.0 0.11.0 | 1.6 1.0.7.0 | 0 1.2.1.1 | 2.6 1.3.8.9 1.3.9.4 | 1.6.2.3 1.6 1.5.2.11 1.0 1.5.3.7 1.6 1.5.4.3 | .6 1.6.10.6.0 .9 1.6.11.3.0 |
| 6.4.0 | 0 0170 | 10221 | 0 0.4.0.0 | 0 0.6.4.0 3 0.6.4.3 6 0.6.4.6 | 0 0.7.11.0 | 2.0 0.0.6.6 | 0.0 0.11.1. 0.0 0.11.1. 0.0 0.11.1. 0.0 0.11.1. | 0.0 1.0.8.0 | 1.0 1.2.3.0 5.0 1.2.3.0 1.0 1.2.4 | 5.9 1.3.10.0 6.9 1.3.10.1 | 1.5.5.8 | 1.7.0.0.0 1.3 1.7.0.0.0 1.6 1.7.1.6.0 1.9 1.7.2.3.0 |
| | 3 0.1.7.2 | 3 0.3.2. | 0.4.9.0 0.4.9.2 0.4.9.4 0.4.9.6 | | 0 0.7.11.1 | 1.3 0.9.1 | 7.0 | 3.9 1.0.9.0 | 5.0 1.2.5. | 3.0 1.4.0. | 5.0 1.5.7.9 1.6 1.5.8.3 7.0 1.5.9.1 | 7.0 1.7.3.0.0 5.3 1.7.3.0.0 1.6 1.7.4.6.0 |
| 0.5. | \$ 0.1.7.3 0.1.7.3 0.1.7.3 | 3.0 0.3.2.0 3.0 0.3.2.0 1.6 0.3.2.0 5.3 0.3.2.1 | 6.0 0.4.9.9 7.6 0.4.9.1 9.0 0.4.10.1 0.6 0.4.10. | 0.0.5.9 | .0 0.0.1. | 2.3 0.9.0. | 7.0 0.11.4. | 6.0 1.1.0.0 | 2 0 1 2 0 | 1.3 11 1.4.2. | 1.6. 1.5. 1.5. 1.5. 1.5. 1.5. 1.5. 1.5. | 9.9 1.7.2.2.0 |
| 6.6. | 0.1.7.6 0.1.7.6 2 0.1.7.6 3 0.1.7.6 | 0 0.3.3. 0 0.3.3. 0 0.3.3. 1 3 0.3.3. | 0.4.10.6 0.4.10.6 3.0 0.4.10.6 4.6 0.4.11.0 | 0.6.6.6 | 0 0.8.2. | 9.9.0.9.9 5.3 0.9.10. | 4.6 0.11.4. 9.0 0.11.5. 1.6 0.11.5. | 4.6 1.1.1.6 | 2 2 1.2 0. | 0.0 1.4.5. | 6 0 1.6.1. | 3.0 1.7.9.0.0 |
| 6.7. | | | 6.0 0.4 II. 7.6 0.4 II. 9.0 0.4 II. | 3.0 0.6.7.0 5.3 0.6.7.3 7.6 0.6.7.6 | .0 0.8.2. .0 0.8.3. .0 0.8.3. .0 0.8.3. | 9.0 0.9.10. 0.9 0.9.10. 4.6 0.9.11. 8.3 0.9.11. | 3.0 0.11.7. | 8.3 1.1.2.1 1.6 1.1.3.0 | 6.0 1.2.10. 0.0 1.2.10. 6.0 1.2.11. | 3.9 1.4.6. 10.6 1.4.6. 5.3 1.4.7. | 1.6 1.6.1.1 9.0 1.6.2. 4.6 1.6.3. | 7.6 1.7.10.6.0 3.9 1.7.11.3.0 0.0 1.8.0.0.0 |
| 6.8. | 4. 0.1.7.1 | | 10.6 0.4 11.5 0.0 0.5.0. 1.6 0.5.0. 3.0 0.5.0. 4.6 0.5.0. | 9.9 0.0.7.9 | 0 0 8 4 | | 0.0 0.11.8 4.6 0.11.8 9.0 0.11.8 | 0.0 1.1.4. 5.3 1.1.4. 10.6 1.1.5. | 0.0 1.3.0. 6.0 1.3.0. 0.0 1.3.1. 6.0 1.3.1. | 6.9 1.4.8. 1.6 1.4.9. 8.3 1.4.9. | 0.0 7.6 1.6.4. 3.0 1.6.5. 1.6.5. | 8.3 1.8.0.9.0 |
| 6.9. | 3 0.1.8. | | | 0.0 0.6.9. | 2.0 0.8.5. | 3.0 0.10.1. 3.0 0.10.1. 6.9 0.10.1. 10.6 0.10.2. | .6.0 0.11.9. 10:6 0.11.10 | | 6.0 1.3.2. | 3.0 1. 7.10. | 9.0 1.6.8 | 9.0 1.8.3.0.0 5.3 1.8.3.9.0 1.6 1.8.4.6.0 4.0 1.8.5.3.0 |
| 6.00 | 0.1.8. 2.1.8. 0.1.8. 0.1.8. | 3.3 0.3.4 | 0.0 0.5.1. | 3.9 0.0.9.3 6.0 0.6.10.0 | 0.8.6 | 6.0 0.10.3. | 0,0 0.11.11 | 6.0.0 | 00134 | 6.0 1.5.1. | 0.0 1.6.0. | 6.0 1.8.6.0.0 2.3 1.8.6.9.0 10.6 1.8.7.6.0 6.9 1.8.8.3.0 |
| 6.10 | 3 0.1.8 | 6.9 0.3.5 7.6 0.3.5 8.3 0.3.5 | .1.0 0.3.1. .3.0 0.3.1. .4.6 0.3.2. | 0.010.6.10. | 0.0 0.0.7. | 5.3 0.10.4 | 9. 6 1.0.0 | 3.0 1.1.10. | 6.0 1.3.5. 0.0 1.3.5. 6.0 1.3.6. | 2.3 1.5.2. 9.0 1.5.3. 3.9 1.5.4. | 6 0 1 7 0 | 3.0 1.8.9.0.0 |
| 6,11 | 4 0.1.8 | 9.0 0.3.5 9.9 0.3.5 10.6 0.3.5 11.3 0.3.5 | 7.6 0.5.2 9.0 0.5.2 10.6 0.5.2 | 3.6 0.6 II. 5.3 0.6 II. 9.9 0.6 II. | 3.0 0.8.8 6.0 0.8.8 9.0 0.8.8 | . 6.3 0.10.5 | .0.0 1.0.1. .10.6 1.0.1 .3.0 1.0.2 .7.6 1.0.2 | 0 0 1.2.0. | 0.0 1.3.6 6.0 1.3.7 0.0 1.3.7 6.0 1.3.8 | 10.6 1.5.4. 5.3 1.5.5. 0.0 1.5.6. | 9.0 1.7.1. 4.6 1.7.2. 0.0 1.7.3. | 11.3 1.8.9.9.0 7.6 1.8.10.6.0 3.9 1.9.11.3.0 |
| 7.0 | | 0.0 0.3.0 | .0.0 0.5.3 .1.6 0.5.3 .3.0 0.5.3 .4.6 0.5.3 | .0.0 0.7.0. .2.3 0.7.0. .4.6 0.7.0. | 0.0 0.8.9 3.0 0.8.9 6.0 0.8.9 | .0.0 0.10.6 .3.9 0.10.6 .7.6 0.10.6 | .0.0 1.0.3 .4.6 1.0.3 .9.0 1.0.3 .1.6 1.0.4 | 10.6 1.2.1. 3.9 1.2.1. | 6.0 1.3.10 | 1.6. 1.5.7. 8.3 1.5.7. | 3.0 1.7.4. 10.6 1.7.5 | 0.0 1.9.0.0.2 8.3 1.9.0.9.6 4.6 1.9.1.6.6 0.9 1.9.2.3.6 |
| Section 1 | 0.1.9 | 3.0 0.3.6 | .4.6 0.5.3 6.0 0.5.3 7.6 0.5.3 6.9.0 0.5.4 6.10.6 0.5.4 | | | | 10.6 1.0.5 | 9.0 1.2.2 2.3 1.2.2 7.6 1.2.3 .0.9 1.2.3 | 0.0 11.7.11 | .11.3 1.3.10 | .4.0 | .g.o 1.g.3.o.6 .5.3 1.g.3.g.6 .1.6 1.g.4.6.6 .g.g 1.g.5.3.6 |
| | 20.1.9 | 6.0 0.3. | 9.9.0 0.5.4 9.10.6 0.3.4 1.0.0 0.5.4 | 3.9 0.7.1. | 9.0 0.8JI 0.0 0.8.H | | | | 0.0 7.4.1 | 0.0 1.5.11 | | .6.0 1.9.6.0.0 .2.3 1.9.6.9.1 .19.6 1.9.7.6.1 |
| | 4, 0.1.9 0, 0.1.9 0, 0.1.9 0, 1.9 | 6 0 0.3 6 9 0.3 7.6 0.3 8.3 0.3 | 7.0.0 0.5.4 7.1.6 0.5.4 7.3.0 0.5.4 7.4.6 0.5.5 | .0.9 0.1.2 | 0.0 0.9.0 | 7.1.6 0.10.6 7.5.3 0.10.1 | 0.1.6 1.0. | 1.9.9 1.2.5 1.3.0 1.2.6 1.0.3 1.2.6 1.1.6 1.2.7 1.6.9 1.2.7 | 0.011.4.3 | 9.0 1.6.1 | .6.0 1.7.10 .1.6 1.7.11 .1.6 1.7.11 | 1.3.0 1.9.9.0. |
| 7.3 | 3.0. 0.1.9 4. 0.1.9 2. 0.1.9 2. 0.1.9 | 9.0 0.3. 19.9 0.3. 10.6 0.3. 11.3 0.3. | 7.6 0 a. 5.5 7.7.6 0.5.5 7.9 0 0.5.5 7.10.6 0.5.5 | 3.3 0.7.3 .7.6 0.7.3 .9.9 0.7.3 | 3.0 0.9.1 6.0 0.9.1 9.0 0.9.1 | 1.8.3 0.10.1 | 0.6.0 1.0.8 0.10.6 1.0.8 11.3.0 1.0.8 11.7.6 1.0.8 | 7.1.6 1.2.7 7.6.9 1.2.7 0.0.0 1.2.8 | .0.0 1.4.5 | 5.5.3 1.6.3 | 1.0.0 1.8.1 | .3.0 1.0.11.3. .0.0 1.10.0.0. .8.3 1.10.0.9. 3.4.6 1.10.1.6. |
| 7. | 4.0.1.10 | 0.0.0 0.3. | 8.0.0 0.5.0 8.1.6 0.3.0 8.3.0 0.3.0 8.4.6 0.3.0 | 7.6 0.7.3 9.9 0.7.3 0.0 0.7.4 2.3 0.7.4 4.6 0.7.4 5.6.0 0.7.4 | 3.0 0.9. | 2.3.9 0.11.0 | 0.4.6 1.0.1 | 0.6.3 1.2.8 0.10.6 1.2.9 1.3.9 1.2.9 | 0.0 1.4. | 1.6.3 | 5.10.0 1.0.4 | 1.0.9 1.10.2.3 |
| 7.5 | \$ 0.1.1 | 0.2.3 0.3. 0.3.0 0.3. 0.3.0 0.3. 0.4.6 0.3. | 8 6.0 0.3.0 8 7.6 0.3.0 8 9.0 0.3.0 8 10.6 p.3. | 7.1.6 0.7.5 7.3.9 0.7.5 7.3.9 0.7.5 | .0.0 0.9. 3.0 0.9. | 3.3.0 0.11. 3.6.0 0.11. 3.10.6 0.11. | 1.6.0 1.0.1 1.10.6 1.1.0 2.3.0 1.1.1 | 1.0.0 0.2.3 0.7.6 1.2.1 1.0.9 | 0.0.0 1.4.1 0.6.0 1.4.1 10.0 1.4.1 1.6.0 1.4.1 | 9.9.9 1.6. | 5.6.0 1.8.5 7.1.6 1.8.5 7.9.0 1.8.6 9.4.6 1.8.6 | 1.9.0 1.10.3.0 5.5.3 1.10.3.9 6.1.6 1.10.4.6 6.9.0 1.10.5.3 |
| | 5 0.1.1 | 0.5.3 0.3. | 3.10.6 p.3. | 7.3.9 0.7.5 | 9.0 0.9. | 7.42 | | | | | | |

| | fromse | ven foot si | cinches b | y one qua | rter of an o | nch, to nu | re foot ele | ven inche | & three que | arters by b | rree inches | |
|-------|--|--|--|--|---|--|--|--|--|--|---|---|
| F.I. | P. F.I.Parts | F.I.Parts | F.I.Parts | F.I.Parts | F.I.Parts | F.I.Parts | F.I.Parts | F.I.Parts | F.I.Parts | F.I.Parts | F.I.Parts | F.I.Par |
| 7.6 | 0.1.10.6.0 | 03900 | 0.3.7.6.0 | 0.7.6.0.0 | 0.9.4.6.0 | 0.11.3.0.0 0.11.3.4.6 0.11.3.9.0 0.11.4.1.6 | | 13.0.6.0 | 1.4.11.0.9 | 16.9.0.0 16.9.7.6 16.0.3.0 16.10.10.6 | 1.8.7.0.0 1.8.8.2.3 1.8.8.0.6 1.6.9.6.9 | 1.10.6.0 1.10.6.0 1.10.7.5 1.10.8.3 |
| 7.3 | 0.1.10.9.0 0.1.10.9.9 0.1.10306 0.1.11.11.3 | 0.3.9.7.6 | 03.8.3.0 | 0.7.7.0.0 0.7.7.3.0 0.7.7.6.0 0.7.7.9.0 | 0.9.5.9.0 0.9.6.0.9 0.9.6.4.6 0.9.6.8.3 | 0.11.5.3.0 | | | 1,5.0.9.0 | 1.7.0 1.6.0 | 1.8.10.3.0 1.8.10.11.3 1.8.11.7.6 1.9.9.3.9 | 1.10.9.0 1.10.0.9 1.10.10.6 1.10.11.3 |
| 7.8 | 0.1.11.0.0 0.1.11.0.0 0.1.11.1.6 0.1.11.2.3 | 0.3.10.0.0 0.3.10.1.6 0.3.10.3.0 0.3.10.4.6 | 0.5.9.0.0 0.5.9.2.3 0.5.9.4.6 0.5.9.6.9 | 0.7.8.0.0 0.7.8.3.0 0.7.8.6.0 0.7.8.9.0 | 0.9.7.0.0 0.9.7.7.6 0.9.7.1.3 | 0.11.7.1.0 | 1.1.5.10.6 | 112600 | 1.5.3.6.9 1.5.4.1.6 1.5.4.8.3 | 1.7.2.7.6 1.7.3.3.0 1.7.3.10.6 | 1.9.2.4.6 | 1.11.0.0 1.11.0.0 1.11.1.0 1.11.2.3 |
| 7.3 | 0.1.11.3.0 0.1.11.3.0 0.1.11.4.6 0.1.11.5.3 | 0.3.10.7.6 | 0.5.10.1.6 | 0.7.9.0.0 0.7.9.3.0 0.7.9.6.0 0.7.9.9.0 | 0.9.8.3.0 | DIS. TRUMPHONESHARING CONTROL OF THE PARTY O | 1.1.6.0.0 | 13.6.6.0 | 1. 5. 7. 6.0 | The second second second second second | 19.5.1.6 | 7.11.3.44 1.11.4.64 1.11.5.3, |
| 7.11 | 8 0.1.11.6.9 8 0.1.11.7.6 3 0.1.11.8.3 | 0.3.11.1.6 | 0.5.10.8.3 | 0.7.10.3.0 | 0.9.9.9.9.0 | 0.11.9.4.6 0.11.9.9.0 0.11.10.1.6 | 1.1.8.11.3 | 1.3.8.6.0 1.3.9.0.0 1.3.9.6.0 | 1.5.8.0.9 1.5.8.7.6 1.5.9.2.3 | 1.7.7.7.6 1.7.8.3.0 1.7.8.10.6 7.7.9.6.0 | 1.9.7.2.3 | 1.11.7.6. 1.11.7.6. 1.11.8.3. |
| 8.0 | | 0.3.11.7.0 0.3.11.9.0 0.3.11.10.0 | 0.5.11.9.9 | 0.7.11.6.0 | 0.9.11.4.0 | 0.11.11.3.0 | 1.1.11.6.9 | 1.4.0.0.0 | 1.5.10.50.6 1.5.11.5.3 1.6.0.0.0 | 1.7.10.9.0 1.7.11.4.6 1.8.0.0.0 1.8.0.7.6 | 1.9.10.7.0 1.9.11.3.9 | 1.11.9.9.1 1.11.10.6.1 1.11.11.3.1 |
| 8.1 | | 0.4.0.3.0 0.4.0.4.6 0.4.0.6.0 0.4.0.7.6 | 0.6.0.4.6 | 0.8.0.6.0 | 0.10.0.7.6 | 1.0.1.1.6 | 1.2.1.3.9 | 1.4.1.6.0 | 1.6.1.8.3 | 1.8.1.3.0 | 1.10.1.4.6 1.10.2.0.9 1:10.2.9.0 1:10.3.5.3 | 2.0.1.6.1 2.0.2.3.4 2.0.3.0.0 2.0.3.0.0 |
| 8.2 | 0.2.0.6.0 | 0.4.0.0.6 | 0.6.1.3.9 | 0.8.1.0.0 | 0.10.2.2.3 | 1.0.2.7.6 | 1.2.3.0.9 1.2.3.6.0 1.2.3.11.3 | 1.4.4.0.0 | 1.6.4.6.0 | 1.8.3.9.0 1.8.4.4.6 1.8.5.0.0 1.8.5.7.6 | 1.10.4.1.0 1.10.4.9.9 1.10.5.6.0 1.10.6.2.3 | 2.0.6.0.0 2.0.6.0.0 2.0.6.0.0 2.0.6.0.0 2.0.7.6.0 |
| 8.3 | 0.2.0.9.9 | 0.4.1.6.0 | 0.6.2.3.0. | 0.8.2.9.0 | 010300 | 1.0.4.6.0 | 1.2.4.9.9 | 1.43.6.0 | 1.6.6.9.0 | 1.8.7.6.0 | 1.10.8.3.0 | 2.0.9.0.0 2.0.9.0.0 2.0.9.0.0 2.0.0.6.0 |
| 8.4 | 0.2.0.11.3 | 0.4.1.10.6 0.4.2.0.0 0.4.2.1.6 0.4.2.3.0 | 0.6.2.9.9 0.6.3.0.0 0.6.3.2.3 0.6.3.4.6 | 0.8.3.9.0 0.8.4.0,0 0.8.4.3.0 0.8.4.6.0 | 0.10.5.0.0 0.10.5.3.9 0.10.5.7.6 | 1.0.5.7.6 1.0.6.0.0 1.0.6.4.6 1.0.6.9.0 1.0.7.1.6 | 1.2.7.0.0 | 1.4.8.0.0 | 1.6.9.6.9 | 1.8.9.4.6 1.8.10.0.0 1.8.10.7.6 1.8.11.3.0 1.8.11.10.6 | 1.10:10.3.0 1.10.11.0.0 1.10.11.8.3 1.11.0.4.6 | 2.1.0.0.0 2.1.0.0.0 2.1.0.0.0 |
| 8.5 | 0.2.1.3.0 | 0.4.2.7.6 | 0.6.3.9.0 | 0.8.5.0.0 | 0.10.6.3.0 | 1.0.7.6.0 | 1.2.8.9.0 1.2.9.2.3 1.2.0.7.6 | 1. 4.10.0.0 1. 4.10.6.0 1. 4.11.0.0 | 1.6.11.3.0 1.6.11.9.9 1.7.04.6 1.7.0.11.3 | 1:9.0.6.0 | | 2.1.3.0.0 2.1.3.0.0 2.1.4.6.0 2.1.5.3.0 |
| 8.6 | | and the second section of the second section s | | 0 8.6.0.0 0 8.6.3.0 0 8.6.6.0 0 8.6.9.0 | 0.10.7.6.0 0.10.7.9.3 0.10.8.1.6 0.10.6.3.3 | | The second secon | CONTRACTOR OF THE PERSON NAMED IN COLUMN 2 | The second secon | 1.9.3.0.0 | 1.11.3.10.6 | 2.1.6.0.0 2.1.6.9.0 2.1.7.6.0 2.1.8.3.0 |
| 8.7 | 0.2.1.0.6 | 0.4.3.10.6 | 0.6.3.9.9 | 2.8.7.9.0 | 0.10.9.8.3 | 1.0.11.7.6 | 1.3.1.6.9 | 1.5.3.6.0 | 1.7.5.5.3 | 1.9.7.4.6 | 1.11.7.3.0 1.11.7.11.3 1.11.8.7.6 1.11.9.3.9 | |
| 8.8 | 0.2.2.0.9 | 0.4.4.0.0 0.4.4.1.6 0.4.4.3.0 0.4.4.4.6 | 0.6.6.2.3 | 0.8.8.6.0 0.8.5.9.0 | 0.10.10.3.9 0.10.10.7.6 0.10.10.11.3 | 1.1.0.4.6 | 1.3.2.5.3 | 1.5.4.6.0 | 1.7.7.8.3 | 1.9.8.7.6 | 2.0.0.0.0 | 2.2.0.0.0 2.2.0.0.0 2.2.1.6.0 2.2.2.3.0 |
| 8.10 | 0.2.2.3.9 | 0.4.4.6.0 0.4.4.7.6 0.4.4.0.6 0.4.4.0.6 | 0.6.6.11.3 0.6.7.1.6 0.6.7.3.9 | 0.8.9.3.0 0.8.9.6.0 0.8.9.9.0 | 0.10.11.6.9 0.10.11.10.6 0.11.0.2.3 | 1.1.2.3.0 | 1.3.4.2.3 1.3.4.7.6 1.3.3.0.9 | 13.6.6.0 13.7.0.0 15.7.6.0 | 1.7.8.9.9 1.7.9.4.6 1.7.9.11.3 | 1.9.11.1.6 1.9.11.9.0 1.10.0:4.6 1.10.1.0.0 | 2.0.1.5.3 2.0.2.1.6 2.0.2.9.9 2.0.3.6.0 | 2.2.3.9.0 2.2.4.0.0 2.2.5.3.0 2.2.6.0.0 |
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| 11.11.000 211.00 0.511.60 0.8.11.3.0 0.11.11.3.0 1.2.100.0 1.5.1010.0 1.8.108.3 1.11.106.0 22.10.3.0 2.5.1010.0 28.10.7.0 1.2.10.7.0 1.2.11.00 1.5.10.10.0 1.8.10.10.0 1.11.10.0 1.2.10.10.0 1.5.10.0 1.5.10.0 1.5.10.0 1.5.10.0 1.5.10.0 1.5.10.0 1.5.10.0 1.5.10.0 1.5.10.0 1.5.10.0 1.5.10.0 1.5.10.0 1.5.10.0 1.5.10.0 1.5.10.0 1.5.10.0 1.5.10.0 1.5.10.0 1.5. | 0 2111000 |
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| 4 | 0.3.1.11.9 | 0.0.3.10.0 | 0.9.6.0.0 | 1.0.7.9.0 | 1.3.9.0.3 | 1.0.11.7.0 | 1.10.1.0.9 | 2.1.3.0.0 | 2.455.3 | 2././.4.0 | 2.10.9.3.9 | 3.1.11.3.0 |
| 12.9.0 | 0.3.2.2.3 | 0.6.4.6.0 | 0.06.00 | 1.0.9.0.0 | 1.3.11.9.0 | 1:7.1.0.0 | 1.10.3.0.0 | 2.1.0.0.0 | 2.40.3.9 | 2.7.0.0.0 | 2.11.0.90 | 3 . 4.3.0.0 |
| 李金星 | 0.3.2.3.9 0.3.2.4.6 0.3.2.5.3 | 0.6.4.7.6 | 0.9.6.113 | 1.0.9.9.0 | 1.4.0.2.3 | 1.7.27.6 | 1.10.5.0.9 | 2.1.7.6.0 | 2.49.113 | 2.8.0.4.6 | 2.11.2.1.6 | 3.2,5.3.0 |
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| 13.11.0 | 03290 03299 032106 | 0.6.5.0.0 | 0 98 53 | 1.0.110.0 | 1.4200 | 1.7460 | 1.107 30 | 2.1.100.0 | 2.50.0.0 | 2 8 4 9 0 | 2.116 30 | 3. 29.0.0 3. 29.0.0 3. 20.6.0 |
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| 13.1.20 | 0.3.3.3.00 | 0.0.0.0.0 | 0.9959 | 1.1.1.0.0 | 1.4311.3 | 77.00 | 1.10.10.3.9. | 2.21.0.0 2.220.0 2.226.0 2.23.00 | 2 5 5 3 0 2 5 5 3 0 2 5 5 9 9 2 5 6 4 6 | 287160 | 2.11.11.0.0 3.0.0.5.3 3.0.1.1.6 3.0.1.9.9 | 3.3.3.0.0 |
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| 13.3.2 | 03.3.7.6 | 0.6.7.3.0 | 0.9.11.0.9 | 1.1.2.9.0 | 1.4.653 | 1.7.10.1.6 | 1.11.1.9.9 | 2.2.5.6.0 | 25923 | 2.9.0.10.6 | 30469 | 3 3 8 3 0 |
| 4 | 0.3.3. W.3 | 0.0.7.10.0 | 0.9.11.3.0 | 1.1.3.9.0 | 1.4.7.0.3 | | | 2 28.00 | 2.6.0.0.0 | 2.0400 | 3.0.5.3.0 3.0.5.113 3.0.67.6 3.0.7.39 | 3.40.0.0 |
| 3 | 03409 | 0.0.83.0 | 0.10.0.2.3 | 1.1.4.3.0 | 1 4 8 3 9 | 1.80.0.0 | 1.11.5.3.9 | 2.2.9.6.0 | 2.6.1.83 | 29.5.10.6 | | 3.4.2.3.0 |
| 13.5.0 | 03 4 3 0 03 4 3 9 03 4 4 6 03 4 3 3 | 03.86.0 03.87.6 03.89.0 03.810.6 | 0.10.0.0.0 0.10.0.11.3 0.10.1.1.6 0.10.1.3.9 | 1.1.5.0.0 | 1.49.3.0 | 1.8.1.0.6 | | | | | 3 0 10 9 0 3 0 11 5 3 3 1 0 1 6 3 1 0 9 9 | |
| 3.6.8 | 03.4.6.0 | 0.6.9.3.0 | | 1.1.6.0.0 | 1 4 106 0 | 1.83.4.6 | 1117.60 | 2.3.0.0.0 | 2.6.4.6.0 2.6.5.0.0 2.6.5.7.6 | 29900 | 3.1.1.6.0 | 3.4.6.0.0 3.4.6.9.0 3.4.7.6.0 |
| | 03.4.9.0 | 0.6.9.6.0 0.6.9.7.6 0.6.9.9.0 | | 117.0.0 | 1.4.11.9.0 | 1.8.4.6.0 | 1.11.9.3.0 | 2.3.2.0.0 | 2.6.6.9.0 | 2.9.11.6.0 | 3.1.4.3.0 | 3.4.9.0.0 |
| 1 14 110 | 0.3.4.10.0 | 0.6.9.0.0 | 0.102.7.0 0.102.9.0 0.103.0.0 0.103.2.3 0.103.4.0 0.103.6.9 | 1.1.8.0.0 | 1.5.1.0.0 | 1.8.5.7.6 | 1.11.10.6.9 | 2.3.4.0.0 2.3.4.6.0 | 269.00 | 2.101.4.6 | 317.00 | 3.5.0.0.0 |
| 13.9.8 | 03.5.2.3 | 0.6.10.4.6 | 0.103.4.0 | 1.1.8.9.0 | 1.5.1.11.3 | 1.8.7.6.0 | 20.0.3.9 | 2.3.5.0.0 | 2.6.10.8.3 | 2.10.3.70.6 | 3.1.9.9.0 | 3.5.2.3.0 |
| 34 | 03.5.4.6 | 0.6.10.10.6 | 0.103.0.0 0.10311.3 0.1041.6 0.1043.9 | 1.1.9.9.0 | 1.5.3.2.3. | 1.8.8.3.0 | 2.0.1.7.6 | 2.3.7.6.0 | 2.7.0.4.6 | 2.10.5.9.0 | 3.1.11.1.6 | 3.5.4.6.0 |
| 13.10.0 | 03.5.6.9 | 0.6.11.1.6 | 0.10.4.6.0 0.10.4.8.3 0.10.410.6 0.10:5.0:9 | 1.1.103.0 | 5.3.9.9 | 189.46 | 2.0.2.11.3 2.0.3.46 2.0.3.9.9 | 2.3.9.0.0 2.3.9.6.0 2.3.9.6.0 | 27.2.7.6 | 2.107.7.0 | 321106 | 3 5 0 9 0 |
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| 14.0.8 | 03.6.0.0 | 07.000 | 0.106.0.0 0.106.2.3 0.106.4.6 0.106.6.9 | 1.2.0.0.0 | 1.5.6.0.0 | 1.90.0.0 | 2.0.6.0.0 2.0.6.5.3 2.0.6.10.6 | 24.00.0 | 27600 | 2.11.0.0.0 | 3.2.6.9.0 | 3.6.0.0.0 |
| 14.1.8 | 0.3.6.3.0 | 0.7.0.6.0 | 0.106.9.0 | 1.2.1.0.0 | 1.5.73.0 | 1.9.1.6.0 | 2.0.7.9.0 | 2.4.2.0.0 | 2.7.8.3.0 | 2.11.2.6.0 2.11.3.1.6 2.11.3.9.0 | 3 2 8 9 0 | 3.6.3.0.0 |
| 14.2.0 | 03.6.6.0 | 0.7.1.0.0 | 0.107.3.9 | 1.2.2.0.0 | 1.5.8.6.0 | 1.9.3.0.0 | 2.0.9.6.0 | 2.43.6.0 | 2.7.9.113. | 2.11.5.0.0 | 3.2.109.9 | 3.6.6.0.0 |
| 14.3.2 | 03.6.8.3 | 07.1.4.6 | 0.10.8.0.0 | 1.2.2.0.0 | 1.5.9.1.6 | 1.9.4.6.0 | 2.0.10.4.0 | 2.4.5.6.0 | 2.8.0.2.3 | 2.11.6.10.6 | 3.3.0.0.9 | 3.6.8.3.0. |
| 34 | 03.6.10.6 | 0.7. 1.10.0 | 0.10.8.5.0 | 1.2.39.0 | 1.5.10.8.3 | 1.9.5.7.0 | 27 0.0.9 | 2.4.7.0.0 | 20.2.53 | 2.11.9.4.0 | 3.3.2.1.3. 3.3.2.11.3 3.3.3.7.6 3.3.4.3.9 | 3.0.77.3.0 |
| | | | 0.10.9.0.0 0.10.9.2.3 0.10.9.4.6 0.10.9.6.9 | | | 1.96.0.0 | 2.1.2.3.9 | 2.4.9.0.0 | 2.0.4.0.3 | 2. 11.11.10.0 | 33583 | 3.7.4.3.0 |
| 14.5.2 | 03730 | 07276 | 0-10-9-9-0 0-10-9-11-3 0-10-10-1-6 | 1.2.5.0.0 1.2.5.0.0 1.2.5.0.0 | 1.6.0.6.9 | 19760 | 2.1.3.23 2.1.3.7.6 2.1.4.0.9 | 2.4.10.00 | 2.8.5.9.9 2.8.6.4.6 2.8.6.113 | 3.0.0.0.0 | 33790 | 3.7.3.0.0 3.7.3.0.0 3.7.4.0.0 3.7.5.3.0 |
| 14.6.0 | 03760 | 07300 | 0-10106-0 | | 16160 | 1.0.0.0.0 | 2.1.4.11.3 | 2.5.0.0.0 2.5.0.6.0 2.5.1.0.0 | 287.60 28809 28876 28923 | 3.0.3.0.0 | 3.3.10.6.0 | 37600 |
| 14.7.0 | 37.9.0 | 0.7.36.0 | 0.10.11.3.0 | 1.2.7.0.0 | 1.0.2.5.3. | 1.9.10.1.0 | 2.7.5.9.9 | | 2.8.9.9.0 2.8.10.3.9 2.8.10.10.6 | 0.05.60 | 34130 | 379.00 |
| 14.8.0 | 03.7.11.3 | 0.7.4.0.0 | 0.11.0.0.0 | 1.2.7.9.0 | 1.6.4:0.0 | 1.9.11.7.6 1.10.0.0.0 1.10.0.4.6 1.10.0.9.0 | 12.1.8.0.0 | 2.5.4.0.0 | 2.0.0.0.0 | 3.0.8.0.0 | 3.4.40.0 | 3.8.0.0.0 |
| 34 0 | 3.0.2.3 | 7.4.40 | 0.11.0.0.9 | 1.4.0.9.0 | 1.0.4.11.9 | 1.10.1.2.0 | 121939 | 2.5.5.0.0 | | 3.0.0.10.0 | | 3.8.2.3.0 |
| 14:10.0 | 2.2.8.6.0 | 07.40.0 | | 12930 | 0 6 6 6 0 | 1.102.3.0 | 211.11.00 | 25700 | 293113 | 3 0 0 4 0 | 34899 | 38 000 38 300 38 330 38 330 |
| 14.10.0 | 38.00 | 07.53.0 | 0.11.1.10.0 | 1.2.109.0 | | 1.104.1.0 | 2.3.0.2.9 | 2.5.9.0.0 | 29509 | 3.1.2.10.0 | 3 47023 9 410106 3 47160 | SECTION SECTION |
| 14.11.0 | 0.3.8.9.0 | 07576 | 011253 | 121130 | 1 0 8 0 9 | 1.10.4.10.6 | 221.83 | 251000 | 29739 | 3 1 4 9 0 | 3 8 2 3 3 8 | 9 9 10 6 0 |

| | from three Inches by three. | Inches and a Quar | rter to two Foot eig | ht Inches and | hree Quarters by | wir Inches |
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| 0 - 3 - 4 | 0 3 - 4 | 0.3.3 | 0.4.0 | 0.4.4 | 0.4.5 | 0.4.3 | 0.5.0 | 0.5.4 | 0.5.4 | 0.5.34 | 0.6.0 | |
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| 01.99 | 01.4.7.6 | 0.1.3.11.3 | 0.1.5.0.0 | 0.1.6.0.9 | 0.1.8.9.0 | 0.1.10.6.9 | | | | | | |
| 01.500 | 0.1.2.9.0 | 01.78.3 | 0.1.0.0.0 | 0.1.10.3.0 | 0.1.10.0.0 | 0.2.0.11.9 | 0.2.2.9.0 | 0.2.3.6.9 | 0.2.6.3.0 | 0. 2.9.0.9 | | |
| 01.7.6.0 | 0-1-9-0-0 | 0-1-10-6-0 | 0.2.0.0.0 | 0.2.1.6.0 | 0.2.3.0.0 | 0.2.4.6.0 | 0.2.6.0.0 | 0.2.7.6.0 | 0.2.0.0.0 | 0.2.106.0 | 0.3.0.00 | |
| 0.1.10.9.0 | 0.2.0.6.0 | 0.2.2.3.0 | 0.2.4.0.0 | 0.2.5.9.0 | 0.2.7.6.0 | 0.2.9.3.0 | 0.3.0.3.0 | 0.3.0.9.0 0.3.2.0.9 0.3.3.4.6 0.3.48.3 | 0.3.2.0.0 | 0.3.43.0 | 0.3.6.00 | |
| 0.2.1.2.3 0.2.2.0.0 4 0.2.2.9.9 | 0.2.4.0.0 | 0.2.6.0.0 0.2.6.11.3 0.2.7.10.6 | 0.2.8.0.0 | 0.3.0.1.0 | 0.3.0.0.0 | 0.3.2.0.0 | 0.3.2.0.0 | 0.3.0.0.0 | 0.3.6.7.6 0.3.8.0.0 0.3.9.4.6 0.3.10.9.0 | 0.3.10.0.0 | 0.3106.0 | |
| 0.2530 | 0.2.376 | 0.2.9.9.0 | 0.3.0.0.0 | 0.3.1.2.3 0.3.2.3.0 0.3.4.46 | 0.3.3.4.0 | 0.3.5.6.90 | 0-3-7-9-0 | 0.3.11.3.0 | 0.40.1.6.0 | 0.4.3.9.0 | 0.4.6.00 | |
| 0.2783 | 0.2101.6 | 0.3.06.9 | 0.3.3.0.0 | 0.3.5.5.3 | 0.3.8.0.0 | 0.3.11.6.0 | 0 4090 | 0.43.2.3 | 0.4576 | 0.4.8.0.0 | 0.5.0.0.0 | |
| 0.21011.3 | 0.3.00.0 | | 03.50.0 | 0.3.8.7.6 0.3.9.8.3 0.3.10.9.0 0.3.11.9.0 | 0.4.1.6.0 | 0.4.1.106 | 0.4.59.0 | | 0.409.0 | 0.5.0.4.6 | 0.5.4.0.0 | |
| 20222 | 0.3.3.4.6 | 0.3.8.0.0 | 0.3.10.0.0 | 0.4.3.0.0 | 0.4.3.0.0 | 0.4.7.9.9 | 0:50.0.0 | 0. 5.0 -0.0 | 0. 5.6.0.0 | 0.3.6.1.6 | | |
| 03399 | 0.3.6.126 0.3.7.9.0 0.3.8.7.6 | 0.3.911.3 0.3.1010.6 0.3.11.9.9 | 0.43.0.0 | 0.4.6.2.3 | 0.47.1.6 0.48.3.0 0.49.4.6 | 0.411.4.6 | 0.2.2.6.0 | 0 5 6 113 | 0.6.11.6.0 | 0.6.1.3.9 | 0.6.46.0 | |
| 037.00 | 0.3.10.4.6 | 0.4.1.8.3 | 0.4.7.0.0 | 0.4839 0.4946 0.41053 | 0.411.7.6 | 0.5.2.11.3 | 0.5.7.6.0 | 0.5.9.0.9 | 0.0.3.7.0 | 0.6.4.23 | 0.0.10.0.0 | |
| 03960 | | 0 4739 | | 0.3.1.7.6 | 0.5.5.3.0 | 0.3.8.10.0 | 0.0.0.0.0 | 0.6.4.1.6 | 0.6.9.1.6 | 0.6.9.11.3 | 07.30.0 | |
| 04090 | 0446.0 | 0.48.3.0 | 0.5.0.0.0 | 0.5.3.9.0 | 0.5.7.6.0 | 0.5.11.3.0 | 0.6.3.0.0 | 0.6.6.9.0 0.6.9.4.0 0.6.108.3 | 0.6.10.6.0 | 07230 | 076.00 | |
| 0.4.4.0.0 | | | 0.5.4.0.0 | | | | | | | | | |
| 0.47.3.0 | 0.4.11.6.0 | 0.53.9.0 | 0.5.8.0.0 | 0.6.0.3.0 | 0.6.4.6.0 | 0.6.0.11.9 | 0.7.1.0.0 | 0.75.30 | 0.7.9.6.0 | 0.8.1.9.0 | 0.8.6.0.0 | |
| | 0.5.3.0.0 | 0.5.7.6.0 | 0.6.3.0.0 | 0.6 4.6 0 | 0.6.10.1.6 | 0.7.1.6.0 | 0.7.60.0 | 0.7.10.6.0 | 0.8.3.0.0 | 0.8.7.6.0 | 0.9.3.0.0 | |
| 0.5.1.9.0 | 0.5.6.6.0 | 0.511.30 | 0.6.4.0.0 0.6.5.0.0 0.6.6.0.0 0.6.7.0.0 | 0.6.8.9.0 0.6.9.9.9 0.6.10,146 | 0.7.0.40 0.7.1.6.0 0.7.27.6 0.7.3.0.0 | 0.7.5.0.9 0.7.6.3.0 0.7.7.5.3 0.7.8.7.6 | 0.7.11.0.0 | 0.8.3.9.0 0.8.3.0.9 0.8.6.4.6 | 0.8.8.6.0 | 0.9.1.3.0 | 0.9.6.0 0 | |
| 0.5.4.2.3 | 0.59.1.6 | 0.6.3.0.0 | 0.6.7.0.0 0.6.8.0.0 0.6.9.0.0 06.10.0.0 06.11.0.0 | 0.7.1.0.0 | 0.7.60.0 | 0.7.9.9.9 | 0.8.4.0.0 | 0.8. 7.8.3 | 0.9.0.7.6 | 0.9.5.6.9 | 0.0.0.0.0 | |
| 0.5.7.5.3 | 06076 | 0.6.5.0.9 | 0.7.0.0.0 | 07.530 | 0.7.00.0 | 0.8.2.6.9 | 0.8.79.0 | 0.9.2.3.0 | 0.9.81.6 | 0.000.00 | 0.10.6.0.0 | |
| 0.5.108.3 | 0.6.5.0.0 | 0.6.9.6.9 | 0.7.3.0.0 | 0.7.8.53 | 0.8.3.0.0 | 0.8.8.6.0 | 0.9.09.0 | 0.9 6.2.3 | 091176 | 0.10.5.0.0 | 0.11.0.0.0 | |
| 0.6.1.0 | 0.6.7.7.6 | 0.7.0.46 | 0.7.4.0.0 | 0.8.0.8.3 | 0.8.5.3.0 | 0.9.1.3.0 | 0.9.46.0 | 0.9.10.1.6 | 0.10.3.9.0 | 0.10.10.9.9 | 0.11.4.6.0. 0.11.4.6.0. 0.11.7.6.0 | |
| 0.03.23 | 0.011.1.0 | 0.7.4.1.6 | 0.7.11.0.0 | 0.8.3.10.6 | 0.8.10.10.6 | 09.3.7.6 | 0.9.9.6.0 | 0.10.5.0.0 | 0.10.9.9.0 | 0.11.3.1.6 | 0.11.0.0.0 0.11.7.6.0 0.11.9.0.0 0.11.10.6.0 | |
| 06.6.00 | 0.7.0.10.0 | 0.7.2.10.6 | 0.8.0.0.0 | 0.8.7.0.9 | 0.9.23.0 | 0.9.8.4.6 | 0.10.3.9.0 | 0107.39 | 0.11.4.1.6 | 0.11.10.3.9 | 1.0.3.00 | |
| 0.69.30 | 0./20.1.0 | 0.0.0.0 | 0.8.4.0.0 0.8.5.0.0 0.8.6.0.0 0.8.7.0.0 | 0.9.1.3.3 | 9.7.0.0 | 0.10.2.3 | 0,00,00 | 0.00 | | | AND ALCOHOLDS | * |
| 0.70.6.0 | 77.00 | 0.8.25.3 | 0.8.8.0.0 0.8.0.0.0 0.8.10.0.0 | 0.9.3.6.9 | 0.9.0.0 | 0.10.7.0.9 | 0.10.10.6.0 | 0.11.5.0.9 | 1.0.0.4.6 | 1.0.6.11.3 | 1.1.6.0 | |
| 0.73.90 | 0.7.106.0 | 08.43.0 | 0.9.0.0 | 0.9.0.9.0 | 010100 | 0.10.8.3.0 0.10.9.53 0.10.10.7.0 0.1011.9.9 | 0.11.2.0.0 | 0.11.9.9.0 | 0.5.10.6 | 101130 | 11000 | |
| 0.7.7.0.0 | 0.8 2.00 0.8 2.00 0.8 3.9.0 | 0.8.9.0.0 | 09400 | 0.10.0.0.0 | 0.10-6.0.0 | 0.11.2.2.3 0.11.2.2.3 0.11.4.6.0 | 011.8.0.0 | 103.00 | 1.0.10.0.0 | 11500 | 1.2.0.0.0 | |
| 0.7403.0 0.711.09 0.711.09 0.8.08.3 | 8546 | 0.9.0.9.0 | 0.0.0.0 | 010430 | 0.10106.0 | 0.11.5.0.0 | 1.0.1.0.0 | 1.0.8.3.0 | 1.3.0.0 | 1.10.90 | 1.25.00 | |
| 08160 | 0 9 0 0 0 | 9460 | 0.10.0 0 0 | 0.107.6.0 | 0.11.3.0.0 | 0.11.10.6.0. | 1.00.00 | 11160 | 1.10.4.0 | 1.2.4.6.0 | 1.2 0 0.0 | |
| 0.89.43 | 0.0.0.0 | 0.0.8.9.0 | 0.103.00 | 0.10.10.8.3 | 11.6.46 | 1.0.2.0.9 | 1.0900 | 1 8 9 9 | 2.2.0.0 | 1.2.103 0 | 1.3.4.0.0 | |
| 0.88 0.0 | W. DEWYEND V. | 9933 | 0.10.7 0.0 0.10.8 0.0 0.10.9 0.0 0.10.10.0 0.0 | 0.11.2.11.3.0 | 0.0.0.0 | 0.699 | 1.1.40.0 | 1.100.3 | 9 8 0 0 | 13.2.6.9 | 1.4.0.0.0 | |
| 0.8405.3 | 3336 | 10.1.10.6 | 0.10.11.0.0 | 11.7.23 | 0.3.46 | 0.11.6.9 | 1.17.9.0 | 1.2.3.11.5 | 3.04.6 | 1.9.8.9.0 | 14.60 | |
| | and the same | | Jan Jan | | | • | | | | | | |

A TABLE OF FEET AND INCHES
from two Foot nine Inches by three Inches and a Quarter to five Foot two Inches and a Quarter by six Inches

1.P

5.6.

7

5.9.

5.10.

6. C.

6.2.

6.6.0

6.3.

6.10.0

5.11.0

.0.0

7.1.0

. 2 . 0

.3.0

1.4.0

.5.0

.6.9

.7.0

. 3. 0

| | | 000 000 20 | or non 1 | nenes by | arree in | ches and | a Quari | ter to five | Foot by | Inches o | ind s qua | vicer by such |
|----|---------|--|---|--|--------------------------|--------------|-------------|--------------------------------|-----------------|-------------------------------------|--|--|
| | E.I.Par | F.I. Bart | F.I.Part | F.I.Parts | F.I.Parts | F.I.Parts | F.I.Part | FI. Parts | FI Parts | FI.Parts | KI Parts | F.I.Parts E |
| - | | 0.3.4 | A CONTRACTOR | | 0.4.0 | | 高大学的 | 0.4.4 | 0.5.0 | 四次田田の下の日本田田の田田 日本日 | 0.5.4 | 0.5.30 |
| | 2.9.9 | 0.90000 | 0.0840 | 0.10.890 | 0.11.1.0.0 | 0.11.9.3.9 | 1.0.57 | 21.1.3.1.0 | 11030 | 1. 0.7 40.6 | 1.3.4.3.0 | 1.3.11.2.3 |
| - | 2.10.5 | 0.9.26.0 | 0.9.11.0.0 | 0.107.6.0 | 0.11400 | 1.0.0.0.0 | 1.0900 | 11.500 | 1.2.2.2.0 | 1.2.9.2.3 | 1.3.7.0.0 | 1.4.3.6.0 |
| | 3 | Cutic | 10.0. | P. 12003 | 0.000 | | 1. 1. 0 40 | 1. 1. 9.0.9 | 1.25.9.0 | 1.3.2.5.3 | | 1.4.5.4.8 |
| | 2.11:0 | 09590 | 0.10.20 0 | 0.1011.3.0 | 0.11,8.0.0 | 1.0.49.0 | 1.1.27.6 | 1.1.10.3.0 | 1.27.0.0 | 13.39.0 | 1.4.0.0.0 | 14.0.83 |
| | | | | | | | | | | | 1.4.4.7.6 | 1.5.1.69 |
| | 3.0.0 | 0 9 0 9 0 | 0.10.6.10.6 | 0.11.3.11.3 | 1.0.1.0.0 | 1.0.10.0.9 | 1.1.7.1.6 | 2.4.23 | 13130 | 31039 | 47.46 | 1.5.4.5.3 1.6 |
| | 3.1.9 | 0.0.03.0 | 0.10.8.7.0 | 0.11.6.9.0 | 1.0.4.0.0 | 1.1.3.0 | 1.1.10.0.0 | 12790 | 1.3.50.0 | 4230 | 1.4.11.6.0 | 1.5.8.9.0 1.6 |
| | 1 | 0.10.1.10.6 | 0.10.11.3.0 | 0.11.6.9.0 0.11.7.8.3 0.11.8.7.6 0.11.9.6.9 | 1.0.0.0.0 | 1.1.4.53 | 1.20.9.0 | 1.211.3.9 | 37.60 | 44.06 | 5.2.3.0 | 1.5.17.6 1.6 |
| | 3.2.8 | 0.10.3.6.0 | 0.11.1.0.0 | 0.11.10.6.0 | 1.0.8.0.0 | 1.5.6.0 | 1.23.00 | 1.3.0.6.0 | 13.1000 | 1.4.7.6.0 | 1.5.5.0.0 | 1.63.113 |
| | 3.3 · g | 0.10.5.11.3 | 0.11.3.7.6 | 1.0.1.39 | 1.0.11.0.0 | 1.1.8.8.3 | 1.2.6.4.6 | 13.4.0.0 | 1.4.1.90 | 1.4.11.5.3 | 1.501.6 | 6.6.0.0 |
| - | 7 7 3 | 010.7.60 | 0.11.5.4.6 | 1.0.2.3.0 | 1.1.1.0.0 | 1.1.10.9.9 | 1.2.8.7.6 | 13653 | 4.430 | 153.00 | 16130 | 1.69.83 |
| | 3.4.8 | 0.10.10.0.0 | 0.11.8.0.0 | 1.0.6.0.0 | 1.1.4.0.0 | 1,2.2.0.0 | 13.0.0.0 | 1.3.10.0.0 | 1.48.0.0 | 1.5.6.0.0 | 6.400 | 1.7.2.0.0 1.8. 1.7.3.5.3 1.8. 1.7.4.10.6 1.8. |
| | 74 | 011 0 3.3 | 0.7.07.0 | 1.0.09.9 | 1.7.7.0.0 | | 3.40 | 1.4.1.09 | 1.4.11.0.0 | 1.5.9.163 | 1.0.0.1.0 | 1.7.0.3.01.8. |
| j | 3.5.0 | 011.1.3.0 | 1.0.0.46 | 1.0.0.9.90 | 1.1.8.0.0 | 1.203.0 | 3.4.6.0 | 1.42.0.0 | 15.23.0 | 1. 6.0.6.9 | 1.6.9.6.0 | 1.7.7.9.0 18. |
| - | 3.6.2 | 0.11.3.8.3 | 1.0.3.0.0 | 1.1.0.6.0 | 1.1.11.0.0 | 1.2.10.6.0 | 13.7.10.0 | 1.4.7.6.0 | 1.5.6.0.0 | 1.6.4.60 | 1.7.1.7.6 | 1.8.1.6.0 19 |
| | 五五五 | 0.11.6.11.3 | 1.0.3.10.6 | 1.1.2.5.3 | 1.2.1.0.0 | 1.3.0.7.6 | 1.3.10.1.6 | 1.48.8.3 | 15.7.3.0 | 1.6.7.1.6 | 7.5.00 | 1.8.2.11.31.0 |
| 3 | 3.7.8 | | | 1.1.5.3.0 | | | | | | | | 18.2.3.0 1.0 |
| | 3 | 0.11.0.2.3 | 1.0.9.1.6 | 1.1.8.0.0 | 1.2.7.0.0 | 1.3.4.10.0 | 1.44.10.6 | 1.5.3.0.0 | 1.6.1.0.0 | 17.0.40 | 1.3.0.76 | 8.10.1.6.0 |
| 1 | 44 | 0.11.11.9.9 | 1.0.10.10.6 | 1.1.9.11.3 | 1.2.0.0.0 | 1.3.8.0.9 | 4.7.1.6 | 5023 | 16530 | 7 4 3 9 | 18346 | 9.3.6.0 1.10 |
| 3 | 3.8.8 | 1.0.5.3.0 | 1.1.1.6.0 | 1.2.0.0.0 | 1.3.0.0.0 | 1.3.11.3.0 | 1.4.10.6.0 | 1.5.8.6.9 | 1.6.0.0.0 | 1.7.8.3.0 | 1.8.7.6.0 | .9.6.9.0 1.10 |
| | 34 | 1.0.3.10.6 | 1.1.3.3.0 | 1.2.1.7.6 | 1.3.3.0.0 | 41 4.6 | 1.5.0.9.0 | 1.6.1.3.9 | 1.6.11.6.0 | 1.7.10.100 | 1.8.10.3.0 | 99 76 110 |
| 3 | 10.0 | 1.0.5.6.0 | 1.1.5.0.0 | 1.2.4.6.0 | 1.3.4.0.0 | 43.6.0 | 1.5.3.0.0 | 1.6.2.6.0 | 1.7.3.3.0 | 1.8.1.6.0 | 19.1.0.0 | 1.100.6.0 1.11. |
| = | 34 | | | | | | | | 17.5.90 | 1.8.5.53 | 0516 | 10.4.9.9 1.11 |
| | 五 | 1.09.6.9 | 1.19.4.0 | 1.2.10.00 | 3.0.0.0 | 4.8.9.9 | 5.0.00 | 1.6.7.3.0 | 7.8.3.0 | 8.8.0.9 | 9930 | 107.8.3 |
| 4 | .0.0 | 1.1.0.0.0 | 1.2.0.0.0 | 1.3.0.0.0 | 1.4.0.0.0 | .5.0.0.0 | 0.0.0.0 | 1.7.0.00 | 1.8.0.0.0 | 1.0.0.00 | 1.100.00 | 11.0.0.0 2.0 |
| | 34 | 1.1.2.53 | 1.2.2.7.0 | 1.3.2.9.9 | 1.4.3.0.0 | 5.3.2.3 | .034.0 | 1.7.3.0.9 | | .93:113 | 10 41 6 | 11.4.3.9 20. |
| | 1 | 1.1.4.0.0 | 1.2.4.4.0 | 33.9.0 | 4.5.0.0 | 5.5.3.9 | 0 5 7 6 | 175113 | 1.8.5.0.0 | 9530 | 1.10.5.0.0 | 11.7:23 20 |
| 7 | . 2. 0 | 1.1.6.6.0 | 1.2.7.0.0 | 3.7.6.0 | 4.8.0.0 | 5.8.6.0 | 6.9.0.0 | 7.9.0.0 | 1.8.10.0.0 | 9.10.6.0 | 1.10.11.0.0 | 11.11.6.0 2.1. |
| | 至 | 1.1.8.1.6 | 1.2.8.9.0 | 3.0.3.9 | | 5.11.8.3 | 6.11.3.0 | 1.7.11.10.6 | 9.0.6.0 | 10.1.1.6 | 11.1.9.0 2 | 0.2 4.6 21. |
| 4 | 3.2 | 1.1.9.9.0 | 1.2.106.0 | 40.23 | 5.0.0.0 | 6.0.9.0 | 7.1.6.0 | 1.8.2.3.0 | 9.4.3.0 | 10.3.0.0 | 11.46.02 | 0.5.3.0 21 |
| | 4 0 | 1.2.0.2.3 | 3.2.0.0 | 1.4.2.0.01 | 5.3.0.0 | 0.3.11.3 1 | 7.6.0.0 | 18.70.0 | 9.5.0.0 | 10.7.8.3 | 11.87.62 | 0.9.6.9 2.1.9 |
| | 45 | 12.276 | 3.3.9.0 | 43.113 1 | 5.5.0.0 | 6.6.0.0 | 2830 | 8.8 2.3 | 9.1000 | 10.10.3.0 | 0.0.0.0.2 | 1.0.5.3 2.2. |
| 4 | .5.2 | 1.2.4.3.0 | 3.50.0 | 46.0.01 | 5.8.0.0 1 | 6.9.3.0 | 7.10.6.0 | 8.1000 | 10.1.0.0 | 11.2.3.0 2 | 0.3.6.0 2 | 1.4.9.0 22.0 |
| | 3 | | | 4.9.6.9 | 5.10.0.0 | 7.0.5.3 | 8.1.10.6 | 93.39 | 10.4.9.0 | 11.6.23 | 0.63.02 | 1.9.0.9 2.2.1 |
| 4 | かかって | 1.2.8.3.0 | 3.9.10.0 | 411.53 | 6.2.0.0 | 73691 | 8416 | 9.5.83 | 10.8.6.0 | 11.8.9.9 2 | 0.00.00 2 | 2.1.4.6 233 |
| 4 | 7.0 | 1.2.10.9.0 | 4.0.6.0 | 5.2.3.0 | 6.4.0.0 | 75.9.0 1. | 8.7.6.0 | 9.8.09 | 10.99.0 | 0.0.9.0 2 | 1.1.1.0 2 | 2.4.3.0 23.0 |
| | 34 | 13.0.46 | 43.3.0 | 5.5.0.9 1. | 6.7.0.0 | 7.7.10.0 1. | 8.0.00 | 10.000 | 11.1.6.0 2 | 0.3.4.6 2 | 1.53.0 2 | 2.8.6.9 23.0 |
| 4 | 8.00 | 3299 | 44.00 | 5.0.0.01 | 6.9.0.0 | 7.10.0.0 | 9.1.1.6 | 10.2.0.0 | 11.5.3.0 2 | 0.6.0.0 2 | 1.80.02 | 2.10.0.0 2.40 |
| 4 | 9.8 | TO SECURE A PROPERTY OF THE PARTY OF THE PAR | Andreas and addition the Administration of the Assessment Co. | 5.8.9.9 1. | | | | | | | | 3.23.9 244 |
| | 3 | 3.53.0 | 4.8.46 | \$ 10.03 1 | 7.1.0.0 1. | 8.44.0 | 9.5.7.6 | 10.7.113 | 11.103.0 2 | 1.1.10.6 2 | 2.43.0 2 | 3 3 0 0 2 4 0 3 5 2 3 2 4 7 3 6 7 6 2 4 9 3 8 0 0 2 4 0 |
| 4 | 10.01 | .2.8.6.01 | 411.0.0 1. | 6.2.5.3 | 7.4.0.0 1 | 8.0.0.01. | 9.9.0.0 | 1011.6.0 2 | 02.0.0 2 | 1.4.0.0 2 | 27.00 2 | 310112 2.51 |
| 4 | 3/1 | 3.10.113 | 3.17.01 | 6.4.3.9 1: | 7.7.0.0 1. | 8.9.83 | 10.0.4.6 | 11.0.8.3 2 | 0.5.9.0 2 | 1.8.53 2 | 2.11.1.0 | 1220 250 |
| | 11.00 | 4 2 2 3 | 334.6 | 6809 | 7.00.01. | 9.0.100 | 103.9.0 | 11.5.53 | 0.8.3.0 2 | 2.0.4.02 | 3.1.10.6 2 | 4 3 3 0 2 5 0 4 4 8 3 2 5 7 4 6 7 6 9 2 5 9 4 7 6 9 2 5 9 |
| 5 | 0.81 | 43.0.0 | 5.6.0.0 1. | 6.0.0.01 | 8.00.011. | 0.3. 0.0 11. | 10.0.0.0 | 11.0.00 2 | 1.0.00 2 | 29.00 2 | 3.0.0.0 2. | 4.9.00 2.60 |
| - | 341 | 4 553 | 3.89.6 | 6.11.9.9 | 8.2.0.0 1. 8.3.0.0 1. | 9.5.10 | 10.8.3.0 1 | 11.10.23 2 | 1.3.9.0 2 | 29.00 2 2439 257,62 257,62 | 3.89.0 2. | 61.3.0 2.04 |
| 3 | 李 | 4.7.0.9 1. | 5.104.6 1. | 72 70 | 8.5.0.0 | 9839 | 10.11.7.6 2 | 0.2.113 2 | 1.63.0 2 | 2.9.6.9 2. | 4.0.10.6 2 | \$290 200 \$423 260 \$5,760 260 \$5,760 260 |
| 5. | 2.81 | 4.9.6.0 1. | 6.1.0.01. | 7.4.6.0 1. | 8.8.0.0 | 9.11.6.0 1.1 | 11.3.0.0 2 | 0.0.6.0 2 | 1.10.0.0 2 | 3.1.0.0 2. | A make the second secon | COLUMN TOWNS OF THE PARTY OF TH |
| | 马, | 4.11.11.3 1. | 6.3.7.6 | 7.6.4.6 | 3.11.0.0 | 10283 | 1.5.3.0 2 | 0.0.6.0 2 0.0.8.46 2 0.9.0.9 2 | 2.0.6.0 2 | 3.4.16 2 | 47.00 2 | 0 1 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 |

A TABLE OF FEET AND INCHES

from 5 foot 3 inches by 3 inches and 1 quarter to 7 foot 8 inches and 3 quarters by 6 inches.

| | | | | TI D-AT | | | TT Donto | El Parto | ET Parts | FIParte | F.I.Parts | FT Parts |
|--|--|--|--|--|--|--|--|--|--|--|--|--|
| 1.Parts | FIParis | 0.3 2 | 0.33 | 0.4.0 | 0.44 | F.I.Parts | 0.4 3 | 0.5.0 | 0.54 | 0.5 2 | 0.53 | 0.6:0. |
| 1.3.0 kg | 150000 | 16460 | 1 7 8 3 9 | 19.0000 | 1.10.3.0.0 | 1.11.7.6.0 | 2.0.11.3.0 2.1.0.5.3 2.1.1.7.6 2.1.2.0.9 | 2.2.3.0.0 2.2.4.3.0 2.2.2.6.0 2.2.6.0 | 2.3.6.0.0 2.3.8.0.9 2.3.0.4.6 2.3.10.8.3 | 9.4000 9.416100 9.5.1.3.0 9.5.2.7.0 | 2.6.3.3.0 2.6.3.1.6 2.6.6.6.9 | a.7.6.0.0 a.7.7.6.0 2.7.9.0.0 2.7.10.0.0 |
| 4. C. A. C. A. | 15400 | 168.0.0 | 1.8.0.0.0 | 19400 | 1.10.8.0.0 1.10.9.0.9 1.10.10.1.0 | 2.0.0.0.0 2.0.1.1.6 2.0.2.3.0 2.0.3.4.6 | 2.1.4.0.0 2.1.5.2.3 2.1.5.4.6 2.1.7.6.9 | 2.2.8.0.0 2.2.9.3.0 2.2.10.6.0 2.2.11.9.0 | 2.4.0.0.0 2.4.1.3.9 2.4.2.7.0 2.4.3.11.3 | 25,5000 | 2.6.8.0.0 2.6.9.5.3 2.6.10.10.6 2.7.0.3.9 | 2.0.4.0.0 |
| 5.5.0 ₄ | 15.7.3.0 | 1.6.11.6.0 | 18030 1450 1500 | 9,9000 | 1.11.0.3.0 1.11.1.3.0 1.11.2.4.0 1.11.3.5.3 | 2.0.4.6.0 2.0.5.7.6 2.0.6.9.0 2.0.7.10.6 | 2.1.8.0.0 2.1.9.11.3 2.1.11.1.6 2.2.0.3.9 | 2.3.1.0.0 2.3.2.3.0 2.3.3.6.0 2.3.4.9.0 | 2.4.5.3 0 2.4.6.6.0 2.4.7.10.6 2.4.7.3 | 2.5.0.0.0 2.5.10.10.6 2.6.0.3.0 2.6.1.7.6 | 2.7.1.0.0 2.7.3.2.3 2.7.4.0.0 2.7.6.0.0 | 2.8.6.0.0 2.8.7.6.0 2.8.0.0.0 2.8.0.0.0 |
| 1.6.0 ₄ | 1.5.10.6.0 | 1.7.3.0.0 | 18.7.6.0 | 1.10.0.0.0 1.10.1.0.0 1.10.2.0.0 1.10.3.0.0 | 1.11.4.0.0 1.11.5.6.9 1.11.6.7.6 1.11.7.8.3 | 2.0.0.0.0 2.0.10.1.0 2.0.11.3.0 2.1.0.4.6 | 2.2.1.0.0 2.2.2.8.3 2.2.3.10.6 2.2.3.0.9 | 2.3.7.3.0 2.3.8.6.0 2.3.9.9.0 | 2.4.10.0.0 2.4.11.0.0 2.5.1.1.6 2.5.2.5.3 | 2.0.3.0.0 2.0.4.4.0 2.6.5.0.0 2.6.7.1.0 | 2.7.8.H.3 2.7.10.4.6 2.7.11.9.0 | 2.9.1.6.0 2.9.3.0.0 2.9.4.6.0 |
| 7.04 | 1.6.1.9.0 1.6.2.6.9 1.6.3.4.6 1.6.4.2.3 | 1.7.6.6.0 | 1.8.11.3.0 | 1.10.4.0.0 | 1.11.8.9.0 1.11.9.9.9 1.11.10.10.6 | 2.1.1.6.0 2.1.2.7.6 2.1.3.0.0 2.1.4.10,6 | 2.2.6.3.0 2.2.7.5.3 2.2.8.7.6 2.2.9.9.9 | 2.3.11.0.0 2.4.0.3.0 2.4.1.6.0 2.4.2.9.0 | 2.5.3.0.0 2.5.5.0.4.0 2.5.7.8.3 | 2.6.8.6.0 2.6.9.10.6 2.6.11.3.0 2.7.0.7.6 | 2.8.4.1.6 2.8.4.1.6 2.8.5.6.9 | 2.9.7.6.0 2.9.7.6.0 2.9.0.0.0 2.9.10.6.0 |
| 9.0 m | 16500 | 1 .7 .10.0.0 | 1.9.3.0.0 1.9.3.11.3 1.9.4.10.6 1.9.5.0.9 | 1.10.8.0.0 1.10.9.0.0 1.10.10.0.0 1.10.11.0.0 | 2.0.1.0.0 2.0.2.0.0 2.0.3.1.6 2.0.4.2.3 | 2.1.6.0.0 2.1.7.1.6 2.1.8.3.0 2.1.9.4.6 | 2.2.11.0.0 2.3.0.2.3 2.3.1.4.6 2.3.2.6.9 | 2.4.4.0.0 2.4.5.3.0 2.4.6.6.0 2.4.7.9.0 | 2.5.0.0.0 2.5.10.3.0 2.5.11.7.6 2.0.0.11.3 | 2.7.2.0.0 2.7.3.4.6 2.7.4.0.0 2.7.6.1.6 | 2.8.7.0.0 2.8.8.5.3 2.8.9.10.6 2.8.11.3.9 | 2.10.1.6.0 2.10.3.0.0 2.10.4.6.0 |
| 9.0 | 1.6.8.3.0 | 1.8.1.6.0 | 1.9.6.9.0 | 1.11.0.0.0 | 2.0.5.3.0 2.0.6.3.0 2.0.7.4.6 2.0.8.5.3 | 2.1.10.6.0 2.1.11.7.6 2.2.0.9.0 2.2.1.10.6 | 2.3.3.9.0 2.3.4.11.3 2.3.6.1.6 2.3.7.3.9 | 9.4.9.0.0 9.4.10.3.0 9.4.11.6.0 9.5.0.9.0 | 2.6.2.3.6.9 2.6.4.0.6 2.6.6.2.3 | 2.7.7.0.0 2.7.8.10.6 2.7.10.3.0 2.7.11.7.6 | 2,9.2.2.3 2,9.3.7.6 2,9.5.0.9 | 2,10.7.6.0 2,10.9.0.0 2,10.10.6.0 |
| 5.10.0 | 1.6.11.6.0 | 1.8.5.0.0 | 1.9.10.6.0 | 1.11.4.0.0 | 2.0.9.6.0 2.0.10.6.9 2.0.11.7.6 2.1.0.8.3 | 2.2.3.0.0 2.2.4.1.6 2.2.5.3.0 2.2.6.4.6 | 2.3.8.0.0 2.3.9.8.3 2.3.10.10.6 2.4.0.0.9 | 2.5.2.0.0 2.5.3.3.0 2.5.4.6.0 2.5.5.9.0 | 2.6.8.9.9 2.6.10.1.6 2.6.11.5.3 | 2.8.2.4.6 2.8.3.9.0 2.8.51.6 | 2.9.7.11.3 2.9.9.4.6 2.9.10.9.9 | 2.11.1.6.0 2.11.3.0.0 2.11.4.6.0 |
| 5.11 · O. | 1.7.2.9.0 | 1.8.8.6.0 | 1.10.2.3.0 | 1.11.8.0.0 | 2.1.1.9.0 2.1.2.9.0 2.1.3.10.0 | 2.2.7.6.0 2.2.8.7.6 2.2.9.9.0 2.2.10.10.6 | 2.4.1,3.0 2.4.2.5.3 2.4.3.7.0 2.4.4.0.0 | 2.5.7.0.0 2.5.8.3.0 2.5.9.6.0 2.5.10.9.0 | 2.7.0.00 2.7.2.0.0 2.7.3.4.6 2.7.4.8.3 | 2.8.7.10.6 2.8.7.10.6 2.8.0.3.0 2.8.10.7.6 | 2.10.1.8.3 2.10.3.1.6 2.10.4.6.9 | 2.11.7.6.0 2.11.9.0.0 2.11.10.6.0 |
| 5.0.0 | 17.6.0.0 | 19.00.00 | 1.10.6.0.0 | 2.0.0.0.0 2.0.1.0.0 2.0.2.0.0 2.0.3.0.0 | 2.1.6.0.0 2.1.7.0.9 2.1.8.1.6 2.1.0.2.3 | 2.3.0.0.0 2.3.1.1.6 2.3.2.3.0 2.3.3.4.6 | 2.4.7.2.3 2.4.7.2.3 2.4.8.4.6 2.4.9.6.9 | 2.6.0.0.0 2.6.1.3.0 2.6.2.6.0 2.6.3.9.0 | 2.7.6.0.0 2.7.7.3.9 2.7.8.7.6 2.7.9.11.3 | 2, 9, 0, 0, 0 2, 9, 1, 4, 6 2, 9, 2, 9, 0 2, 9, 4, 1, 6 | 2.10.7.5.3 2.10.8.10.6 2.10.10.3.9 | 3.0.1.6.0 3.0.3.0.0 3.0.4.6.0 |
| .1.0 | 1.7.9.3.0 | 19.3.6.0 | 1 .10.9.9.0 1 .10.10.8 .3 1 .10.11.7.6 1 .11.0.6.9 | 2.0.4.0.0 2.0.5.0.0 2.0.6.0.0 2.0.7.0.0 | 2.1.10.3.0 2.1.11.3.9 2.2.0.4.6 2.2.1.5.3 | 2.3.4.6.0 2.3.5.7.6 2.3.6.9.0 2.3.7.10.6 | 2.4.10.9.0 2.4.11.11.3 2.5.1.1.0 2.5.2.3.0 | 2.6.5.0.0 2.6.5.3.0 2.6.7.6.0 2.6.8.9.0 | 2.7.11.3.0 2.8.0.6.9 2.8.1.10.6 2.8.3.2.3 | 2.0.5.0.0 2.0.6.10.6 2.0.8.3.0 2.0.9.7.6 | 2.11.1.2.3 2.11.2.7.6 2.11.4.0.9 | 3.0.7.6.0 3.0.0.0.0 3.0.10.6.0 |
| 1.2.C | 1 8 0 6 0 1 8 1 3 9 1 8 2 1 6 1 8 2 11 3 | 1.9.7.00 | 1.11.6.0 1.11.2.5.3 1.11.3.40 1.11.4.30 | 2.0.8.0.0 2.0.9.0.0 2.0.10.0.0 2.0.11.0.0 | 2, 2, 2, 6, 0 2, 2, 3, 6, 9 2, 2, 4, 7, 6 2, 2, 5, 8, 3 | 2.3.0.0.0 2.3.10.1.6 2.3.11.3.0 2.4.0.4.6 | 2.5.3.0.0 2.5.4.8.3 2.5.5.10.6 2.5.7.0.9 | 2.6.11.3.0 2.7.0.6.0 2.7.1.9.0 | 2.8.5.9.9 | 2.10.0.4.6 | 2.11.6.11.3 2.11.8.4.6 2.11.0.0.0 | 3.1.1.6.0 |
| 3.0 Jak | 1.8.3.9.0 1.8.4.6.9 1.8.5.4.6 1.8.6.2.3 | 1.0.10.6.0 | 1.11.5.3.0 | 2.1.0.0.0 2.1.1.0.0 2.1.2.0.0 2.1.3.0.0 | 2. 2. 6. 9. 0 2. 2. 7. 9. 9 2. 2. 8. 10. 6 2. 2. 9.11. 3 | 2.4.1.6.0 2.4.2.7.6 2.4.3.9.0 2.4.4.10.6 | 2.5.8.3.0 2.5.9.5.3 2.5.10.7.6 2.5.11.9.9 | 2.7.3.0.0 2.7.4.3.0 2.7.5.6.0 2.7.6.9.0 | 2.8.11.0.9 2.9.0.4.0 2.9.1.8.3 | 2.10.4.0.0 2.10.5.10.0 2.10.7.3.0 2.10.8.7.6 | 211.11.3.0 3.0.0.8.3 3.0.2.1.6 3.0.3.6.9 | 3.1.9.0.0 |
| 4.0 | 1.8.7.0.0 | 1.10.2.0.0 | 1.11.9.0.0 | 2.1.4.0.0 2.1.5.0.0 2.1.6.0.0 2.1.7.0.0 | 2. 2. 11. 0. 0 2. 3. 0. 0. 9 2. 3. 1 . 1 . 6 2. 3. 2 . 2 . 3 | 2.4.6.0.0 2.4.7.1.6 2.4.8.3.0 2.4.9.4.6 | 2.6.1.0.0 2.6.2.2.3 2.6.3.4.6 2.6.4.6.9 | 2.7.8.0.0 2.7.9.3.0 2.7.10.6.0 2.7.11.9.0 | 2.9.3.0.0 2.9.4.3.9 2.9.5.7.6 2.9.6.11.3 | 210.10.0.0 210.11.46 216.0.9.0 2.162.1.6 | 3.0.5.0.0 3.0.6.5.3 3.0.7.10.6 3.0.9.3.9 | 3.2.3.0.0 |
| . 5 · Custon | 1.8.10.3.0 1.8.11.0.0 1.8.11.10.6 1.9.0.8.3 | 1.10.5.6.0 1.10.6.4.6 1.10.7.3.0 1.10.8.1.6 | 2.0.0.9.0 2.0.1.8.3 2.0.2.7.0 2.0.3.6.9 | 2.1.8.0.0 2.1.0.0.0 2.1.10.0.0 2.1.11.0.0 | 2.3.3.3.0 2.3.4.3.9 2.3.5.4.0 2.3.6.5.3 | 2.4.10.6.0 2.411.7.6 2.5.0.9.0 2.5.1.10.6 | 2.6.4.0.0 2.6.6.11.3 2.6.8.1.6 2.6.9.3.9 | 2.8.1.0.0 2.8.2.3.0 2.8.3.6.0 2.8.4.9.0 | 2.9.8.3.0 2.9.0.6.9 2.9.10.10.6 2.10.0.2.3 | 2.11.3.0.0 2.11.4.10.6 2.11.6.3.0 2.11.7.7.6 | 3.0.10.9.0 3.1.0.2.3 3.1.1.7.6 3.1.3.0.9 | A Description of the Control of the |
| . 6 · C. | 19.1.0.0 | 1.10.9.0.0 | 2.0.4.6.0 | 9.7.0.0.0 9.9.1.0.0 9.9.2.0.0 | 2.3.7.0.0 2.3.8.6.0 2.3.9.7.0 | 2.5.4.1.6 2.5.5.3.0 2.5.6.4.6 | 2.6.11.8.3 2.7.0.10.6 2.7.2.0.9 | 2.8.7.3.0 2.8.8.6.0 2.8.9.9.0 | 2.10.2.0.9 | 2.11.10.4.0 2.11.14.0.0 3.0.1.1.0 | 3.1.4.6.0 3.1.5.11.3 3.1.7.4.6 3.1.8.9.9 | 3.3.3.0.0 |
| · 7 · 04 | 1.9.4.9.0 | 1.11.0.0.0 | 2.0.8.3.0 | 2.2.5.0.0 2.2.6.0.0 2.2.7.0.0 | 2.4.0.9.9 2.4.1.10.6 2.4.2.11.3 | 2.5.8.7.6 | 2.7.3.3.0 2.7.4.5.3 2.7.5.7.6 2.7.6.9.9 | 2.8.11.0.0 2.9.0.3.0 2.9.1.6.0 2.9.2.9.0 | 2.10.8.0.9 2.10.9.4.6 2.10.10.8.3 | 3.0.3.10.0 | 3.1.11.8.3 3.2.1.1.6 3.2.2.6.0 | 3.3.7.6.0 3.3.9.0.0 3.3.10.6.0 |
| · 9 · 0 | 1.9.8.9.9 1.9.9.7.6 1.9.10.5.3 | 1.11.4.0.0 | 2.1.0.0.0 2.1.0.11.3 2.1.1.10.0 2.1.2.9.9 | 2.2.8.0.0 a.2.0.0.0 a.2.10.0.0 a.2.11.0.0 | 2.4.5.0.0 2.4.5.0.0 2.4.6.1.6 2.4.7.2.3 | 2.6.1.1.6 2.6.2.3.0 2.6.3.4.6 | a.7.8.0.0 2.7.9.2.3 2.7.10.4.6 2.7.11.6.9 | 2.9.4.0.0 2.9.5.3.0 2.9.6.6.0 2.9.7.9.0 | 2.11.0.0.0 2.11.1.3.9 2.11.2.7.6 2.11.3.11.3 | 3.0.10.0.0 | 3.2.4.0.0 3.2.5.5.3 3.2.6.10.0 3.2.8.3.9 | 3.4.4.6.0 |
| 9.0 | 1.0.11.3.0 1.10.0.0.0.0 1.10.0.10.6 1.10.1.8 3 | 1.11.8.4.6 | 2.1.50.0 | 2.3.1.0.0 2.3.2.0.0 2.3.3.0.0 | 2.4.9.3.9 2.4.10.4.6 2.4.11.5.3 | 2.6.5.7.6 2.6.6.9.0 2.6.7.10.6 | 2.8.0.9.0 2.8.1.11.3 2.8.3.1.6 2.8.4.3.9 | 2.9.9.0.0 2.9.11.6.0 2.10.0.9.0 | 2.11.6.6.9 | 3.1.4.3.0 | 3.3.1.0.0 | 3.4.7.6.0 |
| ·10.0 | 1.10.2.6.0 | 1.11.11.0.0 | 2.1.7.6.0 | 2.3.4.0.0 2.3.5.0.0 2.3.6.0.0 2.3.7.0.0 | 2.5.0.0.0 2.5.1.6.0 2.5.2.7.6 2.5.3.8.3 | 2.6.10.1.6 2.6.11.3.0 2.7.0.4.6 | 2.8.5.6.0 2.8.6.8.3 2.8.7.10.6 2.8.9.0.9 | 2.10.2.0.0 2.10.3.3.0 2.10.4.6.0 2.10.5.9.0 | 3.0.2.5.3 | 3-111-1-0 | 3.3.3.6.0 3.3.4.11.3 3.3.6.4.0 3.3.7.9.0 3.3.9.3.0 | 3.5.1.6.0 3.5.3.0.0 3.5.4.6.0 |
| . II . C. Jankin . S. la | 1.10.5.9.0 1.10.6.6.9 1.10.7.4.6 1.10.8.2.3 | 20.260 20.346 20.430 10.516 | 2.1.11.3.0 2.2.0.2.3 2.2.1.1.6 2.2.2.0.9 | 2, 3, 8, 0, 0 2, 3, 9, 0, 0 2, 3, 10, 0, 0 2, 3, 11, 0, 0 | 2.5.4.9.0 2.5.5.9.9 2.5.6.10.6 2.5.7.11.3 | 2.7.7.0.0 2.7.2.7.6 2.7.3.9.0 2.7.4.10.6 | 2.8.11.5.3 2.9.0.7.6 2.9.1.9.9 | 2.10.6.3.0 2.10.9.6.0 2.10.10.9.0 | 3.0.5.0.9 3.0.6.4.6 3.0.7.8.3 | 3. 2. LIRO 3. 2. 3. 3. 0 3. 2. 4. 7. 0 | 3.4.1.6.9 | 3.5.70.0.0 |
| 0.0 | 1.10.9.0.0 1.10.9.9.9 1.10.10.7.6 1.10.11.5.3 | 20600 | 2.2.3.0.0 2.2.3.11.3 2.2.4.10.0 2.2.5.0.9 | 2. 4.0.0.0 2. 4.1.0.0 2. 4.2.0.0 2. 4.3.0.0 | 2.5.9.0.0 2.5.10.0.9 2.5.11.1.6 2.6.0.2.3 | 2.7.0.0.0 2.7.7.1.6 2.7.0.3.0 2.7.9.4.0 | 2.9.4.2.3 | 2.11.1.3.0 | 3.0:10.3.9 | 3-2-7-4-6 | 3.4.4.5.3 | 3.6.3.0.0 |
| Charling | 111.2.8.3 | Name and Address of the Owner, which is | Control of the Contro | | | 2.7.0.6.0 2.7.11.7.6 2.8.0.0.0 2.8.1.10.6 | 2.9.7.9.0 2.95.11.3 2.9.10.1.6 4.9.11.3.9 | 2.11.5.0.0 2.11.6.3.0 2.11.7.6.0 2.11.6.0.0 | | | 3.4.10.2.3 3.4.11.7.0 3.5.1.0.0 3.5.2.6.0 | 3.6.6.0.0 3.6.7.6.0 3.6.9.0.0 3.6.0.6.0 |
| 3 | 1.11.3.6.0 | 2.1.29.0 | 2.3.0.4.0 | 2. 4.0.0.0 | 2.6.7.7.6 | 2.8.3.0.0 2.8.5.3.0 2.8.6.4.6 | 2.10.1.8.3 2.10.2.10.6 2.10.4.0.9 | 3.0.1.0.0 | 31.8.9.9 | 3.3.7.9.0 | 3.5.3.11.3 3.5.5.4.0 3.5.6.9.9 3.5.8.3.0 | 3.7.1.0.0 3.7.3.0.0 3.7.4:6.0 3.7.6.0.0 |
| | 1.11.6.9.0 | | 2.3.2.3.0 2.3.3.4.1.6 2.3.5.0.9 | 2.5.0.0.0 2.5.1.0.0 2.5.2.0.0 2.5.3.0.0 | 2.0.9.9.0 2.6.11.10.6 2.7.0.11.3 | 2.8.9.9.9 2.8.0.10.6 | 2.10.0.5.3 2.10.7.7.6 2.10.9.9.9 | 3.0.4.3.0 3.0.5.0.0 3.0.6.9.0 | 3.2.2.0.9 3.2.3.4.6 3.2.4.6 3.2.6.0.0 | 3.4.1.3.0 | 3.5.9.8.3 3.5.11.1.0 3.6.0.6.9 3.6.2.0.0 | 3.7.6.0.0 3.7.7.6.0 3.7.70.0.0 3.7.70.0.0 |
| | 1.11.10.0.0 1.11.10.9.9 1.11.11.7.6 2.0.0.5.3 | | 2.3.6.0.0 2.3.6.11.3 2.3.7.10.6 2.3.8.9.9 | 2.5.5.0.0 2.5.6.0.0 2.5.7.0.0 | 2.7.3.0.9 2.7.4.1.6 2.7.5.2.3 | 2.0.0.0.Q 2.0.1.1.0 2.0.2.3.0 2.0.3.4.0 | 2.10.11.2.3 | 3.0.0.3.0 3.0.10.6.0 3.0.11.9.0 | 3.2.7.3.0 3.2.8.7.6 3.2.9.11.3 | 3.4.5.4.6 3.4.6.9.0 3.4.8.1.6 | 3.6.4.10.0 3.6.6.3.9 3.6.7.9.0 | 3.8.0.0.0 3.8.1.6.0 3.8.3.0.0 3.8.4.6.0 3.8.6.0.0 |
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| \$ 27.2 6.0 2.0.7.4.6 3 2.7.3 4.6 0.0.6.3 0 3 2.7.4.2.3 2.0.0.1.6 3 | 3.0.0, 4.3, 3.2, 5.0.0, 3.4.0.0, 0.3, 3.2, 0.0.0, 3.4.0.0, 0.3, 3.2, 7.0.0, 3.4.0.0, 0.3, 3.2, 7.0.0, 3.4.0.0, 0.3, 3.2, 7.0.0, 3.4.0.0, 0.3, 3.2, 7.0.0, 3.4.0.0, 0.3, 3.2, 7.0.0, 3.4.0.0, 0.3, 4.0.0, 0.3, 3.2, 7.0.0, 3.4.0.0, 0.3, 3.2, 7.0.0, 3.4.0.0, 0.3, 4.0.0, 0.3, 3.2, 7.0.0, 3.4.0.0, 0.3, 3.2, 7.0.0, 3.4.0.0, 0.3, 4.0.0, 0.3, 3.2, 7.0.0, 0.3, 4.0.0, 0.3, 3.2, 7.0.0, 0.3, 4.0.0, 0.3, 3.2, 7.0.0, 0.3, 4.0.0, 0.3, 3.2, 7.0.0, 0.3, 4.0.0, 0.3, 3.2, 7.0.0, 0.3, 4.0.0, 0.3, 3.2, 7.0.0, 0.3, 4.0.0, 0.3, 3.2, 7.0.0, 0.3, 4.0.0, 0.3, 3.2, 7.0.0, 0.3, 4.0.0, 0.3, 3.2, 7.0.0, 0.3, 4.0.0, 0.3, 3.2, 7.0.0, 0.3, 4.0.0, 0.3, 3.2, 7.0.0, 0.3, 4.0.0, 0.3, 3.2, 7.0.0, 0.3, 4.0.0, 0.3, 3.2, 7.0.0, 0.3, 4.0.0, 0.3, 3.2, 7.0.0, 0.3, 4.0.0, 0.3, 0.3, 0.2, 0.3, 0.2, 0.3, 0.3, 0.2, 0.3, 0.2, 0.3, 0.2, 0.3, 0.2, 0.3, 0.2, 0.3, 0.2, 0.3, 0.2, 0.3, 0.2, 0.3, 0.2, 0.3, 0.2, 0.3, 0.2, 0.3, 0.2, 0.3, 0.2, 0.3, 0.2, 0.3, 0.2, 0.3, 0.2, 0.3, 0.2, 0.3, 0.2, 0.3, 0.2, 0.2, 0.3, 0.2, 0.2, 0.2, 0.2, 0.2, 0.2, 0.2, 0.2 | 7.2.7.0 3.0.7.5.3 4.0.0.3.0 4.2.5.0 7.3.0.0 3.0.8.7.0 4.0.1.0.0 4.2.6.4 7.4.0.0 3.0.0.0 4.2.7.8 | 0 4.49.0.0 4.7.2.8.3 4.9.7.0.0 0 4.411.3.0 4.7.4.0 4.0.0.0.0 3 4.5.0.4.0 4.7.5.6.0 4.0.0.0.0 |
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| 9.9.0, 2.7.8.3.0 2.10.1.6.0 3 4, 2.7.0.0.0 2.10.2.4.6 3 2.7.0.10.6 2.10.3.3.0 3 | 0.0.0.00 3.3.0.0.0 3 5.5.3.0 3 0.7.6.3 3.3.1.0.0 3 5.6.3.0 3 0.6.7.6 3.3.2.0.0 3 5.7.4.6 3. | 7.10.0.0 3.10.3.0.0 4.0.0.0.0 4.3.2.3 7.11.7.0 3.10.4.11.3 4.0.10.3.0 4.3.3.6 8.0.0.0 3.10.6.4.0 4.0.11.0.0 4.3.4.0 8.1.10.0 3.10.7.3.0 4.1.0.0.0 4.3.4.0 | 0 4 5 7 0 0 4 8 0 0 0 4 8 8 4 0 7 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 |
| 9.10.0, 2.7.11.6.0 210.5.0.0 3 4, 28.0.3.0 210.5.0.0 3 5, 28.1.1.6 210.6.0.0 3 | 0.10.6.0 3.3.4.0.0 3 5.0.6.0 3. 0.11.5.3 3.3.5.0.0 3 5.0.6.0 3. 1.0.4.6 3.3.6.0.0 3 5.0.6.0 3. | 8.3.0.0 3.10.7.3.0 4.1.0.0.0 4.3.7.6. 8.4.1.6 3.10.0.8.3 4.1.3.3.0 4.3.8.0. 8.5.3.0 3.10.10.10.0 4.1.4.0.0 4.3.10.1. 8.5.4.0 3.11.0.0.0 4.1.5.0.0 4.3.11.5. | 0 4.6.1.00 4.6.6.00 411.0.00 |
| 9.11.0, 28.2.9.0 210.8.6.0 3 28.3.6.0 210.0.3.0 3 28.4.4.6 210.10.3.0 3 | .1.1.3.0 3.3.7.0.0 3 8.0.8.3 3. .1.2.3.0 3.3.8.0.0 3 6.1.0.0 3. | 8.7.6.0 3.11.0.0.0 4.1.5.0.0 4.3.11.5 8.7.6.0 3.11.1.3.0 4.1.7.0.0 4.40.0 8.8.7.6 3.11.2.6.3 41.8.3.0 | 0 4.6.6.6.0 4.9.0.3.0 4.11.4.6.0 |
| 28.4.4.6 210.10.3.0 3 28.5.2.3 210.11.1.0 3 10.0.0, 28.6.0.0 211.0.9.3 3 | 1. 5.0.0 3.3.11.0.0 30.3 10.0 3. 1. 5.0.0 3.3.11.0.0 30.4.11.3 3. | 8.7.0.0 3.11.1.3.0 41.7.0.0 44.0.0 8.8.7.0 3.11.2.5.3 41.8.3.0 44.2.0 8.0.0.0 3.11.3.7.0 41.0.0.0 44.3.4 8.10.10.0 3.11.4.0.0 41.0.0.0 4.4.48. | 3 4.6.0.7.0 4.9.4.60 411.0.6.0 |
| 2, 20.7.7.0 211.0.00.4 3 2, 20.7.7.0 211.1.0.0 3 2, 20.8.5.3 211.2.7.6 3 | 7.7.0.0 3.4.2.0.0 30.70.0 3 1.0.0.0 3.4.3.0.0 36.8.1.0 3 1.0.0.0 3.4.3.0.0 36.8.2.3 3 | 0.0.0.0 3.11.0.0.0 42.0.0.0 4.4.0.0.0 0.1.1.0 3.11.7.2.3 4.2.1.3.0 4.4.7.3, 0.2.3.0 3.11.8.4.0 4.2.2.0.0 4.4.8.7. 0.3.4.0 3.11.0.0.0 4.2.3.0.0 4.4.0.11, | 0 4.7.4.1.0 4.0.7.5.3 3.0.1.0.0 3 4.7.4.1.0 4.0.0.3.0 3.0.3.0.0 |
| 10.1.0, 28.0.3.0 2.11.3.6.0 3 28.10.0.0 2.11.4.4.6 3 28.10.10.0.0 2.11.4.3.0 3 28.11.8.3 211.6.1 6 | 1 10 8 3 3 4 5 0 0 3 0 13 0 3 3 3 4 5 0 0 0 3 7 0 4 0 3 3 4 7 0 0 0 3 7 0 4 0 3 3 4 7 0 0 0 3 7 1 3 3 3 3 | 0.400 311.0900 4.2.500 4.4.11 3 4.2.6.30 4.50 3 6 6 7.10.0 4.0.2.3.0 4.2.6.0 4.5.2.2. | 0 4.70.0.0 40.1 1.3 30.7.0.0 0 4.78 3.0 40.2.70 30.00.0 3 4.70.1.0 40.4.00 50.00.0 |
| 10.2.0, 20.0.0.0 211.7.0.0 3 2.0.1.3.0 211.7.0.0 3 2.0.2.1.0 2116.0.0 3 2.0.2.1.3 2116.0.0 3 | 12.1.0.0 34.8.0.0 37.2.8.0 3. 12.2.5.3 34.0.0 0 37.3.6.0 3. 12.3.4.0 34.0.0 0 37.4.7.0 3. | 00000 +0360 +2000 +356 | 0 4 7 10 0 0 40 5 6 0 5 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 |
| 2 20.2 .11.3 2.11.9.7.0 3 | 37.58.3 3 | 10.0.4.0 4.0.7.0.9 4.3.1.9.0 4.30.3. | |

A TABLE OF FEET AND INCHES from 10 foot 3 inches by 3 inches and 1 quarters to 12 foot 5 inches and 3 quarters to 6 inches.

| WI Davie | FI Berrs | ELParts | FI Perrs | F.I.Parts | F.I.Parts | | | | | | | A CONTRACTOR |
|---|--|--|---|--|--|---|---|--|---|--|---|---|
| r.I.rar to | 0.3.4 | 0.3 2 | 0.3.3 | 0.4.0 | 0.4 4 | 0.45 | 0.43 | 0.5.0 | F.I. Parts | FI Parts | 0.53 | F.I.Parts 0.6.0 |
| | 29 3 9 0 29 4 6 9 29 5 4 6 20 6 2 3 | 2.11.10,6.0 2.11.11.4.6 3.0.0.3.0 3.0.1.1.6 | 3.25 3.0 3.26 2.3 3.27 1.6 3.28 0.9 | 3.5.0.0.0 35.1.0.0 35.20.0 35.3.0.0 | 3.7.6.9.0 3.7.7.9.9 3.7.8.10.6 3.7.9.11.3 | 3.10.1.6.0 3.10.2.7.6 3.10.3.9.0 3.10 4.10.6 | 4.0.8, 3.0 4.0.9.5.3 4.0.10.7.6 4.0.11.9.9 | 4.3.3.0.0 4.3.4.3.0 4.3.5.6.0 4.3.6.0 | 4.3.9.9.0 4.5.11.0.0 4.6.0.4.6 4.6.1.8.3 | 4, 8. 4.6. 0 4 8.5. 10.6 4 8.7. 3.0 4 8.8.7.6 | 4.0.11.3.0 4.11.0.8.3 4.11.2.1.6 4.11.3.6.0 | 5.1.6.0.0 5.1.7.6.0 5.1.9.0.0 5.1.10.6.0 |
| 10.4.0 | CO. M. CARACTER | 3.0.2.10.6 3.0.3.9.0 3.0.4.7.6 | 3.29.11.3 3.210.10.6 3.211.9.0 | 3.5.5.0.0 3.5.6.0.0 3.5.7.0.0 | 38.0.0.9 | 3.10.7.1.6 3.10.8.3.0 3.10.9.4.6 | 4.1.3.4.6 | 4.3.0.0.0 4.3.0.0.0 4.3.10.0.0 4.3.11.9.0 | 4.6.4.3.0 4.6.5.7.6 4.6.6.11.3 | 4.8.10.0.0 4.8.11.4.6 4.9.0.9.0 4.9.2.1.6 | 4.11.5.0.0 4.11.6.5.3 4.11.7.10.6 4.11.0.3.9 | 5.2.0.0.0 5.2.1.6.0 5.2.3.0.0 5.4.4.6.0 |
| 10.5.0 | 2.9.11.0.9 2.9.11.10.6 2.10.0.8.3 | 3.0.5.6.0 3.0.6.4.0 3.0.7.3.0 3.0.7.3.0 | 3.3.0.9.0 | 35.8.0.0 35.9.0.0 35.10.0.0 35.11.0.0 | 3.8.3.3.0 3.8.4.3.9 3.8.5.4.6 3.8.5.5.3 | 3.10.10.6.0. 3.10.11.7.6 3.11.0.9.0 3.11.110.6 | 4.1.5.0.0 | 4.4.1.0.0 4.4.2.3.0 4.4.3.6.0 | 4.6.8.3.6 4.6.0.6.0 4.6.10.10.6 | 4.0.3.6.0 4.0.4.10.6 4.9.6.3.0 | 4.11.10 9. 0 5. 0. 0. 2. 3 5. 0! 1. 7. 6 | 5 2 6.0.0 5 2.7.6.0 5.2.9.0.0 |
| 10.6.0 | 2.10.2.3.9 2.10.3.1.6 2.10.3.11.3 | 3.0.9.0.6 3.0.9.0.6 3.0.10.9.0 3.0.11.7.6 | 3.3.5.5.3 | 3.6.0.0.0 3.6.1.0.0 3.6.2.0.0 3.6.3.0.0 | 3.8.7.6.0 3.8.8.6.9 3.8.9.7.6 3.8.10.8.3 | 3.11.4.1.6 3.11.5.3.0 3.11.6.4.6 | 4.1.11.8.3 4.2.0.10.0 4.2.2.0.0 | 4.4.0.0.0 4.4.7.3.0 4.4.8.6.0 | 4.7.1.6.0 4.7.2.0.0 4.7.4.1.6 | 4.0.0.0.0 4.0.10.46 4.0.11.9.0 | 5. 0. 4. 6. 0 5. 0. 5. 11. 3 5. 0. 7. 4. 6 | 5.3.0.0.0 5.3.1.0.0 5.3.3.0.0 |
| 10.7.0 | 2.10.5.6.9 2.10.6.4.6 2.10.7.2.3 | 31.1.4.6 31.2.3.0 3.1.3.1.6 | 3.3.10.1.6 3.3.11.0.9 | 3.6.5.0.0 | 3.6.11.0.0 3.9.0.9.9 3.9.1.10.0 3.9.2.11.3 | 3.11.7.0.0 3.11.8.7.6 3.11.9.9.0 3.11.10.10.0 | 4.2.3.3.0 4.2.4.5.3 4.2.5.7.6 4.2.6.9.0 | 44.11.0.0 45.0.3.0 4.5.1.6.0 45:2.9.0 | 4.7.6.0.0 4.7.8.0.0 4.7.0.4.0 4.7.10.8.3 | 4.10.2.60 4.10.3.10.6 4.10.5.30 4.10.6.7.6 | 5.0.10.3.0 5.0.11.8.3 5.1.1.1.6 5.1.2.6.0 | 5.3.6.0.0 5.3.7.6.0 5.3.0.0.0 5.3.10.6.0 |
| 10.0.04 | 2.10.8.9.9 2.10.9.7.6 2.10.10.5.3 | 3.1.4.10.6 | 3.4.0.11.3 3.4.1.10.6 3.4.2.9.9 | 3.6.9.0.0 3.6.10.0.0 3.6.11.0.0 | 3.9.4.0.0 3.9.5:0.9 3.9.6.1.6 3.9.7.2.3 | 4.0.0.0.0 4.0.1.1.6 4.0.2.3.0 4.0.3.4.6 | 4.2.8.0.0 4.2.9.2.3 4.2.10.4.6 4.2.11.6.9 | 4.5.4.0.0 4.5.5.3.0 4.5.0.6.0 4.5.7.9.0 | 4.8.0.0.0 4.8.1.3.0 4.8.2.7.0 4.8.3.11.3 | 4.10.9. 4.6 4.10.9. 4.6 4.10.10.9.0 | 5.1.4.0.0 5.1.5.5.3 5.1.6.10.6 5.1.8.3.9 | 5.4.0.0.0 5.4.1.6.0 5.4.3.0.0 5.4.4.6.0 |
| 100 | 2.11.0.10.6 2.11.0.10.6 2.11.1.8.3 | 3.1.7.6.0 3.1.8.4.6 3.1.9.3.0 3.1.0.1.6 | 3.4.5.7.0 3.4.5.7.0 | 3.7.0.0.0 3.7.1.0.0 3.7.2.0.0 3.7.3.0.0 | 3.9.0.3.0 | 4.0.4.0.0 | 4.3.0.9.0 4.3.1.11.3 4.3.3.1.6 | 4.5.9.0.0 4.5.10.3.0 4.5.11.6.0 | 4.8.6.6.0 4.8.7.10.6 | 4.11. 1.6.0 4.11. 2.10.6 4.11.4. 3.0 | 5. 1. 9. 9. 0 5. 1. 11. 2. 3 5. 2. 0. 7. 6 | 5.4.0.0.0 5.4.7.6.0 5.4.0.0.0 |
| 10.10.0 | 2.11.3.3.9 2.11.4.1.6 2.11.4.11.3 | 3.1.11.10.6 3.2.0.0.0 3.2.1.7.6 | 3.4.8.5.3 3.49.4.0 3.40.3.9 | 37.40.0 37.5.0.0 37.6.0.0 37.7.0.0 | 3.10.0.0.0 3.10.1.6.9 3.10.2.7.6 3.10.3.8.3 | 4.0.9.0.0 4.0.10.1.6 4.0.11.3.0 4.1.0.4.6 | 4.3.5.6.0 4.3.6.8.3 4.3.7.10.6 4.3.9.0.9 | 46.2.0.0 46.3.3.0 4.6.4.6.0 4.6.5.9.0 | 4.8.10.6.0 4.8.11.0.0 4.9.1.1.6 4.9.2.5.3 | 4.11.7.0.0 4.11.8.4.6 4.11.9.9.0 4.11.11.1.6 | 5. 2. 3. 0. 0 5. 2. 4. 11. 3 5. 2. 6. 4. 6 5. 2. 7 0. 0 | 5.5.0.0.0 5.5.1.6.0 5.5.3.0.0 |
| 10.11.0 | 2.11 . 7 . 4 . 6 2.11 . 7 . 4 . 6 2.11 . 8 . 2 . 3 | 3.2.3.4.6 3.2.4.3.0 3.2.5.1.6 | 3.4.11.3.0 3.5.0.2.3 3.5.1-1.6 3.5.2.0.6 | 3.7.8.0.0 3.7.9.0.0 3.7.10.0.0 | 3.10.4.0.0 3.10.5.9.9 3.10.6.10.6 3.10.7.11.3 | 4.1.2.7.6 4.1.3.9.0 4.1.4.10.6 | 4.3.10.3.0 4.3.11.5.3 4.4.0.7.0 4.4.1.9.0 | 4.6.7.0.0 4.6.8.3.0 4.6.9.6.0 4.6.10.0.0 | 4.9.3.9.0 4.9.5.0.0 4.9.6.4.6 | 5.0.0.6.0 5.0.1.10.6 5.0.3.3.0 | 5. 2.9.3.0 5. 2.10.8.3 5. 3. 0. 1. 6 | 5.5.6.0.0 5.5.7.6.0 5.5.9.0.0 |
| 1.0.0 | 2.11.9.9.9 2.11.10.7.6 2.11.11.5.3 | 3.2.6.10.6 3.2.7.9.0 3.2.8.7.6 | 3.5.3.11.3 3.5.4.10.6 3.5.5.9.9 | 8.0.0.0 8.1.0.0 8.2.0.0 | 3.10.9.0.0 3.10.10.0.9 3.10.11.1.6 3.10 0.2.3 | 4.1.7.1.0 4.1.8.3.0 4.1.9.4.0 | 4.4.3.0.0 4.4.4.2.3 4.4.5.4.6 4.4.6.6.0 | 4.7.0.0.0 4.7.1.3.0 4.7.2.6.0 4.7.3.0 0 | 4.9.9.0.0 4.9.10.3.9 4.9.11.7.6 | 0.6.0.0 | 3.3.0.0 .3.4.5.3 .3.5.10.6 | 5.6.0.0.0 |
| 40 | 301.0.6 | 3. 2.10.4.6 3. 2.11.3.0 3. 3. 0. 1.6 | 3.5.7.8.3.3 3.5.8.7.6 3.5.9.6.9 | .8.5.0.0 .8.6.0.0 | 3.11.2.3.9 3.11.3.4.6 3.11.4.5.3 | 4.1.10.6.0 4.1.11.7.6 4.2.0.9.0 4.2.1.10.6 | 4.4.7.9.0 4.4.8.11.3 4.4.10.1.6 4.4.11.3.9 | 4.7.5.0.0 4.7.6.3.0 4.7.7.6.0 47.8.9.0 | 4.10.2.3.0 4.10,3.6.0 4.10.6.2.3 | .1.0.10.6 .1.2.3.0 .1.3.7.6 | .3.8.9.0 .3.10.2.3 .3.11.7.6 .4.1.0.9 | 5.6.7.6.0 5.6.7.6.0 5.6.9.0.0 5.6.10.6.0 |
| | 3.0.4.3.9 3.0.5.1.6 0.5.11.3 | 3.1.10.6 3 3.2.9.0 3 3.3.7.6 3 | 5.11.5.3 | 6.0.0.0 6.9.0.0 6.100.0 | 3.11.5.6.6 3.11.6.6.9 3.11.7.7.6 3.11.8.8.3 | 4.2.3.0.0 | 4.5.1.8.3 4.5.1.8.3 4.5.2.10.6 4.5.4.0.9 | 4.7.10.0.0 4.7.11.3.0 4.8.0.6.0 4.8.1.0.0 | 4.10.7.0.0 4.10.8.0.0 4.10.10.1.6 5 4.10.11.5.3 | .1.5.0.0 .1.6.4.6 .1.7.9.0 5.1.9.1.6 | 4.2.6.0 4.3.11.3 4.5.4.6 4.6.0.9 | 5.7.0.0.0 5.7.1.6.0 5.7.3.0.0 5.7.4.6.0 |
| 1.4.0. 3 | 30.7.6.0 3 30.8.4.6 3 30.9.2.3 3 | 3.7.1.0 3 | 6.2.3.0 3 6.3.2.3 3 6.4.1.6 3 6.5.0.0 3 | 93.0.0 | 3.11.10.0.0 3.11.10.0.0 3.11.11.10.0 4.0.0.11.3 | 4.28.7.6 4.29.9.0 4.210.10.6 | 4.5.7.7.0 | 4.8.6.9.0 | 1.11.4.8.3 5 | .1.10.6.0 5 .1.11,10.6 5 .2.1.3.0 5 .2.2.7.6 5 | 48.3.0 49.8.3 411.1.6 5.0.6.9 | 7.0.0.0 7.7.6.0 7.0.0.0 |
| 1.5.Q 3 | 3.0.10.9.9 3.0.11.7.6 3.1.0.5.3 | 3.9.9.0 3.10.7.0 3 | 6.8.9.9 | 9.5.0.0 | 4.0.3.0.9 4.0.4.1.6 4.0.5.2.3 4.0.6.3.0 | 4.3.1.1.6 4.3.2.3.0 4.3.3.4.6 | 1.5.11.2.3 1.6.0.4.6 1.6.1.6.9 | 4.8.9.3.0 4.8.10.6.0 4.8.11.9.0 | 1.11.6.0.0.5 1.11.7.3.0.5 1.11.8.7.6.5 1.11.0.11.3 | 2.6.9.0 5. 2.8.1.6 5. | E A 10 014 | .8.0.0.0 .8.1.0.0 .6.3.0.0 .8.4.6.0 |
| 33333 | .1.4.6.0 3 | 4.0.4.6 3 4.1.3.0 3 4.2.1.6 3 | 7.1 0.0 3 | 10.0.0.0 | 4.0.7.3.0 4.0.8.4.6 4.0.9.5.3 | 4.3.4.0.0 4.3.5.7.0 4.3.6.9.0 4.3.7.10.0 | .6.3.11.3 .6.5.1.6 .6.6.3.9 | 1.9.3.0.0 3 1.9.4.9.0 3 | .0.3.2.3 5. | 3. 0. 3. 0 5. 3. 1. 7. 0 5. | 5.7.9.0 5.9.2.3 5.10.7.6 6.0.0.9 | 8.0.0.0 8.7.6.3 8.0.0.0 |
| 4, 13 2, 3 | 5.3.9 3 | 4.4.9.0 3 | 7.2.5.3 | 10.1.0.0 | 1.0.7.6 | 4.3.10.1.0 | .6.9.10.6 .6.11.0.9 | .9.7.3.0 .9.8.6.0 .9.9.0.0 | .0.7.1.6 5. | 3. 3. 0. 0 5. 3. 4. 4.6 5. 3. 5. 0. 0 5. 3. 7. 1. 6 5. | 6.1.0.0 6.2.11.3 6.4.4.6 6.5.9.9 6.7.2 | 9.1.0.0 9.3.0.0 9.4.6.0 |
| \$ 3. \$ 3. \$ 3. 3 3. | 1.11.0.0 3. | 4.10.0.0 3 | 7.6.2.3 7.7.1.6 7.0.0.9 3. | 4 | | 4.4.2.7.6 4.4.3.9.0 4.4.4.10.6 | 7.1.5.3 | 10.1.0.0 | .0.11.0.9 5. .1.0.4.6 5. .1.1.8.3 5. | 3. 9.10.6 5. 3. 11. 3.0 4. 0. 7.6 5. | | 9.9.0.0 9.10.6.0 |
| 9.0 3. | 2.0.7.6 3. 2.1.5.3 3. 2.2.3.0 3. | 4.10.10.6 3. 4.11.9.0 3. 5.0.7.6 3. 5.1.6.0 3. | 7.9.11.3 3.1.1.10.10.6 3.1.11.0.9 3.1 8.0.0.0 3.1 | 10.9.0.0 4 10.10.0.0 4 10.11.0.0 4 | 1.8.0.9 | 1.4.8.3.0 4 1.4.9.4.0 4 | 7. 6.2.3 4 7. 7. 4.6 4 7. 8.6.9 4 | 10.5.3.0 10.6.6.0 3 10.7.9.0 5 | 1.6.11.3 | 4.2.0.0 5. 4.3.4.6 5. 4.4.9.0 5. 4.6.1.6 5. 4.7.6.0 5. | 7. 1. 0. 0 5. 7. 2. 5. 3 5. 7. 3. 10. 0 5. 7. 5. 3. 0 5. | 10.3.0.0 10.3.0.0 10.3.0.0 |
| 10.0 3. | 2.3.0.6 3. 2.3.10.6 3. 2.4.8.3 3. | 5.2.4.6 3. 5.3.3.0 3. 5.4.1.6 3. | 8 · 1 · 8 · 3 · 3 · 3 · 3 · 6 · 9 · 3 · 6 | 11.1.0.0 4 11.2.0.0 4 11.3.0.0 4 | .2.0.3.0 4 .2.1.4.6 4 .2.2.5.3 4 | 1.4.11.7.0 4 1.5.0.9.0 4 1.5.1.10.0 4 | 8.0.1.6 4.1.3.9 4.2.6.0 | 10.10.3.0 5 | 1.0.6.0 5.4 | 1.8.10.6 5. 1.10.3.0 5. 1.11.7.6 5. | 7.8.2.3 5. 7.9.7.6 5. 7.11.0.9 5. | 10.0.0.0 10.7.6.0 10.0.0.0 10.0.6.0 |
| 11. Q 3. | 2.7.16 3. 2.7.11.3 3. 2.8.0.0 3. | 5.6.0.0 3. 5.6.0.0 3. 5.7.7.6 3. | 8.5.5.3 8.0.40 3. 8.7.3.0 3. 8.0.3.0 3. | 11.5.0.0 4 | 2. 4.0.0 4 | 5.5.3.0 4 | 8.7.3.0 4 | 11.7.0.0 1 | 2.4.1.6 2.5.5.3 2.6.0.0 | 6.6.0 6 | 3.1.11.3 5. 3.3.4.6 5. 3.4.9.0 5. | 11.0.0.0 11.1.6.0 11.3.0.0 11.4.6.0 |
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| 1.0 3.3 | 3.1.7.0 3.1 3.2.5.3 3.1 | 6.3.6.0 30 | 2.3.0.0 4. | 0.1.0.0 4. 0.2.0.0 4. 0.3.0.0 4. | 3.1.0.9 4 3.2.1.6 4 3.3.2.3 4 | 6.1.1.6 4. 6.2.3.0 4. 6.3.4.6 4. | 9.1.2.3 5. 9.2.4.0 5. 9.3.0.9 5. | 0.1.3.0 5. 0.2.6.0 5. 0.3.0.0 5. | 3.1.3.0 5.6 3.2.7.0 5.6 3.3.11.3 5.6 3.5.3.0 5.6 | 1.4.6 5.0 2.0.0 5.0 4.1.6 5.0 | .2.10.6 6. .4.3.9 6. | 0.1.6.0 0.3.0.0 0.4.6.0 0.6.0.0 |
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| 3.0, 3.3 | 3.8.11.3 3.6 3.8.11.3 3.6 | 0.9.7.0 3.9 | 1.10.3.9 4.0 | 0.9.0.0 4. 0.10.0 4. 0.11.0.0 4. | 3.11.8.3 4. | 6.10.1.6 4. 6.11.3.0 4. 7.0.4.6 4. | 10.1.0.9 5. | 0.11.3.0 5. | 3.11.9.9 5.7 1.1.1.6 5.7 1.2.5.3 5.7 | 0.4.6 5.10 1.9.0 5.10 3.1.6 5.10 | 1.3.9.9 6. | 1.4.6.0 |
| 4.04 3.4 | 4.0.2.3 3.7 4.1.0.0 3.7 | 7.0.3.0 3.10 7.1.1.6 3.10 7.2.0.0 3.10 | 02.0.0 4.1 | .2,0.0 4. .3.0-0 4. | 4.2.126 4. 4.3.11.3 4. 4.5.0.0 4. | 7.1.6.0 4.1 7.2.7.0 4.1 7.3.9.0 4.1 7.4.10.0 4.1 | 0.3.5.3 S. 10.4.7.0 S. 10.5.0.0 S. | 1. 5. 6. 0 1. 6. 0. 0 1. 8. 0. 0 | 5.0.9 5.7. 6.4.6 5.7. 7.8.3 5.7. 9.0.0 5.7. | 5.10.6 5.10 7.3.0 5.10 8.7.6 5.10 10.0.0 5.10 | 0.6.8.3 6.1 0.8.1.6 6.1 0.0.6.9 6.1 | .7.6.0 .0.0.0 .0.6.0 |
| 3.4 3.4 5.0, 3.4 | 4.3.0 3.7 | 7. 3. 9. 0 7. 4. 7. 6 3. 10 1. 5. 6. 9 3. 10 | 0.4.10.6 4.1 | 7.0.0 4. | 4.7.1.6 4.7.1.6 4.8.2.3 4.9.3.0 4.9.3.0 | 7.6.0.0 4 7.8.3.0 4 7.9.4.6 4 7.0.4.6 4 | 0.0.6.0 5.1 0.11.0.0 5.2 | 1.40.6.0 5.4 1.11.9.0 5.5 | .0.11.3 5.8. .0.11.3 5.8. | 0.9.0 5.11. 2.1.6 5.11. 3.6.0 5.11. | 3.3.9 6.2 4.9.0 6.4 | .1.b.0 .3.0.0 .4.6.0 |
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| (| Current ! | | | NO A | | | | | | A TOP OF THE PROPERTY OF THE P | | |
| | | | | | 1 to | | | | | 3 | | |
| | | 6 4 1 | | 7 | The state of the s | | | | Theath E | } | | |

A-TABLE OF FEET AND INCHES
from 6 inches by 6 inches and 1 quarter to 2 foot 11 inches and 3 quarters by 9 inches.

| F.I.Parts F | 300 mg / 1 mg | Parte | FI Parte | FI Parte | F.I Parts | F.I Parts | F.I.Parts | F.I.Parts | F.I.Parts | F.I.Parts | F.I.Parts | F.I.Parts |
|---|--|---|---|--|---|--|--|---|--|--|--|--|
| | .I.Parts | DO SERVICE STREET STREET | 0.6 3 | | 074 | 0.72 | 0.7 } | 0.80 | 0.8.4 | 0.8 2 | 0.8.7 | 0.9.0 |
| | | 0.3.6.3.0 | | | | | | | | | | |
| 0.7.0 | 3.7.0.0 3.0.3.0 3.0.0.0 4.0.5.3 | 0.3.0.6.0 0.3.11.1.0 0.4.0.0.9 0.4.2.4.0 | 0.3.11.3.0 0.4.0.11.3 0.4.2.7.0 0.4.4.3.0 | | 0.4.4.0.9 | | 0.5.0.0.0 | | | | | |
| 0.8:0 | 4.2.0.0 4.3.0.0 4.5.1.0 4.6.8.3 | 0.4.4.0.0 0.4.5.7.6 0.4.7.3.0 0.4.8.6.6 | 0.4.6.0.0 0.4.7.8.3 0.4.0.4.0 0.4.11.0.9 | 0.4.8.0.0 0.4.9.9.0 0.4.11.5.0 0.5.1.3.0 | 0.4.0.0.0 0.4.11.9.9 0.5.1.7.6 0.5.3.5.3 | 0.5.0.0.0 0.5.1.10.0 0.5.3.0.0 0.5.5.7.0 | 0.5.3.11.3 0.5.5.10.0 0.5.7.9.0 | 0.5.4.0.0 0.5.6.0.0 0.5.8.0.0 0.5.40.0.0 | · COMPANIES CONTRACTOR | The second secon | | |
| 0.9.0 | 4.8.3.0 | 0.4.10.6.0 0.5.0.1.6 0.5.1.9.0 0.5.3.4.6 | 0.5.0.0.0 0.5.2.5.3 0.5.4.1.0 0.5.5.0.0 | 0.5.3.0.0 0.5.4.0.0 0.5.6.6.0 0.5.8.3.0 | 0.5.5.3.0 0.5.7.0.9 0.5.8.10.6 0.5.10.8.3 | 0.5.7.6.0 0.5.0.4.6 0.5.11.3.0 0.0.1.1.6 | 0.5.0.0.0 | 0.6.0.0.0 0.6.4.0.0 0.6.6.0.0 | 0.0.2.3.0 0.0.4.3.9 0.0.6.4.0 0.0.8.5.3 | | | 0.0.11.3.0 0.7.1.6.0 0.7.3.0.0 |
| 0.10.0 | 5.3.0.0 | 0.5.5.0.0 0.5.6.7.0 0.5.8.3.0 0.5.0.10.6 | 0.5.7.0.0 0.5.0.2.3 0.5.0.0.0 0.0.0.0.0 | 0.5.10.0.0 0.5.11.0.0 0.6.1.6.0 0.6.3.3.0 | 0.6.2.3.0 | 0.6.3.0.0 0.6.4.10.6 0.6.6.0.0 0.6.8.7.0 | 0.6.5.6.0 | 0.0.0.0.0 0.0.0.0.0 0.7.0.0.0 0.7.2.0.0 | 0.7.0.6.9 0.7.2.7.6 0.7.4.8.3 | | | |
| 0.11.04 0. | 5.8.0.0 | 0.5.11.6.0 | 0.6.2.3.0 | 0.6.5.0.0 0.0.6.0.0 0.6.8.0.0 0.6.0.3.0 | 0.6.7.0.0 0.6.9.6.0 0.6.11.4.6 0.7.1.2.3 | 0.6.10.6.0 0.7.0.4.6 0.7.2.3.0 0.7.4.1.6 | 0.7.1.3.0 0.7.3.2.3 0.7.5.1.0 0.7.7.0.0 | 0.7.4.0.0 0.7.6.0.0 0.7.8.0.0 0.7.0.0.0 | 0.7.6.0.0 0.7.8.0.0 0.7.10,10.0 0.8.0.11.3 | | | 0.8.3.0.0 0.8.5.3.0 0.8.7.0.0 0.8.0.0.0 |
| | 6.3.0.0 6.4.6.0 6.6.1.0 6.7.8.3 | 0.6.6.0.0 0.6.7.7.6 0.6.9.3.0 0.6.10.10.6 | 0.6.0.0.0 0.0.10.8.3 0.7.0.4.0 0.7.2.0.0 | 0.7.0.0.0 0.7.1.0.0 0.7.3.6.0 0.7.3.3.0 | 0.7.3.0.0 0.7.4.0.0 0.7.6.7.6 0.7.6.5.3 | 0.7.6.0.0 | 0.7.0.0.0 0.7.10.11.3 0.8.0.10.6 0.8.2.0.0 | 0.8.2.0.0 0.8.4.0.0 0.8.6.0.0 | 0.8.3.0.0 0.8.3.0.0 0.8.7.1.0 0.8.0.2.3 | | 0.8.0.0.0 | |
| 1.1.0 | 6.0.3.0 6.10.0.0 7.0.4.6 7.1.11.3 | 0.7.0.6.0 0.7.2.1.0 0.7.3.0.0 0.7.5.4.0 | 0.7.3.0.0 0.7.5.3.3 0.7.7.1.0 0.7.8.00 | 0.7.7.0.0 0.7.8.0.0 0.7.0.0.0 0.8.0.3.0 | 0.7.10.3.0 0.8.0.0.0 0.8.1.10.6 0.8.3.8.3 | 0.8.1.6.0 0.8.3.4.6 0.8.5.3.0 0.6.7.1.6 | 0.8-4.0.8 0.8.6.8.3 0.8.8.7.6 0.8.10.6.0 | 0.0.8.0.0.0 | 0.8.11.3.0 0.0.1.3.0 0.0.3.4.0 0.0.5.5.3 | 0.0.2.6.0 0.0.4.7.6 0.0.6.0.0 0.0.8.10.6 | 0.10.0.3.9 | 0. 9.0.0.0 0. 9.11 .3.0 0.10 .1 .6.0 0.10 .3 .0.0 |
| 1.2.0 | 7.3.6.0 | 0.7.7.0.0 0.7.8.7.0 0.7.10.3.0 0.7.11.10.0 | 0.7.10.6.0 0.8.0.2.3 0.8.1.10.0 0.8.3.6.9 | 0.8.2.0.0 0.8.3.0.0 0.8.5.6.0 0.8.7.3.0 | 0.6.5.6.0 0.6.7.3.0 0.6.0.1.0 0.6.0.1.3 | | | 0.0.4.0.0 | 0.9.7.6.0 0.9.9.6.9 0.9.11.7.6 0.10.1.8.3 | 0.0.11.0.0 | 0.10.2.6.0 0.10.4.8.3 0.10.6.10.6 0.10.0.0.9 | 0.10.6.0.0 0.10.8.3.0 0.10.10.6.0 0.11.0.9.0 |
| | 7.9.9.0 7.11.3.9 8.0.10.6 8.2.5.3 | 0.8.1.6.0 0.8.3.1.6 0.8.4.9.0 0.8.6.4.6 | 0.8.5.3.0 0.8.6.11.3 0.8.8.7.6 0.8.10.3.9 | 0.8.9.0.0 0.8.10.9.0 0.9.0.6.0 0.9.2.3.0 | 0.0.0.0.0 0.0.2.0.0 0.0.4.4.0 0.0.6.2.3 | 0.9.4.6.0 0.9.6.4.6 0.9.8.3.0 0.9.10.1.6 | 0.9.8.3.0 0.9.10.2.3 0.10.0.1.0 0.10.2.0.9 | 0.10.0.0.0 0.10.2.0.0 0.10.4.0.0 0.10.6.0.0 | 0.10.3.9.0 0.10.5.9.9 0.10.7.10.6 0.10.9.11.3 | 0.10.7.6.0 0.10.0.7.6 0.10.11.0.0 0.11.1.10.0 | 0.10.11.3.0 0.11.1.5.3 0.11.3.7.0 0.11.5.0.0 | 0.11.3.0.0 0.11.5.3.0 0.11.7.6.0 0.11.0.0.0 |
| 1.4.0 0.00.00.00.00.00.00.00.00.00.00.00.00 | | | 0.0.0.0.0 0.0.1.3.3 0.0.3.4.0 0.0.5.0.0 | 0.0.4.0.0 0.9.3.0.0 0.0.7.6.0 0.9.9.3.0 | 0.9.8.0.0 0.9.9.9.9 0.9.11.7.6 0.10.1.5.3 | 0.10.0.0.0 0.10.1.10.0 0.10.3.0.0 0.10.5,7.0 | 0.10.4.0.0 0.10.5.11.3 0.10.7.10.0 0.10.9.9.9 | 0.10.8.0.0 | 0.11.0.0.0 0.11.2.0.0 0.11.4.1.0 0.11.6.2.3 | 0.11. 4.0.0 0.11. 6.1.0 0.11. 8.3.0 0.11.10.4.0 | 0.11.0.2.3 1.0.0.4.0 1.0.2.6.9 | 1.0.2.3.0 1.0.4.6.0 1.0.6.0.0 |
| 1.5.0 | 8.11.9.9 9.1.4.6 9.2.11.3 | 0.0.2.6.0 0.0.4.1.6 0.0.5.0.0 0.9.7.4.6 | 0-0-0-0-0 0-0-8-5-3 0-0-10-1-0 0-0-11-9-9 | 0.0.11.0.0 0.10.0.0.0 0.10.2.0.0 0.10.2.0.0 | 0.10.3.3.0 0.10.5.0.0 0.10.6.10.6 0.10.6.6.3 | 0.10. 7. 6. 0 0.10. 0. 4. 6 0.10. 11. 3. 0 0.11. 1. 1. 6 | 0.10.11.9.0 0.11.1.8.3 0.11.3.7.0 0.11.5.0.0 | 0.11.4.0.0 0.11.6.0.0 0.11.8.0.0 0.11.10.0.0 | 0.11.8 3.0 0.11.10.3.0 1.0.0.4.0 1.0.2.5.3 | I manufacture the state of the | | 1.0.11.3.0 |
| 1.6.0 | 0.4.6.0 0.6.0.0 0.7.7.0 0.0.2.3 | 0.0.10.7.0 | 0.10.1.6.0 0.10.3.2.3 0.10.4.10.0 0.10.6.6.0 | 0.10.7.0.0 | 0.10.10.6.0 0.11.0.3.0 0.11.2.1.0 0.11.3.11.3 | 0.11.0.0.0.0 | | 1.0.0.0.0 1.0.2.0.0 1.0.4.0.0 1.0.6.0.0 | | | 1.1.3.0.0 | 1. 1.0.0.0 |
| 4 0. | 10.1.10.0 | 0.10.8.4.0 | 0.11.1.3.9 | 0.11.0.3.0 | 0.11.5.0.0 0.11.7.6.0 0.11.0.4.0 0.11.11.2.3 | 1.0.4.1.0 | 1.0.5.2.3 | 1.1.2.0.0 | 1.1.2.0.0 | 1.1.5.6.0 | 1.1.10.3.0 1.2.0.5.3 1.2.7.0 1.2.4.0.0 | 1. 2. 3. 3. 0 1. 2. 7. 6.0 1. 2. 9. 9.0 |
| 1 · 5 · 0, 0. | 10.5.0.0 10.6.6.0 10.8.1.6 10.9.8.3 | 0.10.10.0.0 0.10.11.7.6 0.11.1.3.0 0.11.2.10.0 | 0.11.3.0.0 0.11.4.8.3 0.11.6.4.8 0.11.6.0.9 | 0.11.8.0.0 0.11.0.0.0 0.11.11.0.0 1.0.1.3.0 | 1.0.6.5.3 | 10.9.00 | 1.1.2.10.0 | 1.1.10.0.0 | | MARKET AND ARREST | 1.27.0.0 | 3.2.3.0 3.4.0.0 3.6.0.0 |
| 4, 0. | 11 240 | 0.11.4.6.0 0.11.6.1.6 0.11.7.9.0 0.11.9.4.6 | 0.11.0.0.0 0.11.11.5.3 1.0.1.1.0 1.0.2.0.0 | 1.0.4.0.0 | 1.0.10.0.0 | 1.1.3.4.0 | IIIAAA | 1.2.2.0.0 1.2.2.0.0 1.2.4.0.0 1.2.6.0.0 | | 1.3.0.7.0 | - | 1. 3.0.0 1. 4.1.0.0 1. 4.3.0.0 |
| 3 0. | 11.7.0.0 | 0.11.11.0.0 1.0.0.7.6 1.0.2.3.0 1.0.3.10.6 | 1.0.6.2.3 | 1.0.11.0.0 1.1.1.0.0 1.1.3.3.0 | 1. 1.8.11.3 | 1,2,2,7,0 | 1.2.6.4.0 | 1.2.8.0.0 1.2.0.0.0 1.3.0.0.0 1.3.2.0.0 | 1.3.3.0.0 1.3.3.7.6 1.3.7.6.3 | 1.3.7.0.0 1.3.0.1.0 1.3.11.3.0 1.4.1.4.0 | 1. 4.2.8.3 | 48.3.0 4.0.0.0 5.0.0.0 |
| 15 | 0.4.5.3 | 1.0.7.1.6 | 1.1.4.3.0 | 1.1.8.6.0 | 1. 2. 4.2,3 | 1.2.6.4.6 | | 1.3.6.0.0 | 1.3.0.0.0 1.3.11.0.0 1.4.1.10.6 1.4.3.11.3 | 1.4.3.0.0 1.4.5.7.6 1.4.7.0.0 1.4.0.0.6 | 1. 4.9.3.0 1. 411.5.3, 1. 5.1.7.0 1. 5.3.0.0 | 1.5.530 1.5.7.60 1.5.0.00 |
| 4 1. | 0.7.6.0 | 1.1.4.10.0 | 1.1.7.8.3 | 1.2.1.0.0 | 1.2.7.0.0 | AND DESCRIPTION OF THE PARTY OF | 1.3.0.10.0 | 1.4.0.0.0 | 1.4.0.0.0 1.4.8.0.0 1.4.30.1.6 1.5.0.2.3 | 1.5.2.1.0 | 1.5.6.0.0 1.5.6.2.3 1.3.0.4.0 1.6.0.6.0 | 1.0.2.3.0 1.0.2.3.0 1.0.6.0.0 |
| 2.1.0 | | 1.1.8.1.6 | 1.2.0.0.0 1.2.2.5.3 1.2.4.1.6 1.2.5.9.0 | 1. 2.8.0.0 1. 210.6.0 1. 3.0.3.0 | 1.3.3.0.0 1.3.4.6.6 1.3.6.8.3 | 1.3.7.6.0 1.3.9.4.6 1.3.11.3.0 1.4.1,1.6 | 1.4.3.8.3 | | 1.5.4.3.9 1.5.6.4.6 1.5.8.5.3 | 1.5.8.0.0 1.5.10.7.0 1.6.0.9.0 1.6.2.10.0 | 1.6.44.3 1.6.7.1.6 1.6.9.3.0 | 1. 6.11.3.0 1. 7. 3.0.0 1. 7. 3.0.0 |
| 2.2.0 | 1.8.0.0 | 1. 2. 1. 0. 0 1. 2. 2. 7. 0 1. 2. 4. 3. 0 1. 2. 5. 10. 0 | 1.2.7.6.0 1.2.0.2.3 1.2.10.10.6 1.3.0.6.0 | 1.3.3.0.0 | 1.3.8.8.0 | 1.4.3.0.0 1.4.4.0.0 1.4.6.0.0 1.4.6.7.0 | 1.4.11.5.3 | 1.5.4.0.0 1.5.8.0.0 1.5.8.0.0 | 1.0.0.0.0 | 1.6.3.0.0 | 1.7.1.8.3 | 1. 7.8.3.0 1. 7.10.0.0 1. 8.0.0.0 |
| 2.3.0 | 2.3.0.6 | 1.2.7.6.0 1.2.9.1.6 1.2.0.0.0 1.3.0.4.0 | 1.3.7.3.9 | 1.3.0.0.0 1.3.10.0.0 1.4.0.6.0 1.4.2.3.0 | 1. 4.3.0.0 1. 4.5.6.0 1. 4.7.4.6 1. 4.0.2.3 | 1.5.0.4.6 | 1.5.7.2.3 | 1.6.2.0.0 | 1.6.6.6.6.6 | 1.7.3.7.6 | 1.7.10.3.3 | 8.3.3.0 1.8.7.0.0 1.8.0.0.0 |
| 2.4.0 | 2.8.6.9 2.0.1.6 2.11.8.3 | 1.3.3.7.6 | 1.3.0.0.0 1.3.0.8.3 1.4.0.4.0 1.4.2.0.0 | 1. 4. 4. 0. 0 1. 4. 5. 0. 0 1. 4. 7. 6. 0 1. 4. 0. 3. 0 | 1.4.11.0.0 1.5.0.0.0 1.5.2.7.0 1.5.4.5.3 | 1.5.0.0.0 1.5.7.10.0 1.5.0.0.0 1.5.11.7-0 | 1.6.2.11.3 | 1.6.10.0.0 | 1.7.3.0.0 | 1.8.0.1.6 | 1.8.7.2.3 | 1. 0.2.3.0 1. 0.4.0.0 1. 0.0.0.0 |
| | | | 1.4.5.5.3 | 1.5.0.0.0 1.5.2.6.0 1.5.4.3.0 | 1.5.0.3.0 1.5.8.0.0 1.5.9.10.0 1.5.11.8.3 | 1.6.3.4.6 | 1.0.10.8.3 | 1.7.6.0.0 | 18.3.4.6 | 1.8.8.7.6 | 1.0.3.11.3 | 1.0.1.0.0 |
| | | 1.4.4.7.6 | 1.4.10.6.0 1.5.0.2.3 1:5.1.10.0 1.5.3.6.0 | 1.5.7.0.0 | 1.6.1.6.0 1.6.3.3.9 1.6.3.1.6 1.6.6.11.3 | 1.7.0.0.0 | 1.7.6.5.3 | 1.0.2.0.0 | 1.8.9.6.0 | 1.0.5.1.6 | 1.0.0.8.3 1.0.2.00 1.0.5.0.0 | 1. 10.8.3.0 1. 10.30.0 1. 11.0.9.0 |
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| 2.8.0 | 4.0.0.0 4.11.1.0 5.0.8.3 | 1. 5.4.0.0 1. 5.5.7.6 1. 5.7.3.0 1. 5.0.0 | 1.6.1.8.3 1.6.8.4.0 1.6.5.0.0 | 1.6.8.0.0 1.6.0.0.0 1.6.11.6.0 1.7.1.3.0 | 1. 7.4.0.0 1. 7.5.0.0 1. 7.7.7.6 1. 7.0.5.3 | 1.8.3.9.8 | 1.8.11.0.0 | 1.0.0.0.0 | 1.10.2.0.0 | 1. 11.0. 3.0 | 1.11.6.2.3 | 2.0.2.3.0 2.0.4.0.0 2.0.6.9.0 |
| | 5.2.3.0 5.3.0.0 5.3.4.0 5.0.11.3 | 1.5.0.0.0 1.6.0.1.0 1.6.1.0.0 1.6.3.4.0 | 0.0.0.0 | 1.7.4.0.0 1.7.6.6.0 1.7.8.3.0 | 1. 7. N. 3.0 1. 6. 1. 0.0 1. 8. 2. 10.0 1. 6. 4. 6.3 | 1.8.0.4.0 | 0.3.0.3 | 1.10.2.0.0 | 1.11.0.4.0 | 1.11.6.7.6 | 2.0.0.0.0 2.0.2.11.3 2.0.5.1.0 2.0.7.3.9 | 2.0.11.3.0 2.1.1.0.0 2.1.3.9.0 |
| | 5.8.8.0 5.10.0.0 5.11.7.0 6.1.2.3 | . 6.5.a.0 . 6.6.3.0 . 6.9.0.0 | 7.3.2.3 | 1.7.11.0.0 | 1.0.0.0.0 1.0.0.3.9 1.0.10.1.0 1.0.11.11.3 | 0.40.0 | 1.10.1.5.3 | 1.10.10.0.0 | 1.11.0.6.0 | 20 6.3.0 | 2.0.9.6.0 2.0.11.8.3 2.1.1.0.0 2.1.4.0.9 | 9.1.8.3.0 9.2.0.00 9.2.0.00 |
| 2.11.04 | 6 2 0 0 6 43 9 6 5 10 6 6 7 5 3 | 7.2.0.0 | 1.7.0.3.0 | 1.6.6.0.0 | 1 9 3 0 0 1 9 3 0 0 1 9 5 4 0 1 9 7 2 3 | 1,10.0.4.6 | 1.10.0.2.3 | 1.11.2.0.0 | 10.2.0.0 20.4.00 20.6.11.3 | 2.0.11.7.0 | 9.1.0.3.0 9.1.0.3.3 9.1.10.7.0 9.2.0.9.0 | 9. 2. 3.0.0 9. 2. 3.30 9. 2. 7.0.0 9. 2. 9.90 |

A TABLE OF FEET AND INCHES. from 3 foot by 6 inches and 2 quarter to 5 foot 5 inches and 3 quarters by 9 inches ELParts ElParts

| FIParts | F.I.Parts | F.I.Parts | EI.Parts | E.I.Parts | F.I.Parts | LINE SERVICE MARKETINESS | | | EVENT OF THE PARTY OF | | FI.Parts | F.I.Parts |
|---------------|--|---|---|---|--|--|---|---|---|--|--|---|
| 1.1.2 | 0.6.4 | 0.6.4 | 0.6.3 | 0.7.0 | ALCOHOL: | | 经过多度 / 经国际政场通信 | 0.8.0 | SECTION OF STREET | CONTRACTOR STATE | 2.2.3.0.0 | 23.0.00 |
| 3.0.0 | 1.0 100 0 | 7690 | 1.8.3.0.0 1.8.4.8.3 1.8.6.4.6 1.8.8.0.9 | 03.00 | 1.007.0 | 1.107.106 | 1.11.6.10.6 | 2.0.2.0.0 | 201109 | 2.1.8.1.6 2.1.103.0 2.2.0 4.6 | 22523 | 23 23 0 23 4.60 23 600 |
| 3.1.5 | 17330 | 18.0.60 | 18.99.0 | 19890 | 1.10.43.0 1.10.6.0.9 1.10.7.100 1.10.9.83 | 1.11.6.0 | 1.11.10g.0 2.0.0.8.3 2.0.2.7.6 2.0.4.6.9 | 20800 | 21530 | 222600 | 221190 231113 23539 | 23.000 |
| 9.0.03 | 17.060 | 1.8.7.00 | 1.9.46.0 | 1.10 2 0.0 | 1.10.116.0 | 1.11.9.0.0 | 20.6.60 20.8.5.3 20.10.4.6 2.1.0.3.9 | 2.1.4.0.0 2.1.6.0.0 2.1.8.0.0 2.1.10.0.0 | 22369 22376 225783 | 2211.00 2311.0 23333.0 23546 | 23.8.6.0 23.10.83 240.10.6 243.0.0 | 2.46.0.0 2.48.3.0 2.410.0.0 2.5.0.9.0 |
| 3.3.0 | 18390 | 19.1.60 | 1.9.113.0 1.10.0.11.3 1.10.2 7.6 1.10.43.9 | 1.10 0.0.0 | 1.116.0.0 | 2.04.60 2.06.46 2.08.30 2.010.16 | 2.1.23.0 2.1.4.23 2.1.6.1.6 2.1.8.0.9 | 2.2.0.0.0 2.2.2.0.0 2.2.4.0.0 2.2.60.0 | 22990 221199 231106 233113 | 23760 | 24530 24753 24976 24199 | 25.3.0.0 25.5.3.0 25.7.0.0 25.9.0.0 |
| 3.4.0 | 1.8.10.00 | 1.9.8.0.0 | 1.10.6.0.0 | 1.11-4.0.0 | 2.0.2.0.0 2.0.3.0.9 2.0.57.6 2.0.7.53 | 21.0.0.0 21.1.106 21.3.9.0 21.3.7.6 | 2.1.10.0.0 2.1.11.11.3 2.21.10.6 2.23.09 | 2.2.8.0.0 2.2.00.0 2.3.0.0.0 2.3.2.0.0 | 23.6.0.0 23.8.0.9 23.10.1.6 2.4.0.23 | 2.4.6.1.6 2.48.3.0 2.410.46 | 2.5.4.2.3 25.6.4.6 25.8.6.9 | 26.23.0 26.46.0 26.69.0 |
| 3.2.0 | 19.59.9 | 1.1026.0 | 1.11.0.9.0 | 1.11.11.0.0 | 2.0.9.3.0 | 2.1.7.6.0 | 22.5.9.0 2.2.7.8.3 2.2.9.7.6 2.2.11.6.9 | 23.400 23.600 238.00 23.000 | 2.4.23.0 2.4.63.6 2.4.64.6 2.4.8.53 | 25.0.0.0 25.2.7.6 25.4.9.0 25.6.106 | 25.00.9.0 26.0.11.3 26.3.1.6 26.5.3.9 | 2.6.11.3.0 |
| 3.6.0 | 1.10.0.0.0 | 1.10.90.0 | 1.11.7.6.0 | 20000 | 2.1.6.3.9 | 2.23.00 | 23.3.53 23.5.4.6 | 2.4.0.0 2.4.4.0.0 2.4.6.0.0 | 25.0.6.0 | 25.11.1.6 26.1.3.0 26.3.46 | 2.69.8.3 | 2.7.8.3.0 |
| 3.7.2 | 1.10.4.9.0 | 1.113.60 | 2.02.3.0 | 21.200 | 2.2.1.6.0 | 221000 | 23.93.0 23.1123 2.41.16 2.43.09 | 2.48.0.0 2.410.0.0 2.5.0.0.0 2.5.2.0.0 | 258.90 | 26776 | 27633 27876 271099 | 28.5.3.0 28.7.6.0 28.9.0.0 |
| 9.8.0 | 1.10.11.0.0 | 1.11.1.7.6 | 2.0.9.0.0 | 21800 | 22700 | 237106 | 246119 | 25600 | 2.6.5.0.9 | 27.63.0 | 28.3.2.3 28.5.4.6 28.7.60 | 29.23.0 |
| 3.3.5 | 1.11.53.0 | 2.04.6.0 | 21390 | 22300 22400 2260 22820 | 23.40.9 23.510.6 23.783 | 24346 | 25283 | 2.6.2.0.0 | 2.7.1.3.9 | 28.0.7.6 28.2.9.0 28.4.106 | 28:11:11.3 2.9.2.1.6 29.4.3.9 | 2.0.1.6.0 |
| 3.10.04 | 2.0.1.0.0 | 2.011.0.0 | 2.1.10.6.0 2.2.0.2.3 2.2.1.10.6 2.2.3.6.9 | 2·2·10·00 2·2·11·0·0 2·3·1·6·0 2·3·3·3·0 | 23.0.00 23.11.3.0 2.4.1.16 2.4.2.113 | 2.4.0.006 2.5.0.0.0 2.5.2.7.6 | 25.10.53 2.6.0.40 2.6.2.3.9 | 2.0.0.0.0 | 27.0.6.9 | 2.8.9.1.0 2.8.113.0 2.9.1.4.0 | 2.9.8.8.3 2.9.10.10.6 2.10.1.0.9 | 2.10.8.3.0 2.10.10.6.0 2.11.0.9.0 |
| 2 | 2.0.5.9.0 | 2.1.5.6.0 | 2.2.5.3.0 | 23.5.0.0 | 2 4 4 0 0 2 4 6 0 0 2 4 8 4 0 | 2.5.6.46 | 2.6.8.1.6 | 27.60.0 | 28.500 | 29.7.9.0 | 2103.3.0 | 211.0.0.0 |
| 4.0 . 03 | 2.1.1.6.9 | 2.2.0.0.0 | 23.000.0 | 2.4.0.0.0 2.4.1.9.0 2.4.3.6.0 2.4.53.0 | 2.5000 2.5199 2.5376 2.5376 | 2.6.1.10.6 | 27.3.00 | 2.8.2.0.0 2.8.4.0.0 2.8.6.0.0 | 2.9.2.0.9 | 210.2.1.6 | 211.2.2.3 | 3.0.2.3.0 3.0.4.6.0 3.0.6.9.0 |
| 4.1.0 | 2.1.6.3.0 | 2.2.6.6.0 2.2.8.1.6 2.29.00 2.24.4.6 | 2.3.6.9.0 | 2.4.7.0.0 2.4.8.0.0 2.4.10.60 2.5.0.3.0 | 25730 25909 2510106 26083 | 26.11.3.0 | 27.9.83 | 2.8.10.0.0 2.9.0.0.0 2.9.2.0.0 | 2.0.10.3.9 2.10.0.4.0 2.10.2.53 | 210.107.0 | 3.0.1.1.0 | 3.0.11.3.0 |
| 4.2.0 | 2.2.0.60 | 23.2.7.6 | 2.41.6.0 | 25.2.0.0 | 2.6.26.0 | 2.7.3.0.0 | 28 5 53 | 2.9.6.0.0 2.9.8.0.0 2.9.10.0.0 | 2.10.6.60 | 211.9.1.0 | 3.0.783 | 3.1.83.0 |
| 4.3.04 | 2.2.6.9.0 | 237.00 | 249113 | 25.1090 | 2.6.11.6.9 | 28.0.4.6 | 2.9.3.1.0 | 2.10.2.0.0 | 2.11.2.9.0 | 3.0.3.7.0 | 31.853 | 3 2 5 3 0 |
| 4.4.04 | 2.3.1.00 | 2.4.2.0.0 | 2 5 4.8.3 2 5 6.4.6 | 2.6.3.00 | 27.6.9.9 | 28.7.10.6 | 29.8.11.3 | 2.11.10.0.0 | 3.0.1.1.0 | 31.0.16 | 3.2.1.2.3 | 3.3.2.3.0 |
| 4.5.0 | 23.23.0 | 2.4.10.1.6 | 2.50.0.0 | 2.7.0.0.0 | 2.8.2.0.0 | 29346 | 210.4.83 | 2.11.6.0.0 | 3.0.73.9 | 3.1.8.7.0 | 3.2.0.1.3 | 3.3.11.3.0 |
| 4.6.0 | 2.4.1.60 | 25300 | 26.46.0 | 27.000 | 28.7.0.0 | 2.9.10.10.6 | 2.11.0.53 | 3.0.2.0.0 | 3.1.3.6.9 | 32.73.6 | 3.3.6.8.3 | 3.4.0.60 |
| 4.7.8 | 2.4.7.9.0 | 2.5.9.6.0 | 2.7.0.11.3 | 2.8.1.0.0 | 2.9.2.6.0 | 2.10.6.4.6 | 211.8.23 | 3.0.00.0 | 3.2.1.10.0 | 33.3.0.0 | 3 43 53 | 3.5.9.90 |
| 4.8.01 | 25.2.0.0 | 2.6.40.0 | 27.60.0 | 28.8.0.0 | 2.9.11.9.9 | 2.11.0.0.0 | 303113 | 3.1.6.0.0 | 3.28.09 | 3.310.1.6 | 3.5.2.4.6.9 | 3.6.4.60 |
| 4.9.0 | 25.83.0 | 270160 | 2.8.2.53 2.8.4.1.6 2.8.5.9.9 | 2.9.3.0.0 2.9.6.60 2.9.83.0 | 2.10.3.3.0 | 2.11.9.46 2.11.11.3.0 3.0.1.3.6 | 3.041.83 | 3.2.2.0.0 | 33.43.6 3.3.6.4.6 3.3.8 5 3 | 3.48.9. | 3.5.11.1.6 | 3.7.1.6.0 |
| 4.10.014474 | 2.6.2.6.0 2.6.4.0.9 2.6.5.7.6 2.6.7.2.3 | 27.50.0 27.67.6 27.8.3.0 27.9.10.6 | 2.8.7.6.0 2.8.9.2.3 2.8.1010.0 2.90.6.9 | 2.0.1000 | 2.11.2.3.9 2.11.4.1.6 2.11.5.11.3 | 3.04.00 | 31753 | 3.2.10.0.0 | 3.4.0.6.9 3.4.2.7.0 3.4.4.8.3 | 3.5.3.3.6 | 3.6.7.10.6 | 3.7.8.3.0 |
| 4.11.04.54 | 2.6.103.9 | 28.2.00 | 29.23.0 293.113 29.57.6 29.73.9 | 2.10.6.9.0 | 2.11.9.6.9 2.11.11.46 3.0.1.23 | 3.1.0.4.6 | 3.2.5.1.0 | 3,3.10.0.0 | 3.5.0.11.3 | 13.03.00 | 37.03.0 | 0.099 |
| 2. 0. O. SA | 27.300 27.469 27.61.6 27.783 | 28.6.0.0 | 2.9.9.0.0 2.9:108:3 2.10.0:4.6 2.10.2:0.9 | 2.11.5.3.0 | 3.0.4.9.9.3.0.67.6 | 3.1.7.10.6 | 3.2.10.11.3 | 3.4.2.0.0 3.4.5.0.0 | 3.5.5.0.0 | 3.6.10.3. | 38.3.8.3 | 3.9.00.0 3.9.23.0 3.9.4.60 3.9.69.0 |
| 2.1.0 | 27.930 | 2.0.0.6.0 | 21039.0 | 2.11.8.0.0 | 3.1.0.00 | 3 2 3 4 6 | 33870 | 3.410.0.0 | 3.6.3.4.6 | 3 7 6 9 6 | 3.8.10.1. | 3.10.1.6.0 |
| Post to | 2.8.5.0.9 2.8.5.7.0 2.8.6.7.0 2.8.8.23 | 2.9.7.0.0 | 2.11.0.2.3 | 3.03.00 | 3 173.8 | 3.30.0.0 | 3.4.2.5.3 | 3.5.0.0.0 | 3.6.11.7.0 | 38333 | 3.9.0.0 | 3.10.10.00 |
| 2.8.0 | 2.8.11.3.0 | 2.10.1.0.0 | 2.11.6.119 | 3.0.000 | 32269 | 33 8 3 0 | 3.4.0.23 | 3.0.2.0.0 | 37590 | 3.8.11.9. | 3.10.3.7 | 3.11.7.00 |
| 5.4.03 | 2.9.400 2.9.5.69 2.9.7.1.6 2.9.8.3 | 2.108.0.0 2.109.7.6 2.10.113.0 2.11.0.10.6 | 3.0.0.0.0.0 3.0.4.6 3.0.5.0.9 | 3.1.40.0 | 3.2.0.0.0 | 3.4.10.0 | 3.5.9.9.9 | 3.7.0.0.0 | 3.8.2.0.0 3.8.4.1.0 3.8.6.2.3 | 3.0.8.3. | 3.10.102.3 | 4.00.00 4.0.2.3.0 4.0.4.0 4.0.6.0 0 4.0.6.0 |
| P.S. S. S. S. | 2.01.00 | 2.11.2.6.0 | 3 0 6 9 0 3 0 10 10 0 3 0 11 9 9 | 3.2.2.0.0 | 3.3.5.0.0 | 34046 | 363.60 | 3.7.8.0.0 | 3.8.10.3.0 3.9.0.40 3.9.2.53 | 3.10.2.7. | 3.11.6.113 | 41.160 |
| | Element St. | | | | | D | to the same | A STATE OF THE PARTY OF | The state of the | Con an action | | 1 |

A TABLE OF FEET AND INCHES. from 5 foot in inches and 3 quarters by 9 inches

| | I. | ET D. | FIR | irre | NEI D | unches an | EID | WEID ! | PIP. | thes and 3 | | (property and the second | IFID: | |
|---|-----|------------|---|--|--|---|--|---|---|--|--|---|--|---|
| | | ritary | 0.6.3 | 0.6.4 | 0.6.3 | 0 · 7 · 0 | 0.7.5 | 0.7 · 4 | 0.7.3 | 0:8:0 | | | 0.8.3 | F.I.Part |
| | | 5.6.0 | 210.4.6.0 | 311.1076 | 3.1.1.6.0 | 3-2-6.0.0 | 3.3.10.6.0 | 3 5 3 0 0 | 图 1 100000007 / 图 表示的 | CONTROL OF THE PROPERTY OF THE | MATERIAL STREET, STREE | 在 上海的医主动及后部内 | THE RESIDENCE OF THE PARTY OF T | 41.6.0 |
| | | 5.7.9 | 210.00.00 | 30.1.10.6 | 31.8.3.0 | 3.34.0.0 | 343.113 | 3.5.8.7.6 | 37.39 | 3.8.8.0.0 | 3.10.0.9.0 | 311.5.6.0 | 4.0.103.0 | 4.2.3.0. |
| | | | | | | | | | | | | | | |
| | = | 3.0.8 | 211.98.1.6 | 3-1-2-10.6 | 3.2.8 09 | 3.4.13.0 | 3.5.6.53 | 3.6 7.4.6 | 38.2.106 | 3.9.8.0.0 | 3.11.3.2.3 | 4.0.6.3.0 | 4-2-3- 9-0 | 439.0 |
| | 100 | 5-10-0 | 3.0.2.4.6 | 3.1.7.9.0 | 3.3.4.6.0 | 3.4.0.0.0 | 3.6.18.3 | 37.53.0 | 38.10.76 | 3.10-8.0.0 | 3.1.0.4.6 | 41.7.0.0 | 43.0.6.0 | 44.39 |
| | | 2.11 · 0 | 3.0.10.20 | 3.2.2.3.0.6 | 3.3.7.19.6 | 3.5.3.3.0 | 3.6. 8.11.3 | 3.8.0.9.0 | 39.8.3.9 | 3.11.2.0.0 | 407.83 | 423.6.0 | 43.28.3 | 4.4.8.3 |
| | | | 2.1.6.0.0 | 30.0.0.0 | 2.4.6.00 | 2.6.min # | 276.00 | 2.000 | 240.6.00 | 1.0.0 00 | 14.6 0.0 | 124:00 | 4.6.00 | |
| | | 24 | 3.1.9.1.6 | 333330 | 34946 | 3.63.6.0 | 3.7.79.0 | 3.9.3.9.0 | 3-10-7-11-3 | 4.0.0.0.0 | 4.1.10.1.6 | 43.4.3.0 | 4.4.8.2.3 4.4.10.4.6 4.5.0.6.9 | 46.66 |
| | | 34 | 3.2.1.0.9 | 33.0.00 | 3.5.4.1.0 | 3.6.10.6.0 | 3.8.3.0.0 | 3.9.11.3.0 | 311.5.7.6 | 4.0.0.0.0 | 4.2.4.3.9 4.2.6.4.6 4.2.8.5.3 | 43.10.7.6 | 45.4.11.3 | 40.00 |
| | L | 0.044 | 3.2.6.0.0 3.2.6.0.9 3.2.9.7.6 3.2.11.2.3 | | | 37.2.0.0 37.39.0 3.7.5.0.0 3.7.5.3.0 | 3.8.8.0.0 3.8.10.3.0 3.0.0.1:6 3.0.1.11.3 | 3.10.3.0.0 3.10.4.10.6 3.10.6.9.0 3.10.8.7.6 | 3.11.11.53 4.0.1.46 4.0.3.3.9 | 4.1.6.0.0 | 4.3.0.6.9 43.2.7.6 43.4.8.3 | 445.00 447.1.6 4403.0 4411.46 | 4.6.11.6.0 4.6.1.8.3 4.6.3.10.6 4.6.6.0.9 | 4.7.6.0.6 4.7.8.3.6 4.7.10.6.6 4.8.0.9 |
| | | 34 | 3.3.2.3.9 | 3.4.7.6.0 3.4.9.1.6 3.4.109.0 3.5.0.40 | 363113 | | | | | | | | | |
| | 6 | 4 . 04 424 | 3-3-10-1-0 | 3.5.2.0.0 3.53.7.6 3.53.3.0 3.55.10.6 | 3.6.0.0.0 3.6.108.3 3.7.0.4.6 3.7.2.0.9 | 38.4.00 38.5.9.0 38.7.6.0 38.9.3.0 | 3.9.11.0.0 3.10.09.9 3.10.2.7.6 3.10.4.53 | | 41.1.0.0 41.2.113 41.4.106 41.6.09 | 428.0.0 42.00.0.0 43.0.0.0 43.2.0.0 | 4.43.00 4.45.0.9 4.47.1.6 4.49.23 | 4.5.10.0.0 4.6.0.1.6 4.6.2.3.0 4.6.4.4.6 | 475.0.0 47.7.2.3 47.0.4.6 47.11.6.0 | 40.0.00 |
| | 6 | 5.04 | | 3.5.8.6.0 3.5.10.1.6 3.5.11.9.0 3.6.1.4.6 | 373.9.0 375.5.3 377.0 3789.9 | 3.8.11.0.0 3.9.0.9.0 3.9.2.6.0 3.9.4.3.0 | 3.10.6.3.0 3.10.8.0.0 3.10.0.186 3.10.1183 | 4. A. P. D. A. | 10 0 4.6 | 1 - 0.0 | 4:411.3.0 4:51:3:9 4:59:46 4:56:53 | 46.6.6.0 40.8.7.6 46.10.9.0 47.0.106 | 48.1.0.0 48.3.113 48.6.1.6 48.83.0 | 49.11.3. |
| | 6 | 6. 9 | 3.4.9.0.9 | 3.6.3.0.0 | 37.106.0 | 3.0.6.0.0 | 3-11-1-6-0 | 40.0.00 | 42.46.0 | 4.4.0.0.0 | 45.76.0 45.9.6.9 45.117.6 46.18.7 | 4.7.3.00 | 49.0.8.3 | |
| | 6 | 14 | 3.5.1.0.0 | 3-6-0-6-0 | 3.8 - 5:3 -0 | 3-10-1-0-0 | 3.118.0:0 | 4.1.4.6.0 | 43.0.3.0 | 4.4.8.0.0 | 4.6.3.0.0 | 4.7.11.6.0 | 49.7.3.0 | 4.11.3.0.0 |
| Column | 6 | | 3.58.00 | 3.3.4.0.0 | 3.0.0.0.0 | 3.108.00 | 4.0.4.0.0 | 12:0.00 | 13.8.00 | 1.5.1.0.0 | 1.7. 0:00 | 18.8. 11 | 4.10.4.0.0 | cana |
| Colored Colo | 6 | ·0 · 0 | 3.6.2.3.0 3.6.3.9.9 3.6.5.4.6 | 3.7.10.6.0 | 3-0-6-0-0 | 3-11-3-0-0 | 4.041.3.0 | 42.7.6.0 | 443.00 | 4.6.0.0.0 | 4.7.8.3.0 | 40.4.6.0 | 411.0.0.0 | 5.0.0.0.0 |
| | 6 | | 3.6.8.6.0 | 38:5.00 | 3-10-1-6-0 | 2-11-10-0-0 | 4.1.6.6.0 | 4.3.3.0.0 | 4:4:11.8.0 | 1.6.8 0.0 | 18 1.6.0 | 410.1.00 | 411.0.6.0 411.11.83 5.0.1.10.6 | 5.1.6.04 |
| 10 | 6 | 1 | 3.7.2.0.0 | 3.8-11-6-0 | 3.108.3.0 | 4.0.5.0.0 | 42.1.90 | 4.3.10.60 | 45730 | 47.6.0.0 | 4.0.0.00 | 4109.60 | 5.0.6.3.0 5.0.8.53 50.107.6 | 5.2.3.00 |
| 7.1. 0 | 7 | .0.0 | 3.7.0.00 | 306.00 | 3.11.3.0.0 | 4.1.0.0.0 | 10.0.00 | 1.1.6.0.0 | 1.63.00 | 48.0.0.0 | 40.0.0.0 | 4.113.10.0 | 51.3.0.0 | 5.3. 2.3.0 5.3. 2.3.0 5.3. 4.0.0 |
| 7 2 9 3 5 0 0 0 0 0 5 0 0 0 0 0 0 0 0 0 0 0 0 | 7 | | | | | | | | | | 410:53:0 | 5.0.2.6.0 | 51.0.60 | 5.3.0.0.0 |
| 7 3 9 3 9 3 9 3 11 6 0 4 1 7 8 9 4 4 1 7 8 9 4 4 1 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8 | 7 | .8.0 | 3.8.9.60 | 3.10.7.0.0 | 4.0.4.6.0 | 4.2.2.0.0 | 4.3.11.6.0 | 4.5.9.0.0 | 47.6.6.0 | 4.94.0.0 | 4.11.1.6.0 | 5.0.11.0.0 | 5.2.6.3.0 | 5.4.6.0.0 |
| 7 4 9 38 10 9 0 31 18 0 0 41 18 3 0 45 3 0 45 3 0 45 3 0 45 3 0 0 0 45 3 0 0 45 3 0 0 45 3 0 0 45 3 0 0 45 3 0 0 45 3 0 0 45 3 0 0 0 45 3 0 0 0 45 3 0 0 0 45 3 0 0 0 45 3 0 0 0 45 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 7 | 3. 2 | 39.2.2.3 | 310.11.6.0 | 40.9.09 | 427.3.0 | 44.4.11.3 | 4.0 2.7.0 4.6.4.60 | 48.2.3.0 | 410.0.00 | 411.9.9.0 | 5.1.7.6.0 | 53.3.0.0 | 5.5.0.0.0 |
| 7 5 9 3 10 23 0 40 26 0 42 50 0 42 100 0 45 100 0 45 100 0 45 100 0 51 200 0 51 200 0 52 100 0 52 50 13 50 13 0 52 100 0 52 50 13 50 13 0 52 100 0 52 50 13 50 13 50 13 0 52 50 13 50 1 | 7 | | 3.9.10.0.0 | 3118.0.0 | 41 6.0.0 | 4340.0 | 4.5.2.0.0 | 4.7.0.0.0 | 48.10.0.0 | 4108.0.0 | 5.0.6.0.0 | 52.4.00 | 53.110.0 54.2.0.0 54.4.2.3 | 5.6.2.30 |
| 7.6. Q 3.00.60 | 7 | | 3.10.2.8.3 | 4.0.010.6 | 41.11.00 | | | | 49399 | 4.11.2.0.0 | 5.1.2.3.0 | 53.0.6.0 | F F. 0 100 | 5.6.9.0.0 5.6.9.0.0 |
| 7.7.9 311450 41360 43313 45160 45160 45160 46160 4600 4600 4600 500 500 500 500 500 500 500 500 500 | 7. | 6.0 | | 4.0:0.0.0 | 42.7.6.0 | | | | | 5.9.0.0.0 | 5.1.6.4.6 | 53.4.0.0 | 55.53.1.6 | |
| 7.8.9 3.11.10.0 41.10.0 43.0 83 453.6 453.6 453.6 453.6 452.113 44.12.7 840.0 83.3 83 83 83 83 83 83 83 83 83 83 83 83 83 | 7. | | 3.11.3.2.3 | 41.7.6.0 | 43.0 6.0 | 4.51.00 | 468.1.6 | 4.8 6.9.0 48.8.7.6 48.10.60 | 410.3.46 | 5.0.8.0.0 | 5.2.2.7.6 | 5.43.46 5.43.60 | 5.5.11.10.6 5.62.0.9 5.6:4:3:0 | 58.0.00 58.0.00 |
| 7 9 9 40530 42460 44500 46300 48430 400560 50080 5200 53430 55000 57990 59990 50990 50000 57990 58990 50000 57990 58990 50000 57990 58990 50000 57990 58990 5 | 7. | | | 4.1.6.9.0 | 43.5.7.0 | 4.54.50 | | | | | 5.3.3.0.0 | | | 500 0.00 |
| 7.10.0 4016.0 4211.0 0 44.1060 46.1000 48.9.60 4109.00 50.8.60 52.800 54.7.60 56.7.00 58.6.69 5106.01 41.0.00 41.0.00 41.0.00 50.10.00 50.000 54.7.60 56.7.00 58.6.69 5106.01 41.0.00 5 | 7 | | | | | 4.61.30 | 47.8.9.9 4.7.10-7.6 4.8.0.5.3 | | | 5.1.8.00 | 53.5.09 53.7.16 53.9.23 | 55 6.3.0 | 573 40 | 3.9.6.9.0 |
| | 7: | 14 3 3 | 40.6.9.9 | | 44553 | | STATE OF THE PARTY | | | | Wall Park Inch | | | |
| 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | | 45.5 | 41.0.0.0 | 13.0.7.6 | | | 192113 | | \$0.10.53 \$1.0:4.6 \$1.2.3.9 | \$3.0.00 \$3.0.00 | 549 59 | | 20.10.10.0 | 221.0.0.0 |
| | 7 | 11. 04.5.4 | 41.5.00 41.7.3.9 41.8.106 44.10.5.3 | 43.5.6.0 | 45.6 113 45.8 7.6 45.10 3.0 | 7.80.0 | 9 6 6 9 | 411.4.6.0 | 51 4.3.0 | 53. 8.00 53. 8.00 53. 8.00 | 553.00 55.5.90 55.7.906 55.7.906 | 57.36.0 | 50.553 | 541 - 3 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 |

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A TABLE OF FEET AND INCHES

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|---|---|---|--|--|---------------------------------------|--------------|---|---|--------------------------------|--|---|-------------|
| ELParis | FI.Parts | FIParts | F.I.Parts | F.I.Parts | F.I.Parts | F.I.Parts | F.I.Parts | FLParts | FLParts | F.L.Parts | FLParts | EL Parts |
| | 0.6.4 | 0.6.4 | 0.6.34 | 0.7.0 | 0.7.4 | 0-7-4 | 0.7.3 | 0.8.0 | 0.8.4 | 0.8.5 | 0.8.3 | 0.0.0 |
| 8.0.9 | 4.2.0.0.0 | 440.0.0 | 46.0.0.0 | 4.8.0.0.0 | 4.10.0.0.0 | 5.0.0.0.0 | 5.2.0.00 | 5.4.0.0.0 | 5.6.0.0.0 | 58.0.0.0 | 5.10.0.0.0 | 6.0.0.0.0 |
| 1 | 42.483 | 4433.0 | 46.3.4.6 | 48.3.6.0 | 410.37.6 | 50.39.0 | 52.3.100 | 54400 | 5.6.4.1.6 | 58.0.0.0 58.2.1.6 58.4.3.0 58.6.4.6 | 5.10.4.4.6 | 6.0.4.6.0 |
| 8.1.8 | 42.6.30 | 4.4.6.6.0 | 46.6.0.0 | 48700 | 4.10.7.3.0 | 5.0.7.6.0 | 52.7.9.0 | 5.4.8.0.0 | 5.6.8.3.0 | 58.8.6.0 | 5.10.8.0.0 | 6.0.0.0.0 |
| 3,3 | | 449996 | 46.8.5.3 46.10.1.6 46.11.9.9 | 4.8.18.6.0 | 4.10.10.10.6 | 50.11.3.0 | 53.1.6.0 | 5.3.0.0.0 | 570.46 | 58.8.6.0 5.810.7.6 59.0.9.0 59.2.106 | 3.11.1.1.0 | 6.1.3.0.0 |
| 8.2.9 | 43.0.60 | 4.5.1.0.0 | 47.3.2.3 | 4.0.2.0.0 | 411.43.0 | 5.1.3.0.0 | 58.3.6.0 | 5.5.4.0.0 | 57.4.60 | 59500 59716 59930 591146 | 5.11.5.6.0 | 6.1.6.0.0 |
| 1 | 433723 | 455.10.6 | 47.6.60 | 4.9.5.00 | 411.6.1.6 | 51.6.9.0 | 537 46 | 55.8.0.0 | 5.7.8.7.6 | 59930 | 5-11-9-10.6 | 6-1-10-6-0 |
| 8.3.0 | 4.3.8.3.9 | 457.00 | 478.3.0 | 4.0.0.0.0 | 441.0.0.0 | 5.1.10.6.0 | 53.11.3.0 | 5.6.0.00 | 58.0.9.0 | 510.1.6.0 | 6.0 2.3.0 | 6.2.3.0.0 |
| 3,1 | 43.11.53 | 46046 | 18139 | 410.2.3.0 | 3.0.3.2.9 | 5223.0 | 5431.6 | 56.6.0.0 | 58.4.10.6 | 5105.00 | 6.0.6.7.6 | |
| 8.4.9 | 4.42.69 | 462.00 | 483.0.0 | 4.10.5.9.0 | 5.0.5.0.0 | 5.2.6.0.0 | 5.4.7.0.0 | 5.6.8.0.0 5.6.10.0.0 5.7.0.0.0 5.7.2.0.0 | 58.9.0.0 | 5-10-10-0.0 5-11-0-1-6 5-11-2-3-0 | 6.0.11.0.0 | 6.3.0.0.0 |
| 34 | 4.4.5.83 | 46.6706 | 4.8.8.0.9 | 410.93.0 | 5.0.10:5.3 | 32.117.6 | 5.5.0.g.g | 57.2.0.0 | 5.93.23 | 511. 4.4.6 | 6.1.3.4.0 | 6.3.6.9.0 |
| 8.5.0 | 4.47.3.0 | 4.6.8.6.0 | 48.9.9.0 48.11.5.3 49.1.1.6 4.9.2.0.9 | 411.0.0.0 | 51.0.3.0 | 53.1.6.0 | 55.2.9.0 | 57600 | 59.5.3.0 59.73.9 | 511 6 6 0 511 8 7 6 511 10 9 0 6 0 0 10 6 | 6.1.9.113 | 63.900 |
| 32 | 4.411.113 | 47.1.46 | 4.9.2.0.9 | 411.430 | 51.583 | 33.31.6 | 33.8769 | 5.7.10.0.0 | 59.11.5.3 | 6 0 0 10.6 | 6.2.2.3.9 | 64390 |
| 8.0.0 | 453.00 | 47.3.00 | 49.6.23 | 4.11.0.0.0 | 5.1.9.3.9 | 53.00.0 | 5.5.10.6.0 | 5.8.0.0.0 | 5.10.1.6.0 | 6.0.3.0.0 6.0.5.1.6 6.0.7.3.0 6.0.0.4.6 | 6.2.6.8.3 | 648.3.0 |
| 8 7 0 | 4.5.6.23 | 47.0.30 | 499.6.0 | 411.11.3.0 | 52.0.113 | 34.27.6 | 5.6.439 | 5.8.6.0.0 | 510783 | 6.0.0.4.6 | | |
| 是 | 45.9.3.9 | 4.7.11.1.6 | 410.0.11.3 | 5.0.2.9.0 | 5.2.6.9 | 54.6.4.6 | 5.6.8.2.3 | 50.000 | 5.10.9.9.0 | 6.0.11.6.0 | 6.3.1.3.0 | 6.5.3.0.0 |
| 8.8.0 | 4.6.2.00 | 1.8.4.0.0 | 4106.00 | 5.0.8.0.0 | 5.2.8.2.3 | 54.101.6 | 5.7.0.09 | 59.2.0.0 | | | 63.79.9 | 6.59.9.0 |
| 143 | 4.6.3.69 | 4.8.5.7.6 | 4106.0.0 410.78.3 410.9.46 410.11.0.9 | 5.0.9.0.0 | 5311.99 | 5.5.1.10.6 | 57.3.11.3 | 39.0000 | 5.11.8.0.0 | 6:1.8.0.0 6:1.10.1.6 6:2.0.3.0 6:2.2.4.6 | 6.4.0.2.2 | 0.0.0.0.0 |
| 8.9.6 | 4:68.30 | 4.8.10.6.0 | 4.11.0.0.0 | 5.1.3.0.0 | 53.53.0 | 5:5.7.6.0 | 5.7.9.9 | \$10.0.0.0 | 6.0.2.3.0 | | 6.4.6.0.0 | 0.0.0.0.0 |
| 14.5 | 40.0.00 | 4.9.0.1.6 | 4.11.0.0.0 411.2.5.3 4.11.4.1.6 4.11.5.0.0 | 5.1.4.9.0 | 5.3.7.0.0 | 559.46 | 5.7.11.8.3 | 510.2.0.0 | 6.0.43.0 | 6.2.8.0.0 | 6.4.8.11.3 | 6.0.11.3.0 |
| 8.10.6 | | | 4.11.7.6.0 | | | 5-6-7.0.0 | 58.5.6.0 | 5.10.8.0.0 | 6.040.6.0 | 6.3.1.0.0 | 6:5:3.6.0 | |
| 37 | 47.40.0 | 4.9.8.3.0 | 4.11.9.2.3 4.11.10.100 5.0.0.6.9 | 5.1.11.9.0 | 54.2.3.9 | P.h. A.In. h | 5.8.7.5.3 | 2.10.10.0.0 | 6.1.2.7.6 | 63.5.3.0 | 655.7.106 | 6.7.8.3.0 |
| 8.11.0 | | | | | | | 5.9.1.3.0 | 5-11-4-0-0 | 6.1.6.9.0 | | 6.6.0.3.0 | 6.8.3.0.0 |
| 五 | 47.11.100 | 4.10-2.00 | 5057.6 | 5.2.8.0.0 | 54.00.00 | 57040 | 5.05.1.6 | 511.8.0.0 | 6.1.8.99 | 63.9-6.0 6347-6 644.9-0 643.10-6 | 6.6.2.5.3 | 6.8.7.6.0 |
| 9.0.9 | 4.8.3.00 | 4.10.6.0.0 | 5.0.9.0.0 | 5.3.0.0.0 | 5:5:3:0.0 | 5.7.6.0.0 | 5:0.0.0.0 | 6.0.0.0.0 | 6,2.3.0.0 | 6.4.6.0.0 | 6.6.9.0.0 | 6:0.0.0.0 |
| 34 | 48.5.1.6 | 4.10.9.3.0 | 5.1.0.4.6 | 53360 | 35 6 7 6 55 8 53 | 5.79.90 | 5.10.0.10.6 | 6.0.6.0.0 | 6.2.7.1.6 | 6.4.6.0.0 6.4.8.1.6 6.4.103.0 6.5.0.46 | 67.1.4.6 | 6.9.4.6.0 |
| 9.2.2 | 48.9.30 | 4.11.0.6.0 | 51.3.0.0 | 5.37.0.0 | 5.5.10.3.0 | 5.8.1.6.0 | 510.4:00 | 6.0.8.0.0 | 6.2.11.3.0 | 6.5.2.6.0 | 5.7.5.9.0 | 6.9.9.0.0 |
| 4 | 49.0.46 | 4.11.3.9.0 | 518.99 | 5.310.6.0 | 5.6.3.8.3 | 5.8.5.3.0 | 5.10.8.7.6 | 6.1.0.0.0 | 6.3.3.4.6 | 6.5.2.6.0 6.5.47.6 6.5.6.9.0 6.5.810.6 | 5.7.10.1.6 | 0.001.00 |
| 9.2.0 | 4.9.3.6.0 | 411.7.00 | 5-1-10-6-0 | 54.2.0.0 | 5.6.5.6.0 | 58.0.0.0 | 5.11.0.6.0 | 6.1.4.0.0 | 6.3.7.6.0 | 6.5:11.0.0 | 5.8.2.6.0 | 6.10.6.0.0 |
| 3, | 40876 | 4-11-10 30 | 52.3.6.9 | 54560 | 5.6.9.1.6 | 5.9.2.7.6 | 511.6.3.0 | 6.1.10.0.0 | 6.41.83 | 6.5:11.0.0 6.6.1.1.6 6.63.3.0 6.65.4.6 | 8.0.00 | 5.10-10.6.0 |
| 9.3.2 | 49.9.9.0 | 5.0.3.1.6 | 52.5.3.0 | 549.0.0 | 57.0.0.0 | 5.9.46.0 | 5.11.8 3.0 | 6.2.0.0.0 | 6.43.9.0 | 6.6.7.6.0 | 5.8.11.3.0 | 5.11.3.0.0 |
| | 7.0.20 | , , , | 124000 | 00 | 2/0-0 | 03,000 | 0.0.2 03 | 0.2.0.0.0 | 49.113 | 7.7.10.0 | .9 3.99 | 11990 |
| 9.4.0 | 410.40.0 | 5.0.9.7.6 | 3.1.8.3 | 55.4.0.0 | 57.8.0.0 | 5.10.0.0.0 | 6.0.4.0.0 | 6.2.10.0.0 | 6.5.0.0.0 | 6.7.4.0.0 6.7.6.1.6 6.7.8.3.0 6.7.10.4.6 | 9.8.0.0 | 7.0.0.0.0 |
| 34 | 410883 | 3.1.0.10.0 | 3.5.0.9 | 59.3.0 | 8.1.53 | 5.105.7.6 | 6.0.999 | 6.3.2.0.0 | 6.5.6.2.3 | 5.7.10.4.6 | 10.0.4.0 | 0.6.9.0 |
| 9.5.6 | 4.10.109.0 | 5.1.4.1.6 | 3.8.5.3 | 5.6.0.0.0 | 58.3.3.0 | 5.10.7.6.0 | 6.0.11.9.0 | 63.0.0.0 | 5.5.8.3.0 | 68.0.6.0 68.2.7.6 68.4.9.0 68.6.10.6 | 10.8:11.3 | 0.9.0.0 |
| | | | | | | | | | | | | |
| 9.0.0 | 4.11.6.0.9 | 5.1.10.7.6 | 4.3.2.3 | 6.7.9.0 | 9.0.3.9 | 5.11.4.10.6 | 6.1.9.53 | 6.4.2.0.0 | 0.0.4.0.0 | 5.8.9.0.0 | 11.3.8.3 | 1.8.3.0 |
| | 4.11.9.23 | 5.2.1.10.0 | 40.00 | 0.11.3.0 | 9.3 7.3 | 2.11.0.1.0 | 0.7.1.39 | 0.4.0.0.0 | 1.0.100.3 | :03.4.0 | 11.0.0.0 | . 2.0.9.0 |
| 李 | 5.0.0.39 | 52.5.1.6 | 49:113 | 7.2.0.0 | 9.7.6.9 | 6.0.2.3.0 | 6.25.23 | 6.4.10.0.0 | 72.99 | 97.7.6 7 | 0.0.53 | 253.0 |
| 9.8.0 | 5.0.5.0.0 | 52.100.0 | 53.0.0 | 7.8.0.0 | 10.1.0.0 | 6.0.6.0.0 | 6-2-11-0-0 | 6-5-4-0-0 | 6.7.0.0.0 | 10.2.0.0 | 0.4.9.9 7 | 3.0.00 |
| 是五 | 5.0.6.6.9 | 52.11.7.6 3 | 54835 | 7.99.0 3 | 102.9.9 | 6.00.00 | 6.3.0.113 | 6.5.6.0.0 | 58 4.0.0 | 10.2.0.0 7 | 0.9.23 | 3.4.0.0 |
| 9.9.8 | 5.0.11.30 | 3.4.6.0 3 | 50.0.0 | 83.0.0 | -10.6-3.0 | 6-1-1-6-0 | 6.3.6.0.0 | 6.6.0.0.0 | 8.53.0 0 | 10.10.6.0 7 | 1.3.9.0 7 | 3.0.0.0 |
| 45 | 5.1.2.46 | 37.9.0 3 | 511.5.3 3 | 8.6.6.0 3 | 10-10-0-9 | 51530 | 3.10.7.6 | 6.6.6.0.0 6.6.6.0.0 | 8046 6 | 10.106.0 7 | 1.8 1.0 2 | 3.11.3.0 |
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| 9.11.9 | 5.1.11.9.0 3 | 45.6.0 5 | 6.11 - 3.0 5 | 950.0 5 | 0.0.0.0 | 5.2460 | 6:4.103.0 | 5.7:400 6 | 9.9.9.0 7 | 03.6.0 7 | 2.9.3.0 7 | 5.3.0.0 |
| 弘 | 5.2.2.106 3 5.2.4.53 | 4840 5 | 7.2.7.6 3 | 08.6.0 6 | 0.2.4.6 | 28.3.0 | 5. 4.0.9 0 | 7.8.0.0 | 103.123 | 03.6.0 7 05.7.6 7 86.900 7 | 3.3.6.9 7 | 570.0 |
| | | 50.00 5 | 7.6.0.0 5 | 10.0.0.0 6 | 0.60.0 6 | 3000 | 5.5.6.00 6 | 8.0.0.0 6 | 10.60.0 7 | 1.0.0.0 7 | 3.6.0.0 7. 3.8.2.3 7. 3.0.4.0 7. 40.0.9 7. | 6.0.0.0 |
| | 5.2.7.6.9 5.2.7.6.9 5.2.9.1.6 5.2.10.8.3 | | 7.6.00 5 | The second secon | 0.9.7.3 | 3396 | 55711.3 | 8 8000 | 10.10.1:0 7 | 1.4.3.0 7 | | |
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| 34 3 | 3 4113 5 | 5.9.9.0 5 | 8.5:0:0 5 | 11.0.3.0 0 | 1.6.8.3 6 | 41.1.6 | 67.60 6 | 9.2.00 6 | | 1107.6 7. | 4939 7 | 73.9.0 |
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| 20.5. 2 5 | 54.30 6 | 7.8.6.0 | 03.00 6 | 041.0.0 | 3.6.3.0 6 | 6:46.0 6 | 8.8:00 | 11.4:00 7 | | | | |
| 10.5. St. 2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2 | 54.46 | 7.8.6.0 St. 6 St. | 2536 | 0.11.0 0 6: 0.9.0 6: -2.0.0 6: -4.3.0 6: | 9.400 | 0340 0 | 8.8.9.0 6. 8.1883 6. 9.0.7.6 6. 9.2.6.9 6. | 11.0.0.0 7 | 1.110.0 7 2.12.0 7 2.553 | 48 26 7 | 7:1:9:0 7 | 01.30 |
| 10. | 3 511-3 50 | 14:0 34 | 9.9 01 | 43.0 03 | 11.0.3 | 0.77.0 | 9.209 0 | 7. | 2003 7 | 5.0.10.6 7. | 1.03.9 | 03.9.0 |

A TABLE OF FEET AND INCHES. from so foot 6 unches by 6 unches and 1 quarter to 12 foot 5 inches and 3 quarters by 9 inches

| | | | | | | | rts inches | | | | | TIT D |
|---------------|--|---|--|---|--|--|---|--|--|--|--|---|
| F.I.Barts | THE RESERVE OF THE PERSON NAMED IN | F.I.Parts | | | | COMPANY OF STREET | | THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER. | | F.I.Farts | DESCRIPTION OF THE PARTY OF THE | |
| 10.6.0 | | 0.6.5 | | | | A STATE OF THE PARTY OF THE PAR | 0.7.3 | CONTRACTOR CONTRACTOR SERVICES | THE RESIDENCE OF THE PARTY OF T | | Control of the Contro | 7.10.60.0 |
| 3, | 554076 | 58.3.0.0 58.47.0 58.6.3.0 58.7.10.6 | 541.0.2.3 | 6.1.7.9.0 | 6 433.9 | 6.7.0.0.0 | 6.0.8.46 | 7.0.0.0.0 | 7.2.0.6.0 | 7.5.5.1.0 | 78 2 10 6 | 7-10.83.0 |
| 10.7.0 | 5.6.3.3.9 5.6.3.3.9 56.4.0.6 | 580.00 | 511 530 | 6.2.1.0.0 6.2.2.0.0 6.2.4.0.0 6.2.6.2.0 | 6 4 8 9 0 6 4 10 6 9 6 5 0 4 6 6 5 2 2 3 | 67.6.46 | 6.10.0 3.0 | 7.0.8.0.0 | 23390 | 7.5.11.6.0 | 78730 | 711300 |
| 10.8.0 | 5.68 0.0 5.6 9.6 9 5.6 11 1.6 | 59.40.0 | 60.0.0.0.0 | 6.2.8.0.0 | 6.5.4.0.0 | 6.8.0.0.0 6.8.1.10.6 6.8.3.9.0 68:57.6 | 6.10.8.0.0 | 7.1.80.0 | 7.4200 | 7.6.8.0.0 | 7.0 4 0.0 | 80000 |
| 10:0.0 | 57230 57399 57346 | 50.10.6.0 510.0.1.6 510.1.9.0 510.3.4.6 | 6.06.9.0 | 63300 | 6.5.11.3.0 | 68760 | 6.11.58.3 | 7.2.2.0.0 | 24830 24039 5046 23253 | 77.460 | 710.0.0.0 | 8:0:900 8:0:1:3:0 8:1:3:0:0 |
| 10.10.0 | 578.6.0 57.10.0.0 57.11.7.6 | 510.5.0.0 510.6.7.6 5108.3.0 510.0.10.6 | 6.1.1.6.0 | 63.10.0.0 | 66666 | 693.0.0 | 0.11.00 | 7.28.00 | 7.5 4.6.0 7.5 60.0 7.58 7.6 | 78.1.0.0 78.3.1.0 78.53.0 78.53.0 | 7.100.6.0 | 8 · · · · · · · · · · · · · · · · · · · |
| 10.11 . 0 | 58290 58439 585100 | \$10.11.0.0 \$11.1.1.6 \$11.2.0.0 \$11.44.6 | 6.1.8.3.0 | 64500 | 67360 | 6:0:10.6:0 6:10.0:4.6 6:10 2:3.0 6:10:4:1.6 | 7.07.3.0 | 23.40.0 23.60.0 23.80.0 23.100.0 | 7.6.0.0.0 7.6.29.0 7.6.410.0 7.6.511.3 | 18 9 6 6 29 19 0 29 3 100 | 7.11.6.3.0 | 823.00 8253.0 827.60 8.27.60 |
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| 11.1.035 | 50330 50490 50646 50743 | 00000 00210 003.90 00546 | 62990 | 65700 | 68.4.3.0 68.6.0.9 68.7.106 68.9.8.3 | 611346 | 711000 | 748000 | 77,530 | 7.10.2.6.6 7.10.47.6 7.10.69.0 7.10.810.6 | 0.1.0.3.9 | 0.43.9.0 |
| 11.0. D | 5.0.0.0 0 5.0 11.0.0 510.0.7.6 510.22.3 | 60700 | 63.46.0 | 6.6.3.6.0 6.6.5.6.0 6.6.7.3.0 | 69.1.6.0 69.1.3.9 69.3.1.6 69.4.11.3 | 6.11.0.000 | 72.66.6.0 | 7.5.00.0 | 78360 | 7.10.11.00 | 8.23.09 | 8.4.6.0.0 8.4.8.3.0 8.4.10.6.0 8.5.0.0.0 |
| 11.3.01419.14 | 5.103:0.0 5.10:53:0 5.10:6:10:6 5.10:8:5:3 | 6.1.3.1.6 | 631130 | 0.6 9.0 0 0.6 10.9 0 6 7 0.6 0 6 7 2 3 0 | 6.9.6.9.0 6.9.8.6.9 6.9.0.46 6.00.2.3 | 7.0.4.6.0 | 73 23 0 | 76000 | 78 119 0 78 119 0 79 1 10 0 79 3 11 3 | 711976 | 82530 82753 82976 821199 | \$ 53.0.0 \$ 553.0 \$ 57.60 \$ 6.9.90 |
| 11. 4.04.5 | 5.10.10.0.0 5.10.11.6.9 5.11.1.1.6 5.11.2.8.3 | 6.1.8.0.0 6.1.9.7 6 6.1.11.3.0 6.2.010.6 | 646.00 | 67400 | 6.10.2.0.0 6.10.3.9.9 6.10.5.7.6 6.10.7.5.3 | 71.000 | 73.10.00 73.11.113 741.106 743.99 | 7.6.8.0.0 | 7.08.00 | 8.0.4.0.0 8.0.6.1.6 8.0.8.3.0 8.0.10.46 | 3 6 36 | 8.6.2.3.0 8.6.4.6.0 8.6.6.9.0 |
| 11.5.0 | 5-11-4:3-0 5-11-5-9-9 5-11-7-4-6 5-11-8-11-3 | 62260 62416 62590 62596 | 65.2.3.3 | 6.7.11.0.0 6.8.0.9.0 6.8.2.6.0 6.8.4.3.0 | 6.10.9.3.0 6.11.0.9 6.11.0.10.6 6.11.2.8.3 | 71.76.0 | 4583 | 77.6.0.0 | 7.10.4.3.0 7.10.4.3.0 7.10.6.4.6 7.10.8.5.3 | 8.1.2.7.6 8.1.4.90 8.1.610.6 | 3.1000 | 8 6.113.0 8 7.1.6.0 8 7.3.90 |
| 34 | 6.0.1.7.6 | 0.0.03.0 | 6.5.9.2.3 | 6.89.60 | 6.114.6.0 6.11.6.3.9 6.11.8.1.6 6.11.9.11.3 | 7.2.0.9.0 | 75750 | 7.8.4.0.0 | 7.11.4.8.3 | 8.21.3.0 | 4 9 8 3 8 4 11 10 0 8 5 2 0 9 | 8 28 30 8 7 10 6 0 8 8 0 9 0 |
| 7 11/ | 6.0.4.0.0 6.0.63.9 6.0.7.10.6 6.0.9.5.3 | 6:3:3:6:0 6:3:5:1:6 6:3:5:1:6 6:3:8:4:6 | 6.63.7.6 6.67.3.9 | 69.400 | 7.0.1.6.0 | 7.3.2.3.0 | 7.6.3.0.9 | 7.8.10.0.0 | 7.118.9.9 | 8 2 7 7 . 0 8 2 9 9 0 8 2 11 10 6 | 8 5 6 5 3 8 5 8 7 6 8 5 10 0 0 | 8 8 5 3 0 8 8 7 6 0 8 8 9 0 0 |
| | 6.1.0.6.9 | 631176 | 6.7.0.4.6 | 9.0000 | 1.08.0.0 | 73.7 10.6 | 6 8 10.6 | 7.0.0.0.0 | 0.5.0.9 3.0.7 1.6 8.0.9.2 8 | 3.38.46 | 65.4.6 | 8.0.2.3.0 8.0.4.6.0 8.0.69.0 |
| 34 | 6.1.9.11.3 | 6.4.7.9.0 6.4.7.9.0 6.49.46 | 67399 | 104.90 | 1. 1. 0. 9 | 7.43.46 | 7.283 | 7.10.2.0.0 | 13.40 | 429.0 | 7.43.9 | 3.10.1.60 3.10.3.9.0 3.10.6.0.0 |
| | . a. E a a | 6.411.0.0 6.5.07.6 6.5.2.3.0 6.5.3.10.6 | 58.5.0.0 / | | 2.4.0.0 | 7 5. 1.6.0 | 7.8.4.2.0 | 7.11.0.0.0 | 2.1.8.3 | 49130 | 8.3.3.0 | 11.0.9.0 |
| 34 6 | 5-2-1053 | 6.5.5.6.0 6.5.7.1.6 6.5.8.0.0 6.5.10.4.6 | 68 103.9 | 6.11. 6.0.0 7 6.11. 8.6.0 7 6.11. 10.3.0 7 | 2.0.20 | 7.5.6.4.6 | 8.0.0.0 | 7.11.6.0.0 7.11.8.0.0 7.11.10.0.0 | 2599 | 57906 | 8776 | .11.53.0 3.11.7.6.0 3.11.0.0.0 |
| 34 0 | 53.1.6.9 | 66.33.0 | 93.467 | 03.6.07 | 3.3.7.6 | | 0.7.9.0 | 0.20.0 | 3 4 1 0 8 | 6.8.6.0 8 | .9.8.0.0 | 7.0.2.3.0 7.0.4.60 7.0.6.90 |
| 34 6 | 37.09 | 66.6.6.0 | 9.10.1.6 9.10.1.6 9.11.0.0 7 | ·0.8.9.0 7 ·0.00.0 7 ·1.0.3.0 7 | 3.10.100 | 73.00 | 101.60 | 0.10.0.0 1.0.0.0 1.2.0.0 | 31039 | 7.5.0.0 | 10.1.1.6 10.33.0 | 2.1.3.00 |
| | 4.6.0.0 | 67.7.0.0 | 10.8.3.0 7 | 1.3.6.0 7 | 4 6 9 9 0 7 | 7.6 9.0 7 | | 1.8.00 | | | 11.2.3.0 | 2.3.00 |
| 9.1.00 | 41153 | 5.7.10.00 6.8.0.4.6 6.8.2.00 | 11.3.0.0 7 | 2.4.0.0 7 | 53237 | 8.6.0.0 | 1.10.11.6.0 8 1.11.3.1.6 1.11.3.0.0 8 1.11.7.0.0 8 | | 5.4:100 5.6:113 5.9.0.0 | 8.10.0.0 | 11.899 | 27.6.9 |
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| F.I.Parts | F.I.Parts | F.I. Parts | F.I. Parts | F.I.Parts | F.I. Parts | EI.Parts | F.I. Parts | F.I.Parts | EI.Parts | ELParts | F.I.Parts | EI.Parts |
|-----------|--|------------|------------|-----------|------------|-----------|------------|-----------|----------|---------|-----------|----------|
| | 0.9.4 | 0.9.4 | 0.9.3 | 0.10.0 | 0.10.4 | 0.10. 2 | 0.10.3 | 0.11.0 | 0.11.4 | 0.11.5 | 0.11.3 | 1.0.0 |
| 0.9.0 | 0.6.11.3.0 | 0.7.8.3.0 | 0.7.11.0.9 | | | | | | | | | |
| 0.10.0 | 0.7.8.6.0 0.7.10.9.9 0.8.1.1.6 0.8.3.5.3 | 0.7.11.0.0 | 0.8.1.6.0 | 08.4.0.0 | 0.8:0.0:9 | 0.9.2.3.0 | 0.9.7.6.9 | | | | | |

A TABLE OF FEET AND INCHES.

AZTABLE OF FEET AND INCHES

| from 3 foot's inches by | o inches and one quarter to. | 5 foot winches and 3 quarte | en by i foot |
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| F. B. FIRM F. Parts N. Parts | El Parts El Parts El Parts | El Parts El Parts El Parts | F.L. Harts F.L. Rarts |
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A TABLE OF FEET AND INCHES.

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| | 000 | 67010 | 69496 | 611346 | 1,300 | 73676 | 7.5.83.0 | 78.930 | 7 105 0.0 8 | 0313 | 28008 | 17398 | 7.000 |
| | 8.7.0 | 67700 | 698106 | 611.108 3 | 2300 | 7 423 0 | 76690 | 78 37 30 | 1010 0 0 | 1046 | 3 3 3 6 8 | 5700 | 7 600 |
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| | 34 | 6.11.083 | 7137.6 | 7.3.0.00 | 7.6.0.0.0 | 7.8 9.00 | 7100000 | 8.0.9.0.0 8.0.11.8.3 8.1.2.4.6 | 83000 | 5300 | 878.00 | 9.11.11.3 | 90000 |
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| | 9.0.0 | 23.06.0 | 7.63.0.0 | 287.6.0 70.04.6 | 7.11.0 0.0 | 8.1.400 | 8.3.9.0.0 8.3.117.6 8.4.23.0 8.4.410.0 | 8.6.4.2.3 86.6.10.6 86.6.10.6 | 8 8 8 9 0 8 8 11 6 0 8 9 2 3 0 | 8 11 1 3 9 8 11 4 1 5 8 11 6 11 3 | 9 1 3 9 0 6 | 931053 | 9 6 3 00 |
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A TABLE OF FEET AND INCHES from 10 foot 11 inches by 9 inches and 1 quarter to 12 foot 5 inches and 3 quarters by 1 foot

| A CHIEF WATER | | e to just th | inches vy | guuna | and I que | arter to | 2 foot 5 t | nches and | ts quart | ers by 1 | oot . | et describe intellement in section |
|--|---|--|--|---|---|--|---|---|--|--|---|--|
| F.I.Part | s FI Part | s F.I.Parts | F.I.Parts | F.I.Parts | F. I. Parts | F.I.Parts | F.I.Parts | F.I.Parts | F.I.Parts | F.I.Parts | F.I.Parts | F.I.Parts |
| A TENNESSEE | 0.94 | 092 | 0.93 | 0.10.0 | 0.104 | 0.10% | 0.10 3 | THE REPORT OF THE PROPERTY OF | 0.114 | 0.11 5 | 0.113 | 100 |
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| 11.0.0 | | 0 88.6.0.9 | 811.3.0.0 | 9.2.0.0.0 | 9.4.9.0.0 | 0.7.6.0.0 | 9.10.3.0.0 | 0.1.0.0.0 | 10.3.0.2.3 | 0.0.3.1.0 | 0.0.3.0.0 | 11.0.0.0.0 |
| 2000 | 35,9.0 | 6 8.8.0.0.0.0 | 811.7.10.6 | 9.2.5.0.0 | 0.3.2.1.6 | 9.7.11.3.0 | 9.10.3.8.4.0 | 10.1.5.0.0 | 0.3.11.0.0 10.4.2.7.6 10.4.5.5.3 | 0.0.8.0.0 0.6.4.9.0 0.7.2.7.6 | 0.0.3.0.0 | W.O. 3.O. 0 W.O. 0.O. 0 |
| 11.1.0 | 100.0.0. | 0 8.0.3.6.0 | 9.0.0.9.0 | 0.2.10.0.0 | 9.5.7.3.0 | 9.8.4.6.0 | 0.11.1.0.0 | 10.1.11.0.0 | 0.4.8.3.0 0.4.11.0.0 | 0.7.5.6.0 | 10.10.2.0.0 10.10.5.8.3 10.10.6.7.6 10.10.11.6.9 | 11.1.0.0.0 |
| 2 | 80.00. | 3 8.9.26.7.6 | 9.0.8.0.0 | 9.3.3.0.0 | 9.0.2.11.3 | 9.9.0.4.6 | 211.0.0.0 | 0.2.7.3.0 | 0.5.1.10.0 | 0.7.11.3.0 | 0.0.8.7.0 | 11.1.0.0.0 |
| 11. 2.0 | 8.7.3.0.0 8.7.5.9.5 8.7.5.9.5 | 0 8.0.3.4.6 | 0.1.0.11.3 | 9.3.10.6.0 | 9.6.0.7.6 | 0.0.5.7.6 | 0.0.3.2.3 | 10.3.0.0.0 | 0.5.0.3.0 | 0.8.7.10.6 | 0.11.2.6.0 0.11.5.5.3 0.11.8.4.8 0.11.11.3.9 | 11.2.0.0.0 11.2.3.0.0 11.2.0.0.0 |
| 11.3.0 | 0.8.0.9.0 | 81.0.10.6.0 | 9.1.8.3.0 0.1.6.A.3 | 9.4.6.0.0 | 9.7.3.0.0 | 9.0.1.6.0 | 0.0.11.3.0 | 10.3.9.0.0 | 0.0.3.11.3 | 0.9.4.6.0 | 11.0.2.3.0 | 11.2.0.0.0 11.3.0.0.0 11.3.3.0.0 |
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| 11.5.0 | 8.9.7.3.0 | 9.0.3.1.0 | 9.3.1.3.9 | 9.5.11.0.0 | 9.9.0.3.0 | 9.11.7.10.0 | 10.2.6.0.9 | 10.5.4.3.0 | 10.B.2.5.3 10.B.5.3.0 | 10.11.0.7.0 | 11.1.10.0.0 | 11.4.9.0.0 |
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| 11.6.0 | 80.6.9.9 | 9.1.3.0.0 9.1.3.4.6 9.1.7.9.0 9.1.0.1.6 | 0.4.1.6.0 | 9.7.0.0.0 | 9.9.10.6.0 | 10.0.0.0.0 | 10.3.7.6.0 | 0.0.0.0.0 | 0.9.4.6.0 | 11.0.3.0.0 | 11.3.1.6.0 11.3.4.5.3 11.3.7.4.6 11.3.0.3.9 | 11.6.0.0.0 |
| 11.7.0 | 8.14.1.0.0 | 0.2.0.6.0 | 9.4.8.9.9 | 9.7.7.6.0 | 0.10.8.2.3 | 10.1.4.10.6 | 0.4.3.6.0 | 10.7.2.3.0 | 0.10.0.11.3 | 11.0.11.7.6 | 11.3.0.3.9 | 11.6.9.0.0 |
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| 11.8.0 | 811.11.0.0 | 9.2.10.0.0 | 9.5.0.0.0 | 9.8.8.0.0 | 9.11.7.0.0 | 10.2.6.0.0 | 0.5.5.0.0 | 0.8.4.0.0 | 0.11.3.0.0 | 11.2.2.0.0 | 11.5.1.0.0 | 11.8.0.0.0 |
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| 11.9.0 | 0.0.8.3.0 0.0.0.6.0 0.1.0.10.6 0.1.3.2.3 | 9.3.7.0.0 | 9.6.6.9.0 9.6.9.2.3 9.6.11.7.6 9.7.2.0.9 | 9.9.0.0.0 9.9.8.6.0 9.9.11.0,0 | 10.0.7.9.9 | 10.3.4.0.0 10.3.7.1.6 10.3.9.9.0 | 10.0.3.9.0 10.0.6.5.3 10.0.0.1.0 | 10.9.3.0.0 10.9.3.0.0 10.9.8.6.0 | 11.0.2.3.0 11.0.5.0.9 11.0.7.10.6 | 11.3.1.0.0 11.3.4.4.6 11.3.7.3.0 | 11.6.0.0.0.0 11.6.3.8.3 11.6.6.7.6 11.6.9.6.0 | 11.9.3.0.0 |
| 11.10:0 | 9.1.5.6.0 | 0.4.5.0.0 | 9.7.4.6.0 | 9.10.4.0.0 | 0.1.3.6.0 | 10.4.3.0.0 | 10.7.2.6.0 | 10.10.2.0.0 | 11.0.10.8.3 | 11.4.1.0.0 | 11.7.0.6.0 | 11.9.9.0.0 |
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| 12.1.0 | 9.3.9.3.0 | THE RESERVE AND ADDRESS OF THE PARTY. | | 0.0.10.0.0 | 0.3.0.3.0 | 0.6.10.6.0 | 10.0.10.0.0 | 11.0.11.0.0 | 11.3.11.3.0 | 11.6.11.6.0 | 11.9.11.9.0 | 12.1.0.0.0 |
| 4 | 0.4.1.10.6 0.4.4.2.3 | 9.7.2.3.0 | 7 4 | 0.1.3.0.0 | 0.4.0.9.9 | 0.7.3.0.0 | 10.10.1.5.3 | 11.1.4.6.0 | 11.4.4.10.0 | 11.7.5.3.0 | 11.10.5.7.6 | 12.1.6.0.0 |
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| - Strange | 0.58.4.0 | 0.8.40.0 0.8.6.0.6 0.8.0.3.0 0.8.1.7.6 | 0.11.7.8.3 | 0.2.6.0.0 0.2.8.6.0 0.2.11.0.0 0.3.1.6.0 | 0.5.11.10.6 | 0.0.0.0.0 | 10.11.10.11.3 | 11.3.2.6.0 | 11.5.0.0.0 11.6.0.6.0 11.6.3.4.6 11.6.5.2.3 | 11.9.4.3.0 | 12.0.5.1.0 | 2.3.3.0.0 2.3.0.0.0 2.3.0.0.0 |
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| 12.5.0 | 0.6.10.3.0 | 001160 | 10.0.0.0.0 | 0.3.11.6.0 | 0.7.0.8.3 | 0.10.1.10.6 | 11.1.3.0.9 | 11.4.4.3.0 | 1.7.5.3.3 | 11.10.0.7.0 | 12.1.10.0.0 | 2.4.0.0.0 |
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| 1.0.0 | 1.0.3.0.0 | 1.02 | 1.0% | 1.0 | 4 | 2 | 1.1.2 | 7.2.0 | - 4 | . 2 | 1.24 | 1.3.0 |
| 1 | 1.0.2.3 | 1.1.0.3.0 | 1.1.6.6.0 | | | 9-1-1-1 | | | | | | S. C. C. C. C. |
| 1.1.04 | 1.1.3.3.0 | 1.1.6.6.0 | 1.1.0.0.0 1 | 2.1.0.0 | 2.7.6.0 | 2022 | | | | | | |
| 1.2.0 | 1.2.0.5.3 | - | | 2.4.3.0 1 | | 12000 | .3.9.0.9 | 1.4.4.0.0 | | | | |
| 女 | 2.3.6.0 2.0.0.0 2.0.7.0 | 1. 2.10.1.6 | 3.4.0.0 | 3.2.0.0 | 3.5.6.0 | 40.4.0 | 4.3.11.3 | 1.4.7.6.0 | .5.2.7.0 .5.2.7.0 | 5.6.3.0 | 1.6.1.6.9 | |
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| 1.5.0 | .5.1.2.3 | 1.58.601 | | | 6.9.3.0 | | | 1.7.0.0.0 | 8.2.3.0 | 8.0.6.0 | 1.8.10.0.0 | 1.0.3.0.0 |
| 3 | .0.1.5.3 | 1.6.2.0.0 | 6.3.11.3 1. | 6.5.0.0 6.8.3.0 6.11.6.0 7.2.9.0 | | | | 1.8.1.6.0 | 8.0.4.6 | 9.5.4.6 | | 0.6.2.0 |
| 1.6.04 | 6,7.0.0 | 1.7.0.1.0 | 7.1.0.0 1. | 7.0.3.0 | 3.100.0 1 8.1.9.9 1 8.5.1.6 | 8.3.0.0 | 1.8.7.6.0 | 0.00.0 | 9.40.0 | 9.9.0.0 0.0.7.6 | 1.10.1.6.0 | 10.6.0.0 |
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A TABLE OF FEET AND 'INCHES from I foot 7 inches by I foot and 3 quarters of an inch by I foot 3 inches

| Financial Financial States by | The state of the s | Charles Management Control of the Co | to 4 foot and 3 qui | arters of an inc | th by 1 foot 3 inches |
|---|--|--|--|--|---|
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A TABLE OF FEET AND INCHES

from 4 foot I Inch by I foot and I quarter of an Inch to 6 Foot 6 inch & 3 quarter by I foot 3 inches FI Parts FI Parts El Parts El Parts FI Parts FI Parts FI Parts FI Parts FI Parts 5.0.3.6.9 5.1.2.6.0 5.2.4.7.0

A TABLE OF FEET AND INCHES

| from 6 foot 7 inches | by I foot as | nd I quarter of an | inch to g foot and | quarters of an inc | h by I foot 3 inches. |
|--|--|---|--|--|---|
| FI Parts FI Parts FI Parts | FI Parts FI Parts | F.Parts F.Parts | FI Parts F.I Parts | F.I.Parts F.I.Parts | F.I.Parts F.I.Parts |
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| 6.10.0 611.8.6.0 7.1.5.0.0 | 7.3.7.0.0 7.4.0.0.0 | 7.0.00.0 78.30.0 | 7.0.11.0.0 7.11.8.0.0 | 81, 40 0 03 1,00 81, 80 0 83 47 0 81, 17 0 83 83 0 | 849.6.0 60.6.0.0 651.2.3 60.9.0 854.2.3 67.50 |
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| 8.4.0.7.0 8.6.7.3.0 8.4.0.7.0 8.6.7.3.0 8.4.0.8.3 8.6.0.4.0 8.3.0 8.5.0.9.0 8.7.1.0.0 8.5.3.9.9 8.7.4.7.0 | 8.8.11.0.0 810.11.9.0 | 0.0.5.0.0 0.2.04.0 0.0.0.1.0 0.2.0.0,0 0.1.0.5.3 0.3,1,1,0 0.1.3.0.0 0.3,4.0.0 0.1.7.0.0 0.3,7.0.0 | 0.5.1.9.9 0.7.2.0.0 | 0.6.8.0.0 0.06.7.0 08.11.7.0 0.110.3.0 0.9.3.2.3 0.113.0.0 0.0.0.0.0 0.11.7.0 0 | 0.1.0.0.8 0.3.1.8.0 0.1.4.6.0 0.3.5.3.0 |
| 8.4.0. 8.6.1.0.0 8.8.2.0.0 | 8.9.11.9.9 0.0.0,9.0 | 9.2 1.8.3 9.4.2.7.6 | 0.6.0.1.6.0.8.1.0.0 | 010.5.5.3 0.0.0.4.0 | 0.2.3.7.6 0.4.6.0 0.2.7.3.9 0.4.8.30 0.2.7.3.9 0.4.8.30 |
| | 80.6.2.3 0.0.7.3.0 80.0.4.0 0.0.0.6.0 8110.6.0 0.1.1.0.0 8113.0.0 0.1.5.3.0 | 0.2 0.3 0 0.4 0.4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 0.0.6.5.3 0.8.41.0.0 0.7.1.0.0 0.0.3.0.0 0.7.5.3.9 0.0.0.0.0 0.7.8.0.0 0.0.10.0.0 | 011, 0, 0, 0, 1, 1, 7, 0 011, 4, 1, 0, 0, 1, 5, 3, 0 011, 7, 8, 3, 0, 1, 8, 10, 0 011, 11, 3, 0, 0, 2, 0, 0, 0 0, 0, 2, 0, 0, 3, 4, 1, 6 | 6.3.2.6.3 6.3.0.0 6.3.6.4.6 6.3.7.3.0 6.3.6.6.6 6.3.7.3.0 |
| 8.6.0 ₄ 8.8.4.6.0 8.00.1.0 | 611.0.1.0 0.1.11.0.0 0.0.1.3.0 0.2.2.0.0 0.0.4.0.0 0.2.0.0.0 0.0.7.8.3 0.2.0.3.0 | 0.4.0.0.6 0.4.4.2.3 0.6.5.7.6 0.4.7.6.0 0.0.0.0.0 | 0 8 3 7 0 0 0 0 5 0 0 0 8 7 0 0 0 0 0 0 0 0 0 8 10 0 0 0 0 0 0 0 | 00.0 4.0 0.27 0.0 0.0 0.0 0.11 3 0.2 11 4.0 | 0.40 7 8 0.0 1 0.0 0.50 0 0 0 7 2 30 0.5 6 0 0 0 7 0 0.0 0.3 6 2 3 0 7 0 9.0 |
| 8.7.0 8.0.1.0.0 8.0.1.0.0 8.0.1.0.0 8.0.1.0.0 8.0.1.0.0 8.0.1.0.0 8.0.1.0.0 8.0.1.0.0 8.0.1.0.0 8.0.1.0.0 8.0.1.0.0 8.0.0 8.0.0.0 8.0 | 0.0.10.10.5 0.3.0.5.0 0.1.2.0.0 0.3.3.0.0 0.1.5.3.0 0.3.7.0.0 0.1.8.5.3 0.3.0.3.0 | 0.5.2.1.6 0.7.3.0.0 0.5.5.5.3 0.7.7.1.6 0.5.8.0.0 0.7.10.0.0 0.5.0.0.0 0.8.1.10.0 | 0.0.3.4.0 0.11.7.0.0 0.0.8.0.0 0.11.6.0 0.10.0.3.0 0.0.2.0.0 0.0.3.8.3 0.0.5.6 0 | 0.18,7.0 0.310.3.0 0.20.2.3 0.4.1.0.0 0.2,3.0.0 0.4.5.0 0 0.2,7.3.0 0.4.6.1.0 | 0.5 1. 10.5 0.6 1. 5.0 0.6 3. 6.0 0.8 5.3.0 0.6 7. 3. 0 0.8 0.0.0 0.7 2. 7 3 0.0 45.0 0.7 2. 7 3 0.0 45.0 |
| 8.7.0 8.0.1.9.0 811.3.0.0 8.0.4.9.9 811.0.7.0 8.0.7.0.0 811.0.9.0 8.0.0.11.3 0.0.0.0,0 8.0.0.11.3 0.0.0.0,0 8.0.0.10.0 0.0.7.1.0 9.0.0.1.0 0.0.0.3.0 9.0.0.1.2 30.1.1 4.0 | | 0.5.8.0.0 0.7.10.0.0 0.0.0.0.0 0.6.1.10.0 0.0.3.4.0 0.8.5.3.0 9.0.0.0.0 0.0.0.0.0 0.7.1.3.0 0.0.3.4.0 | 0.0.7.1.0 0.0.0.0 0 0.0.0.0.0 0.1.0.0.0 0.11.2.0.0 0.1.4.0.0 0.11.5.5.3 0.1.7.0.0 | 0273004616 020000005000 0325305440 03000005800 | 0.7.6.3.0 0.9.8.3.0 |
| 7.00 | 0.3.0.4.8 0.5.2.8.0 0.3.3.6.9 0.5.5.0.0 0.3.6.0.0 0.5.0.0.0 0.3.0.11.3 0.6.0.3.0 | 0.7.4.7.0 00.0 0.0 0.7.7.11.3 0.00.1.0 0.711.3.0 000.1.0.0 0.8.2.6 0 00.40.6 | 011.8.0.0 0.1.11.0.0 0.0.0.3.0 0.2.2.0.0 0.0.3.0.0 0.2.0.0.0 0.0.7.2.3 0.2.0.0.0 | 041.10 0.03.30 0440.300.00.00 048.30 00.00.00 | 0.6 1 8 3 0.0 3.0.0 0.8 9 0 9 000 11.3.0 0.9 0 9 0 011 3.0.0 0.9 2 5 3 011 0.0.0 0.9 5 1 6 011 0.0.0 |
| | 0.3.0.0.0 0.5.0.0.0 0.3.0.11.3 0.0.0.3.0 0.4.1.1.0 0.0.3.0.0 0.4.4.3.0 0.0.0.0.0 0.4.7.0.0 0.0.0.0 0.4.0.8.3 0.7.1.3.0 | 08.540.0 040.6.3.0 06.0.2.3 00.4.7.0 | 0.0.10.7.0 0.3.7.0.0 0.7.2.0.0 0.3.4.0.0 | 05.3.4.0 07.5.9.0 05.5.11.3 07.9.4.6 | 00.3.6.0 11.0.0.0.0 |
| 8.11.0 4. 0.0.3.6.0 0.2.6.1.6 3. 0.0.8.7.0 0.2.1.3.0 3. 0.0.1.8.3 0.3.2.46 8.11.0 4. 0.1.5.0.0 0.3.5.6.0 5. 0.1.6.0.0 0.3.1.0.0 3. 0.1.1.11.3 0.4.2.10.0 | 0.4.7.6.0 0.6.10.0.0 0.4.10.8.3 0.7.1.3.0 0.5.1.10.0 0.7.4.0.0 0.5.5.0.9 0.7.7.0.0 0.5.8.3.0 0.7.11.0.0 0.511.5.3 0.8.2.3.0 | 00.7.1.0 011.9.9.0 0.0.10.5.3 0.0.1.1.0 0.0.1.9.0 0.0.4.0.0 0.0.5.0.0 0.0.7.10.0 | 0.2.0.4.0 0.4.3.0.0 0.2.3.9.0 0.4.0.0.0 0.2.7.3.0 0.4.0.0.0 0.2.0.8.3 0.5.1.6.0 | 0.3.10.6.0 0.5.1.0.0 0.6.2.0.0 0.8.4.7.0 0.6.5.7.0 0.8.8.3.0 0.6.9.2.3 0.6.11.0.0 0.7.0.0.0 0.0.3.6.0 0.7.4.3.0 0.0.7.1.0 | 0.10.10.10.0 11.1 . 5.3.0 |
| Management Transfer of the Control o | 0.511.5.3 0.8.2.3.0 0.0.2.7.0 0.8.5.0.0 0.0.5.0.0 0.8.6.0.0 0.0.0.0 0.0.0.0.0 0.7.0.2.3 0.0.3.3.0 | 005.0.0 0.0.7.10.0 006.4.0 0.0.11.3.0 0.011.8.3 0.1.2.7.0 011.3.00 0.1.6.0.0 | 0.3.2.1.8 0.5.5.0.0 0.3.5.6.9 0.5.6.5.0 0.3.0.0.0 100 0.0.0 | 0711.5.3 10.02.4.0 | 1.0.1.7.6 11.2.46.0 11.0.5.3.0 11.2.6.30 11.0.0.0.0 11.3.0.00 11.1.0 8.3 11.3.3.9.0 11.1.4 4.0 11.3.7.0.0 |
| 9.0.0 ₁₄ 0.2.3.0.0 0.4.6.0.0 0.2.6.0.9 0.4.0.1.6 0.2.9.1.6 0.5.0.3.0 0.3.6.2.3 0.5.3.4.6 | 0.6.0.0.0 0.0.0.0.0 0.7.0.2.3 0.0.3.3.0 0.7.34.0 0.0.6.6.0 0.7.6.6.9 0.0.0.0 | 011.3.00 0.1.6.0.0 211.0.3.0 0.1.9.4.0 8.11.0.7.0 0.2.0.9.0 0.0.0.11.3 0.2.4.1.0 | 0.4.7.3.0 10.6.7.0.0 | 0.8.10.1 6 0.11.1.3.0 | 1.1.8.0.0 11.3.7.6.0 |

A TABLE OF FEET AND INCHES, from 9 foot 1 Inch by 1 foot and 1 quarter of an inch to 11 foot 6, inches and 3 quarter by 1 foot 3 inches.

| Fl.Parts | FI.Parts | F.I.Parts | FI.Parts | THE RESIDENCE OF THE PARTY OF T | F.I.Parts | THE PERSON NAMED IN COLUMN 2 I | FI.Parts | F.I.Parts | FI.Parts | F.I. Parts | F.I. Parts | FI.Parts |
|--|--|---|--|--|--|--|--|---|---|--|--|---|
| 9.1.9 | 9.3.3.3.0 | 0.5.6.6.0 | 9.7.9.9.0 | 9.10. +.0.0 | 10:0.4:3:0 | 1.1 2 | 1.13 | 10.7.2.0.0 | 10.0.5.3.0 | 10.2 2 | 11.1.11.00 | 1.3.0 |
| 3 | 03046 | 0.0.0.0.0 | 0.87.30 | 9.10.7.0.0 | 10.0.10.10.6 | 10.3.2.3.0 | 10.5.2.2.3 10.5.5.7.0 10.5.0.0.0 | 0.7.5.60 | 10.0.8.0.0 | 11.0.0.1.6 | 11.1.11.0.0 11.2.3.5.3 11.2.7.1.6 11.2.10.0.0 | 11.4.0.0.0 |
| N. Mary | 9.5.0.8.3 | 0.0.7.0.0 0.0.0.1.0 0.7.1.3.0 0.7.4.4.0 | 9.0.8.0.0 | 9.11.5.3.0 | 10.1.8.0.0 10.2.8.1.6 10.2.3.5.3 | 10.3.9.0.0 10.4.0.4.6 10.4.3.9.0 | 10.0,0.0.0.0 10.0,3.11.3 10.0,7.4.0 | 10.8.7.0.0 10.8.7.0.0 | 10.10.7.6.0 | 11.1.2.7.6 | 11.3.2.6.0 | 11.5.6.0.0 |
| 9.3.9 | 9.5.3.9.0 9.5.0.0.0 9.5.0.0.0 | 9.7.7.6.0 9.7.0.7.6 9.8.1.9.0 9.8.4.0.0 | 0.0.11.3.0 | 10.0.3.0.0 | 10.2.6.0.0 | 10.4.10.6.0 | 10.7.2.30 10.7.5.8.3 10.7.9.1.0 | 10.0.0.0.0 | 10.11.0:0.0 | 11.2.1.6.0 | 11.4.5.3.0 | 11.0.0.0.0 |
| 9.4.8 | 9.6.4.0.0 9.6.7.0.0 9.6.6.1.6 | 9.8.11.1.6 | | 10.1.7.3.0 | 10.3.11.3.0 | 10.0,0.0.0 10.6.3.4.6 | 0.8.4.0.0 | 10.10.8.0.0 | 11.1.3.0.0 | 11.3.4.0.0 | 11.5.8.0.0 | 11.8.0.0.0 |
| 9.5.0 | 02120 | 0.0.3.4.0 | 100000 | 10.0 | (0,4.9.7.) | 00.0.0.2.0 | 10.0.2.3.0 | 10.11.0.0.0 | 11,1.10.8.3 | 11.4.2.10.0 | 11.0.7.0.0 | 11.9.3.0.0 |
| 9.6.9 | 98.1.5.3 98.4.0.0 98.7.0.9 | 0.0.5.0.0 0.0.0.0.0 0.11.0.1.0 0.11.0.4.0 | 10.0.10.3.0 | 10.3.2.0.0 | 10.5.7.2.3 | 10.7.11.7.6 | 10.10.7.6.0 | 11.0.8.6.0 | 11.3.0.11.3 | 11.5.1.9.0 11.5.5.4.6 11.5.0.0.0 11.6.0.7.6 | 11.7.0.0.0 | 11.10.2.3.0 |
| 9.7.8 | 0.0.1.8.3 | 0,11.0.6.0 | 10.2.2.3.0 | 10.4.7.0.0 | 10.0.5.1.0.0 | 10.8. 9.9.0 10.9.1.1.6 10.9.4.6.0 | 10.11.2.4.8 | 11.2.2.0.0 | 11.4.3.2.3 | 11.0.4.30 | 11.0.4.3.0 | 11.11.0.0.0 |
| 9.8.0 | | 0,11,0,6.0 10,0.0.7.0 10,0.3.0.0 10,0.0.0.0 | | | | | | | | | | 12.0.0.0.0 12.0.4.0.0 12.0.8.3.0 |
| 9.9.2 | Charles and the Control of the Contr | THE RESERVE AND ADDRESS OF THE PARTY OF THE | Control of the Contro | The Personal Property lies and | | Million D. And The Man College of Control of | 111111111111111111111111111111111111111 | | 11 | III TO CONCIO | 11.11.00.00.00 | 12.1.7.0.0 12.1.7.0.0 12.1.11.3.0 |
| 33 | 0.11.11.4.0 10.0.2.5.3 | 10.2.1.7.0 | 10 6 1 6 0 | 10.7.8.9.0 | 10.10.0.2.3 | 11.0.5.7.6 | 11. 2.11.0.9 | 11.2.4.0.0 | 11.7.0.11.3 | 11.10.3.4.0 | 12.0.8.9.0 | 12.2.3.0.0 12.2.6.0.0 12.2.10.6.0 12.3.2.3.0 |
| WALL STATE | 10.0.5.0.0 10.0.8.6.0 10.0.11.7.6 10.1.2.8.3 | 10.3.2.1.6 10.3.5.3.0 10.3.8.4.6 | 10.5.0.10.0 | 10.8.4.8.0 | 10.10.10.1.6 | 11.1.3.9.0 | 11. 3. 9. 4. 6 | 11.5.8.0.0 | 11.8.1.0.0 11.8.5.0.0 11.8.8.7.6 11.0.0.2.3 | 11.10.7.0.0 | 12.1.0.0.0 12.1.4.2.3 12.1.7.10.0 12.1.11.0.0 | 12.3.0.0.0 12.3.0.0.0 12.4.1.6.0 12.4.5.3.0 |
| 11. 11 . 11 | 10.1.5.0.0 10.1.8.0.0 10.1.11.10.0 10.2.2.11.3 | 10.4.2.7.6 | 10.0.2.30 | 10.0.2.3.0 10.0.5.6.0 | 10.11.4.0.0 10.11.8.0.0 10.11.11.4.6 | 11.2.1.10.6 | 11.4.4.3.0 | 11.0.10.0.0 | 11.9.3.0.0 | 11.0.0.0.0 | 12.2.3.3.0 | 12.4.0.0.0 12.5.0.0.0 12.5.4.6.0 |
| 10.0.0 | 10.2.0.0.0 10.2.0.0.0 10.3.0.1.0 10.3.3.2.3 | 10.5.0.0.0 10.5.3.1.6 10.5.6.3.0 | 10.7.6.0.0 10.7.0.2.3 10.8.0.4.6 | 10.10.0.0.0 | 11.0.6.0.0 | 11.3.0.0.0 | 11.5.0.0.0 | 11.8.3.0.0 | 11.10.0.0.0 | 12.1.0.0.0 | 12.3.6.0.0 | 12.0.0.0.0 12.0.3.0.0 12.0.7.0.0 |
| 10.1.0 | | 10.0.0.6.0 | 10. 9. 6.00 | 10.11.00 | 111720 | 11 1 1 1 0 | 46 7 00 | 1100000 | 11.11.8.3.0 | 12.2.0.0.0 | 12.4.5.0.0 12.4.8.0.0 12.5.0.5.3 12.5.4.1.6 | 12.7.3.0.0 12.7.0.0.0 12.7.0.0.0 |
| 10.2.0 | 10.4.0.6.0 10.4.0.6.0 10.5.0.7.6 | 10.7.1.0.0 | 10.9.7.6.0 10.9.10.8.3 10.10.1.10.6 | 11.0.2.0.0 | 40060 | | 1 2 6 2 | 1. 10 . 2 . | 12.0.0.11.3 | 12.3.5.0.0 12.3.5.0.0 12.3.8.7.0 12.4.0.3.0 | 12.6. 3.2.3 | 12.8.0.0.0 |
| 10.3.0 | 10.5.3.8.3 10.5.0.0.0 10.5.0.0.0 | 10.8.1.6.0 | 10.10.8.3.0 | 11.1.3.0.0 | 11.3.0.9.0 | 11.6.4.0.0 | 11.8.7.0.0 | 11.11.0.0.0 | 12.2.0.0.0 | 12.4.7.0.0 | 12.0.10.0.0 | 12.0.5.3.0 |
| 10.4.0 | 10.6.3.11.3 10.6.7.0.0 10.6.10.0.0 | 10.0.2.0.0 | 10.11.9.0.0 | 11,2,4,0.0 | 11.4.7.8.3 | 11.7.2.7.0 | 11.0.0.1.0 | 12.0.4.6.0 | 12.2.11.5.3 | 12.5.2.0.0 12.5.6.4.6 12.5.10.0.0 12.6.1.7.6 | 12.8.5.0.0 | 12.10. 4.0.0 12.10. 8.3.0 12.11. 0.0.0 |
| 10.5.9 | 10.7.7.3.0 | 10.0.8.3.0 10.0.11.4.6 10.10.2.6.0 10.10.5.7.6 | 11.0.3.4.6 | 11.2.10.0.0 | 11.5.8.11.3 | 11.8.0.9.0 | 11.10.7.10.0 | 12.1.0.0.0 | 12.3.10.1.0 | 12.7.0.6.0 | 12.0.0.4.6 | 12.11.7.6.0 12.11.11.3.0 13.0.3.0.0 |
| 10.6.9 | 10.8.1.4.0 10.8.4.5.3 10.8.7.0.0 | 10.10.8.0.0 10.10.11.10.6 10.11.3.0.0 | 11.1.7.3.0 | 11.3.11.0.0 | 11.0.3.0.0 | 11.9.2.3.0 | 11,11,0-7.0 | 12.2.3.0.0 | 12.5.7.0.0 | 12.7.7.9.0 12.7.11.4.6 | 1210.6.0.0 | 13.0.0.0.0.0 |
| A COUNTY | 10.0.4.8.3 | 10.0.0.4.6 | 11.2.4.0.0 | 11.5.0.6.0 | 11.7.11.5.3 | 11.10.0.4.6 | 12.1.2.0.0 | 12.3.3.6.0 | 12.6.6.2.3 | 12.8.6.7.6 | 12.11. 2.2. 3 | 13.1.0.0.0 13.2.1.0.0 13.2.5.3.0 |
| 4433 | 10.10.1.10.0 | 11.0.0.0.0 | 11. 3. 2.5. 3 | 11.0.4.0.0 | 11.8.6.0.9 11.8.9.4.6 11.0.0.8.3 | 11.10.10.0.0 11.11.1 .10.6 11.11.5.30 11.11.8.7.6 | 12.1.0.3.0 12.1.0.8.3 12.2.1.1.6 12.2.4.6.9 | 12.4.2.0.0 12.4.5.6.0 12.4.0.0.0 12.5.0.6.0 | 12.0.0.0.0 12.7.1.3.0 12.7.4.0.6 12.7.8.5.3 | 12.0.0.0.0.0 | 13.0. 8.7.6 13.1. 6.3.0 | 13.3.4.0.0 13.3.4.0.0 13.3.8.3.0 |
| The state of the s | 10.10. 8.0.0 10.10.11.0.0 10.11.2.1.6 10.11.5.2.3 | 11.1.4.0.0 | 11.4.0.4.0 | 11.6.8.0.0 11.6.11.3.0 11.7.2.6.0 11.7.5.0.0 | 11.0.4.0.0 | 12.0.0.0.0 12.0.3.4.6 12.0.6.9.0 12.0.10.1.6 | 12.2.8.0.0 12.2.11.5.3 12.3.2.10.6 12.3.6.3.0 | 12.5.4.0.0 12.5.7.6.0 12.5.11.0.0 12.6.2.6.0 | 12.8.0.0.0 12.8.3.6.0 12.8.7.1.0 12.8.7.1.0 | 12.10. 8.0.0 12.10.11.7.6 12.11. 3.3.0 12.11.6.10.6 | 13.1.4.0.0 13.1.7.8.3 13.1.11.4.6 13.2.3.0.0 | 13.4.0.0.0 13.4.3.0.0 13.4.7.0.0 |
| 10.9.0 | 10.11.8.3.0 10.11.11.3.0 11.0.2.4.6 11.0.5.5.3 | 11.2.4.0.0 | 11.5.0.0.0 | 11.7.0.0.0 | | 12.1.1.0.0 | | 12.6.6.0.0 12.6.0.6.0 12.7.1.0.0 | 12.0.2.3.0 | 12.11.10.0.0 13.0.2.1.6 13.0.5.9.0 | 13.2.0.0.0 | 13.5.3.0.0 13.5.0.0.0 13.5.0.0.0 |
| 10.10.0 | 11.0.8.6.0 | 11.3.5.0.0 | 11.6.1.6.0 | 11.8.10.0.0 | 11.11.6.6.0 | 12.2.3.0.0 | 12.4.11.0.0 | 12.8.3.0.0 | 1210.4.6.0 1210.8.0.0 1210.11.7.0 | 13.1.1.0.0 13.1.4.7.0 13.1.8.3.0 | 13.3.0.0.0 | 36.0.0.0 |
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| 11.0.0 | 11.2.5.11.3 | 11.5.2.0.6 | 11.7.11.0.0 | 1.11.3.3.0 | 12.1.5.8.3 | 12,4.0.0.0 | 12.6.81.6.0 12.7.3.0.0 12.7.6.5.3 | 2.0.8.6.0 2.0.0.0.0 2.0.3.6.0 | 130.5.5.3 | 13.3.2.4.6 | 13.5.11.3.0 | 3.6.6.3.0 |
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| Water | 1.7.4.1.6 | 1.0.71.1.0 P 1.0.2.3.0 P | 2,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0 | 3730 | 20.3.00 | 2.0.3.4.0 2.0.3.9.0 2.0.0.9.0 | B.O. 1.5.3 P.O. 4.10.0 S.O. 8.3.0 | 3.2.77,6.0 3.3.3.0.0 3.3.0.6.0 | 3.5.0.0.0 3.5.0.0.0 3.6.1.1.6 3.6.4.8.3 | 3.6.7.7.6 | 311.2.0.0 311.5.8.3 311.0.4.0 40.1.0.0 | 4.2.0.0.0 4.2.3.0.0 4.2.7.0.0 4.2.11.3.0 |
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A TABLE OF FEET AND INCHES

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| 34311 | 1.0.4 | 1.02 | 1.03 | 1.1.0 | 1.14 | 1.12 | 1.13 | 1.2.0 | 1.24 | 1.2 2 | 1.23 | 1.3.0 |
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| 11.11.42 | 12.1.11.00 | 12.5.2.7.0 | 12.8.2.3.3 | 12.11.2.30 | 31.000 32.00 32.540 32.683 | 13.4.0.0.0 13.5.1.00 13.5.2.30 13.5.2.30 | | 13.10.10 0.0 13.11.1 0.0 13.11.5 0.0 | 14.2. 4.10.0 | 14.4.9.6.0 14.5.1.1.6 14.5.4.0.0 14.5.8.4.6 | 4.7.0.3.0 4.8.0.113 4.8.4.7.6 4.8.8.3.5 | 14.10.0.0. 14.11.0.0. 14.11.4.0. 14.11.8.3. |
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| 1.8.0 | | 2.2.5.0.7.0 | | 2.3.4.0.0 | I street seems to the seems | 2.30.0.0 2.30.1.6 2.4.2.3.0 2.40.4.6 | The state of the s | 2.4.40.0 2.4.8.3.0 2.5.0.0.0 2.5.40.0 | | | The second secon | 2.6.0.0 |
| 1.9.4 | CONTRACTOR OF STREET | - | 2.3.6.0.0 2.3.0.6.3 2.4.2.6.0 | | 2.4.0.3.0 2.5.1.4.0 2.5.5.5.3 | 25.27.0 | 2.5.7.1.3 2.6.6.1.3 2.6.4.3.0 | 2.6.5.6.0 | 27700 | 2.6.7.6.0 2.0.11.0.0 2.7.4.3.0 2.7.8.7.0 | | 2.7.0.0. 2.8.3.0. 2.8.7.6. |
| 1.10.0 | 2.3.11.0.0 2.4.3.3.0 2.4.7.1.0 2.4.10.11.3 | 2.4.5.0.0 2.4.8.10.0 2.5.0.0.0 2.5.4.7.0 | 2.4.10.6.0 2.5.3.5.3 2.5.0.4.0 2.5.10.3.0 | | | | | 2.7.10.0.0 | 2.8.6.5.3 | 28.5.4.0 28.9.9.9.0 2.0.2.1.0 | 2.8.0.0.0 2.8.10.11.3 2.9.3.4.6 2.9.7.9.9 | 2.0.4.0. |
| The state of | 2.5.6.6.0 2.5.0.4.6 2.6.2.2.3 | | | 2.7.8.0.0 | | 2.7.7.6.0 2.7.11.7.6 2.8.3.0.0 2.8.7.10.6 | 2.8.9.7.3 2.8.8.7.3 2.9.1.0.9 | | THE RESERVE AND PARTY AND PARTY AND PARTY AND PARTY. | 2.0.0.00 | 2.10.4.8.3 2.10.0.1.6.0 2.11.1.6.0 | 2.0.0.0.0 2.11.3.0 2.11.7.0 3.0.0.0 |
| 2.0.0 | 2.6.6.0.0 2.6.9.9.9 2.7.1.7.6 2.7.5.5.3 | 2.7.310.0 | 2.7.0.11.3 2.8.1.10.0 2.8.5.0.9 | 2.8.4.0.0 | 1.9.0.2.9 | 20.4.1.0 20.6.3.0 200.4.0 | 2.0.0.2.4.0 2.10.2.4.0 2.10.0.0.0 | 2.11.0.9.0 | 2.11.2.7.6 | 2.11.4.4.0 2.11.8.9.0 3.0.1.1.0 | 3.0.7.39 3.0.1.0.0 | 3.0.4.0.0 |
| 1. J. W. 1. | 2.7.9.3.0 2.8.1.0.0 2.8.4.00 2.8.8.3 | 2.9.3.1.0 | + | 2.10.8.0.0 | 2.10.10.5.3 | 2.10.8.7.0 2.11.0.0.0 2.11.4.10.0 | 2.11.11.3.9 | 3.0.5.0.0 | 30.3.0.0 | 3.7.3.3.8 | 3.2.7.0.0 | 3.2.3.0.0 |
| The state of the s | 2.0.0.0.0 2.0.4.3.0 2.0.6.1.0 2.0.1.11.3 | | 2.10.1.0.6 2.10.5.5.5 2.10.0.4.1 2.11.1.3.4 | 2.11.8.0.0 | | 241.0.0.0 30.1.1.0 30.5.3.0 30.0.4.0 | 3.0.7.8.3 | 3.1.0.0.0 | 3.2.1.1.6 | 3.2.3.4.0 | 3.3.0.0.0 | 3.3.0.0 |
| 2.3.0 | 2.10.3.90 2.40.7.0.0 2.40.11.4.0 2.11.3.2.3 | | | 3.0.0.0.0 | 3.0.0.9.0 | 3.1.1.0.0 | 3.2.0.5.3.2 | 3.2.7.3.0 3.2.7.3.0 3.2.1.6.0 3.3.30.0 | | | 3.2.0.0.9 | 3.40.00 3.5.3.00 3.5.7.00 3.5.7.00 |
| 34 | 3.0.3.7.6 3.0.3.7.6 3.0.6.5.3 | | | 31, 4.0.6 31, 8.0.6 3.2.8.0.6 3.2.40.6 | | | | | | A CONTRACT MANY MANY BOOK | | |
| 2.5.0 | 3.0.40.3.0 3.1.2.0.0 3.1.5.40.0 3.1.0.8.3 | 3.1.5.6.0 | 3.2.0.04 3.2.4.8. 3.3.8.6. | 3.3.0.0.0 | 3. | 3.3.40.6.6 3.4.2.7.6 3.4.6.6.6 3.4.6.6.6 | 3.4.5.0.0 | 3.5.1.0.0 | 3.5.6.3.6 | 30.7.10.0 | 30.00.00 | 3 2 3 8 |

A TABLE OF FEET AND INCHES
from a foot 6 inches by 1 foot 3 inches and 1 quarter to 4 foot 11 inches and 3 quarter by 1 foot 6 inches

| FLParts | RI Parts | FIParis | FI Parts | FIParts | ELParts | FLParts | EI.Parts | FI Parts | El Parts | F.I.Paris | ELParis | F.I. Parts |
|----------|---|--|---|--|--|--|---|---|--|---|---|--|
| 14 13 13 | 1.3 4 | 7.3 2 | 1.33 | 1.4.0 | 1.44 | 1.4 2 | 1.43 | 1.5.0 | 3.7.1.00 | 3.7.0.00 | 1.5.3 | 3.0.0.0.0 |
| 2.0.0 | 338/13 | 3 3 0 0 0 0 | 3.4.4.3.9 | 34.8.0.0 | 35.7.8.3 | | 3.5.10.0.0 3.6.0.0.0 3.6.11.0.9 | | 3.7.5.0.0 | 3.8.1.40 | 3.6. 4.0.0 3.6. 6.11.3 3.0.5.0.0 3.0.5.0.0 | |
| 2.7.0 | 3 4 9 0 0 | | | | 3.6.3.0.0 | 3.6.7.6.0 3.6.11.7.6 3.7.3.00 3.7.7.60 | 3.7.3.3.0 3.7.7.3.3 3.6.3.0.0 | | | | | |
| 2.8.0 | 37,000 | 3.5.7.60 | 36.7.00 | 3.6.8.0.0 3.7.0.0.0 3.7.8.0.0 | 3.7.4.0.0 3.7.8.0.0 3.8.0.1.6 3.8.4.2.3 | 3.8.0.0.0 3.8.4.1.0 3.8.8.3.0 3.9.6.4.6 | 3.8.8.0.0 3.0.2.3 3.0.4.4.0 3.0.8.0.0 | 3.0.40.0 3.0.6.3.0 3.0.0.0.0 3.0.4.0.0 | | 3.10.8.0.0 3.11.0.4.0 3.11.4.0.0 3.11.0.1.0 | 341.4.0.0 3.11.8.5.3 4.0.0.0.0 4.0.5.3.0 | 4.0.0.0.0 |
| 2.9.0 | 3.6.11.3.0 | 307,00 | 3 7 3 8 9 3 8 3 6 0 | 3.8.0.0.0 | 3.8.8.3.0 3.0.4.3.3 3.0.4.4.6 3.9.8.5.3 | 3.0.4.6.0 3.0.8.7.6 3.10.8.0.0 3.10.4.10.6 | 3.10.0.0.0.0 3.10.4.11.3 3.10.0.1.0 3.11.1.3.0 | 3.11.1.3.0 | 3.11.5.3.0 3.11.0.0.0 4.0.1.00 4.0.0.2.3 | 4.0.1.6.0 4.0.5.10.6 4.0.10.3.0 4.1.2.7.0 | #.0.0.0.0 #.1.0.7.0 #.1.11.0.0 | |
| 2.10.0 | 3.7.3.6.0 | 3.7.11.0.0 3.8.2.0.0 38.6.0.0 38.10.7.0 | | 3.0.4.0.0 | 3.10.0.6.0 3.10.4.6.9 3.10.8.7.6 3.11.0.8.3 | 3.10.9.0.0 3.11.5.3.0 3.11.9.4.6 | 3.11.5.6.0 3.11.0.8.3 4.0.1.10.6 4.0.6.0.9 | #.0.3.0.0 #.0.6.3.0 #.0.10.6.0 | 4.0.0.6.0 4.1.2.0.0 4.1.7.1.6 4.1.11.5.3 | 4.1.7.0.0 4.1.11.4.6 4.2.3.0.0 4.2.8.1.6 | 4.2.3.6.0 4.2.7.11.3 4.3.0.4.6 4.3.4.9.0 | 4.3.0.0.0 4.3.4.0.0 4.3.0.0.0 |
| 2.11.0 | 38.5.00 | | 3.0.11.3.0 3.0.3.2.3 3.0.7.1.0 3.10.11.0.0 | 340.8.0.0 341.0.0.0 341.4.0.0 | 3.11.4.0.0 3.11.8.0.0 4.0.0.00 | 4.0.1.6.0 | 4.0.10.3.0 4.1.2.5.3 4.1.6.7.6 4.1.10.9.9 | 4.1.7.0.0 4.1.11.3.0 4.2.3.0.0 | #.2.3.0.0 #.2.8.0.0 #.3.0.4.6 #.3.4.8.3 | 4.3.0.0.0 | 4.3.9.3.0 4.4.1.8.3 4.4.6.1.6 4.4.10.6.9 | 4.4.6.0.0 4.4.0.6.0 4.5.3.0.0 4.5.7.6.0 |
| 3.0.0 | 3.0.0.0.0 3.0.0.0.0 3.0.4.7.0 | 310.6.0.0 | 3.11.3.0.0 | 4.0.0.0.0 4.0.4.0.0 4.0.8.0.0 | 4.0.0.0.0 | 4.1.6.0.0 4.1.10.1.6 4.2.3.3.0 4.2.6.4.6 | 4.2.3.0.0 4.2.7.2.3 4.2.11.4.0 4.3.3.0.0 | 4.3.0.0.0 4.3.4.3.0 4.3.8.0.0 | 4.3.0.0.0 4.4.1.3.0 4.4.5.7.0 4.4.0.11.3 | 4.4.6.0.0 4.4.0.4.6 4.5.2.0.0 4.5.7.1.6 | 4.5.3.0.0 4.5.7.5.3 4.5.11.0.0 4.0.4.3.0 | 4.6.0.0.0 4.6.0.0.0 4.7.1.6.0 |
| 3.1.0 | 3.11.0.3.0 | 3.11. 9.6.0 4.0.1. 4.6 4.0.5.3.0 4.0.9.1.6 | 4.0.6.0.0 4.0.10.8.3 4.1.3.7.0 | 4.1.4.0.0 | 4.2.1.3.0 4.2.5.3.0 4.2.9.4.0 | 4.2.10.6.0 4.3.2.7.6 4.3.6.0.0 | 4.3.7.9.0 4.31,11.3 4.44.1.6 | 4.4.5.0.0 4.4.0.3.0 4.5.1.0.0 | 4.5.2.3.0 4.5.6.6.0 4.5.10.10.6 4.6.3.2.3 | 4.5.11.6.0 4.6.3.10.6 4.6.8.3.0 4.7.0.7.6 | #.6.8.0.0 #.7.1.2.3 #.7.5.7.6 #.7.6.0.0 | 4.7.6.0.0 4.7.0.6.0 4.8.3.0.0 4.8.7.6.0 |
| 3.2.0 | 4.0.3.6.0 | 4.1.1.0.0 4.1.4.0.0 4.1.8.0.0 | 4.1.10.0.0 4.2.3.5.3 4.2.0.4.0 | 4.2.8.0.0 4.3.0.0.0 4.3.4.0.0 | 4.3.5.6.0 4.3.9.6.9 4.4.1.7.6 | 4.4.3.0.0 | 4. 5.0.6.0 4. 5. 4.8.3 4. 5. 8.10.0 | 4.5.10.0.0 4.6.2.3.0 4.6.6.6.6 | 4.6.7.6.0 4.6.11.9.9 4.7.4.1.6 | 4.7.5.0.0 4.7.0.4.6 4.8.1.0.0 4.8.6.1.6 | 4.8.2.6.0 | #.0.0.0.0 #.0.4.0.0 #.0.0.0.0 #.0.1.0.0 |
| 3.3.0 | 4.1.6.0.0 | 4.2.4.6.0 4.2.8.4.6 4.3.0.3.0 4.3.4.1.6 | 4.3.3.3.3.9 4.3.0.1.0 | 4.4.0.0.0 4.4.4.0.0 4.4.8.0.0 | 4.4.0.0.0 4.5.1.0.0 4.5.5.10.0 | 4.5.7.6.0 4.5.71.7.0 4.6.3.0.0 | 4.0.5.3.0 | 4.7.3.0.0 4.7.7.3.0 4.7.7.3.0 | 4.8.0.0.0.0 | 4.8.10.6.0 | 4.0.8.3.0 4.10.0.8.3 4.10.5.1.0 | 4.10.6.0.0 4.10.10.6.0 4.11.3.0.0 |
| 3.4.0 | 4.2.0.2.3 4.2.10.0.0 4.3.1.0.0 4.3.5.7.6 | 4.3.8.0.0 4.3.1.10.0 4.4.3.00 4.4.7.7.0 | 4.4.6.0.0 4.4.0.11.3 4.5.1.10.0 | 4.5.4.0.0 4.5.8.0.0 4.0.0.0.0 | 4.6.2.0.0 4.6.6.0.0 4.6.6.0.1.6 | 4.7.0.0.0 4.7.4.1.0 4.7.8.30 | 4.7.10.0.0 4.8.2.2.3 4.8.0.4.0 | 4.8.8.0.0 4.0.0.3.0 4.0.4.0.0 | 4.0.6.0.0 | 4.10.4.0.0 4.10.8.4.0 4.11.0.0.0 | 4.11.2.0.0 4.11.6.5.3 4.11.10.10.0 | 3.0.0.0.0 3.0.4.0.0 5.0.9.0.0 5.1.1.0.0 |
| 3.5.0 | 4.4.1.3.0 | 4.4.11.6.0 | 4.5.0.0.0 | 4.0.8.0.0 | 4.7.6.3.6 | 4.8.4.6.0 | 4.0.2.0.0 | 4.10.1.0.0 | 4.10.11.3.0.0 | 5.0.1.10.0 5.0.6.3.0 | 5.0.7.0.0 | 5.1.0.0.0 5.1.10.0.0 5.2.3.0.0 |
| 3.6.0 | 4.5.4.6.0 | 4.6.3.0.0 | 4.7.1.6.0 | 4.8.0.0.0 | 4.8.10.6.0 | 4.0.0.0.0 | 4.10.7.6.0 | 4.11.6.0.0 | 5.0.4.6.0 | 5.1.3.0.0 | 5.2.1.0.0 5.2.5.11.3 5.2.10.4.0 | 5.3.0.0.0 5.3.4.6.0 5.3.0.0.0 |
| 3.7.0 | 4.0.7.0.0 | 4.7.0.0.0 4.7.0.0.0 4.7.0.4.0 4.8.2.3.0 | 7.8.5.3.0 4.8.0.2.3 | 4.0.4.0.0 | 4.10.2.9.0 | 4.11.1.6.0 | 5.0.0.3.0 | 5.0.11.0.0 | 5.2.2.0.0 | 5.2.8.0.0 5.3.0.0.0 5.3.5.3.0 | 5.3.7.3.0 5.3.7.8.3 5.4.4.6 | 5.4.0.0.0 5.4.0.0.0 5.5.30.0 |
| 3.8.0 | 4.7.7.23 4.7.11.0.0 4.8.3.0.0 4.8.6.7.0 | 4.8.0.0.0 4.8.10.0.0 4.0.1.10.6 4.0.5.0.0 | 4.0.0.0.0 | 4.11.0.0.0 | 4.11.7.0.6 | 5.0.6.0.0 | 5.1.5.0.0 | 5.2.4.0.0 5.2.6.3.0 5.3.8.6.0 | 5.3.3.0.0 5.3.7.3.9 5.3.71.7.0 | | 5.5.1.0.0 | 5.6.0.0.0 3.6.4.6.0 3.6.9.0.0 |
| 3.9.0 | 4.8.10.5.3 4.0.3.3.0 4.0.0.0.0 | 4.9.9.7.6 4.10.1.6.0 4.10.5.4.6 4.10.0.3.0 | 4.11.0.9.0 | 5.0.4.0.0 | 5.0.11.3.0 | 5.1.10.6.0 | 5.2.0.0.0 | 5.3.0.0.0 | 5.4.8.3.0 | 5.5.7 0.0 | 5.6.6.0.0 | 5.7.6.0.q 3.7.10.6.0 3.9.3.0.0 |
| 3.10.0 | 4.10.1.8.3 4.10.5.6.6 4.10.9.3.6 | 4.11.1.1.6 | 5.0.4.6.0 | 5.1.4.0.0 | 5.2.3.6.6 | 5.3.3.0.0 | 5.3.0.3.6 5.3.0.3.6 5.4.2.6.6 5.4.6.8.6 | 5.5.2.0.0 | 5.6.1.6.0 | 5.0.0 7.0 5.7.1.0.0 5.7.5.4.0 3.7.5.6.0 | | 3.0.0.0.0 3.0.4.6.0 3.0.0.0.0 |
| 3.11.0 | 4.11.4.11.3 | 5.0.4.7.6 | 5.1.8.3.0 | 5.2.8.0.0 | 5.3.7.0.6 | 5.4.7.0.0 | 5.5.3.0.6 5.5.7.3.0 5.5.11.5.3 5.6.3.7.0 | 5.6.11.3.0 | 5.7.11.0.9 | 5.8.6.6.6 | 5.0.6.3.0 5.0.0.8.3 5.0.3.6 | 5.10.0.0.0 5.10.0.0.0 5.11.3.0.0 |
| 4.0.0 | 5.0.8.2.3 5.1.0.0.0 5.1.3.0.0 | 3.1.8.1.6 5.2.0.0.0 5.2.3.40.6 | 5.3.0.0.0 | 5.4.0.0.0 | 5.5.0.0.0 | 5.6.4.1.0 | 5.7.0.0.0 5.7.4.2.3 5.7.8.4.2.3 | 5.8.0.0.0 5.8.4.3.0 | 5.0.4.3.9 | 5.10.4.4.0 | 5.11.0.0.0 | 6.0.0.0.0 6.0.4.6.0 6.0.9.0.0 |
| 4.1.40 | 3.1.11.5.3 5.2.3.3.0 5.2.7.0.0 | 5.2.11.7.6 5.3.3.6.0 5.3.7.4.6 | 5.3.7.0.0 5.3.11.9.0 5.4.3.0.0 5.4.7.8.3 | 3.5.0.0.0 5.5.4.0.0 5.5.8.0.0 | 3.6.6.2. 3.6.4.3.6 3.6.8.3.6 | | 5.8.0.0.9 5.8.4.9.0 5.8.8.11.3 | 5.0.0.0.0 5.0.5.0.0 5.0.5.0.0 5.0.0.3 5.0.0.3 | 5.10.5.3.0 | 5.11.5.0.0 | 0.0.5.0.0 | 6.1.0.0.0 |
| 4.2.0 | 5.3.0.0.0 5.3.0.0.0 5.3.10.3.0 | 3.4.3.3.6 2.3.4.0.00 2.3.4.0.00 | 3.5.3.6.0 5.5.7.0.0 5.5.7.5.3 | 5.0.4.0.0 5.0.8.0.0 5.7.0.0.0 | 3.7.4.5. 5.7.8.6.6 3.8.0.6.6 | 5.8.9.0.0 | 5.0.5.3.9 5.0.0.0.0.0 5.10.1.8.3 | 5.10.10.0.0 | 5.11.10.0.0 | 6.0.11.0.0 | 6.1.7.0.6 6.2.3.11.3 6.2.3.40 | 0.3.0.0.0 |
| 4.3.0 | 3.4.9.9.0 | 3.5.0.7.0 5.5.0.0.0 5.6.3.4.0 | | 5.7.8.0.0 5.8.0.0.0 5.8.4.0.0 | THE RESERVE THE PARTY NAMED IN | 5.0.0.4.0 5.10.1.6.0 5.10.5.7.0 | 5.11.0.5 | 0.0.3.0.0 | 6.1.3.0.0 | 0.2.4.0.4 | 0.3.5.3.0 | 6.4.0.0.0 6.4.0.6.0 6.5.3.0.0 |
| 4.4.0 | 3.5.0.2.3 5.0.1.0.0 5.0.4.0.0 | 2 5.0.0.3.0 3.0.10.1.0 2 5.7.2.0.0 2 5.7.5.10.0 | 3.7.71.0.9 3.8.3.0.0 3.8.3.11.3 | 5.9.0.0.0 5.9.4.0.0 5.9.8.0.0 | 5.10.0.11. | 3.11.1.10.0 5.11.0.0.0 5.11.0.1.1 | | 6.1.3.9.0 6.1.8.0.0 6.2.0.3.0 | 0.2.4.8. | 0.3.5.7.0 | 0.4.0.0.0 | 0.5.7.0.0 0.6.0.0.0.0 0.6.4.6.0 0.6.0.0.0 |
| 4.5.0 | 5.0.8.7.0 5.7.0.5. | 2 5.7.0.0.0 3 5.8.1.7.0 2 5.8.5.0.0 | 5.0.0.0.0 5.0.0.0.0 | 5.10.0.0.0.0 5.10.4.0.0 5.11.0.0.0 | | | | 0.2.8.0.0 | 6.3.9.11.3 | 0.5.3.0.0 | 0.0.0.3.6 | 6.7.4.6.0 6.7.6.0.0 6.7.6.0.0 |
| 4.6.0 | 5.8.3.8. 5.8.7.6. | | | | 0.0.5.4 | 0.1.0.0. | 0 6.30.3.9 | 0.4.0.0.0 | 0.5.3.2.3 | 0.0.4.7.0 | 6.7.6.0.6 6.7.10.6.4 6.8.2.11.3 | 6.8.7.6.0 6.0.0.0.0 6.0.4.6.0 6.0.4.6.0 6.0.4.6.0 |
| 4.6.0 | 5.8.7.6. 5.8.11.3.6 5.9.3.11. 5.9.6.11. | 5.10.4.0.0 5.10.8.7.0 5.11.0.6.0 | 5.10.10.6.0 5.11.2.5.3 5.11.0.3.6 6.0.2.3.0 6.0.0.2.3.0 | 0,0,0,0,0 | 6.2.5.0. 6.2.0.0 | 0 0.3.3.4.6 0 0.3.7.6.6 | 0.45.0.6 | 0.5.0.0.0 | 6.6.8.5. | 6.7.76.1.1 6.8.2.6.0 | 6.8.11.0.0 | 0.0.1.0.0 0.0.0.0.0.0 0.0.0.0.0 0.1.3.0.0 |
| 4.8.0 | 5.10.0.4. 5.10.10.2. 5.11.2.0. | 5,11.0,0.0 5,11.4,4.0 5,11.6,3.0 5,0.0.7.0 0,0.4.0.0 | 0.0.10.1.0.0 | 0.2.8.0. | 0.3.1.10. | 0 6.5.0.0. | 0.5.9.9.9 | 0.6.11.9.0 | 6.8.6.04 | 6.9.3.7.0 | 0.10.5.0.4 | 7.0.0.0.0 |
| 3 | 0.0.1.5. | 0 0.0.4.0.0 0 0.0.7.0.0 6 0.0.11.0.0 3 0.1.3.7.0 | 0.2.5.9.9 | 0.3.4.0.0 | 0.40.2 | 0 6.5.0.0. 0 5.5.3. 0 5.8.3. 0 6.0.4. 0 6.6.4.6. | 0 6.7.6.9 | 0.8.0.0.0 | 6.9.6.11.3 | 0.10.4.0.1 0.10.0.1.1 0.11.1.0.1 0.11.5.10.1 | 7 0 20 | 7.0.0.0.0 7.1.0.0.0 7.1.0.0.0 7.1.0.0.0 7.2.3.0.0 7.2.7.0.0 |
| * 53 | 0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0. | 0 0.1.7.0.0 | 6.3.0.6.6 6.3.0.6.6 6.3.0.6.6 | 0.5.0.0. | 0.5.2.3 0.5.0.3 0.6.0.2.5 | 0 0.0.4.6. 0 0.0.4.6. 0 7.0.9. 0 7.4.0. 0 0.7.9.0. | 0 6.8.3.12 | 0.00.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0 | 0.10.7.00 | 6.11.5.10 6.11.60.3. 7.0.2.7. | 7.1.5.0. | |
| 4.10.0 | 0.2.0.3. | 0 6.211.0.0 0 6.3.2.0.0 6 6.3.6.0.0 3 6.3.6.7.0 | 0.5.9.3.9 | 0.5.4.0. 0.5.6.0. 0.6.4.0. 0.6.4.0. | 0.7.0.9. | 0.8.5.3. | 0 0 8.11.6.0 0 6.0.3.8. 0 6.0.5.0.5 0 6.10.6.0.5 | 0.10.10.6.0 | 7.0.5.5 | 7.8.7.0. 7.8.7.0. 7.1.3.9. 7.2.0.6. | 7.1.0.6. 7.2.6.4. 7.2.6.6. | 7.3.0.0.0 7.3.4.0.0 7.4.0.0 7.4.0.0.0 |
| 4.11.0 | 037,2 | 0 0 4 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 6.6.5.0.5 | 00.00 | 0 7.0.0 0 0 3.0 0 0 8.0.0 0 0 8.0.0 | 3 6.6.1.6 | 0 0,10,4.3. | 7.0.3.0.0 | 7.1.10.8 | 7.3.9.3 | 7.4.40 | 7.4.0.0.0 7.40.0.0 7.3.3.0.0 9.7.3.7.0.0 |

A TABLE OF FEET AND INCHES
from 5 foot by 1 foot 3 inches and 1 Quarter to 7 foot 5 inches and 3 quarters by 1 foot 6 inches.

| ELPart | FLParts | FIParts | FT Parts | ET Posse | FIR | A CANCELLO PROPERTY AND A STREET | TELE | The D | Justin Ceres | | o unches. | 11.11 |
|---------------------|--|--|--|---|--|--|---|--|---|--|---|--------------------------------------|
| AND CASE TO SEE THE | 1.3 4 | 1.3 2 | 1.3 3 | 1.4.0 | F.I. Paris | 1.4 5 | 1.4.3 | F.I.Parts | F.I. Paris | F.I. Parts | F.I. Parts | F.I.Parts |
| 5.0.50 | 0.4.30.0 | 6.3.6.0.0 | 6.0.0.0.0 | 08.000 | 6.9.30.0 | 6.10.6.0.0 | 6.11.0.0.0 7.0.1.2.3 | 7.1.0.0.0 | 7.2.30.0 | 7.3.0.0.0 | 7, 4.9.0.0 | 7.6.0.0.0 |
| 5.1.0 | 6.5.6.3.6 | 6.0.0.6.0 | 6.8.0.9.0 | 0.0.0.0.0 | 6.10.7.30 | 6.11.0.0.0 | 7.0.0.0.0 | 7.2.5.00 | 7.3.3.3.63 | 7.431.00 | 7.0.2.0.0 | 7.9.9.8.8 |
| 3 | 00.000 | 0.7.5.30 | 6.8.8.6.6 | 6.6.6.0.0 | 6.11.7.5.3 | 7.0.8.0.0 | 7.1.10.1.3 | 7.3.5.0.0 | 7,40.00 | 7.3.3.0.6 | 7.0.7.2.3 | 7.7.10.6.0 7.8.3.0.0 7.8.7.0.0 |
| 3.2.4 | 0.7.5.1.0 | 0.8.40.0 | 0.0.4.0.0 | 0.0.8.0.0 0.4.0.0 0.4.40.0 | 7.0.30.0 | 7.1.3.0.9 | 7.3.20.6.0 | Z 3.0.0.0 Z 4.0.00 | 75.1.0.0 | 7.0.5.0.0 | 7. 7. 8.0.0 | 7.9.0.0.0 |
| 5.3.0 | 6.8.0.0.0 | 6.9.46.0 | 6.10.8.3.0 | 7.0.0.0.0 | 51200 | 7.2.7.6.0 7.2.11.7.6 7.3.3.0.0 7.3.7.10.6 | 7.3.11.3.0 | 7.5.3.0.0 | 7.0.0.0.0 | 7.7.10.6.0 | 7. 8.9.9.0 7. 9.2.3.0 7. 9.6.8.3 | 7.10.1.6.0 |
| 5.4.0 | 6.9.40.0 | 6.10. 8.0.0 | 7.0.0.0.0 | 7.1.8.0.0 | 7.2.8.0.0 | 7.4.0.0.0 | 7.4.11.9.0 | 7.6.8.0.0 | 7.7.7.8.3 | 7.9.40.0 | 7.0.3.6.0 | 7.11.3.0.0 |
| 3 | 6.0.11.7.6 | 6.11.3.9.0 | 7.0.7.0.0 | 7.2.0.0.0 | 7.3.0.0.0 7.3.4.1.0 7.3.8.2.3 | 7.5.8.3.8 | Parane and a | | 7.8.4.3.9 | 7.10.0.0.0 | 7.11.0.3.3 | 8.0.4.6.0 8.0.9.0.0 8.1.1.6.0 |
| 5.5.0 | 6,10.7.3.0 6,10.11.0.0 6,11.2.10.6 6,11.0.8.3 | 7.0.3.4.6 | 7.1.7.8.3 | 7.3.0.0.0 | 7.4.0.3.0 7.4.4.3.0 7.4.8.4.0 | 7.5.4.6.0 7.5.8.7.6 7.6.8.0.0 7.6.4.0.6 | 7.6.8.9.0 7.7.6.11.3 7.7.5.1.6 7.7.9.3.9 | 7.8.5.3.0 | 7.0.5.3.0 | 7.10.0.6.0 | 8.0.1.9.0 | 8.1.0.0.0 8.1.10.0.0 8.2.3.0.0 |
| 5.6.40 | 7.0.3.3.9 | 7.1.3.0.0 | 7.2.7.0.0 | 7.4.0.0.0 | 7.5.4.0.0 | 7.0.0.0.0 | 7.8.1.6.0 | 7.0.6.0.0 | 7.10.10.0.0 | 8.0.3.0.0 | 8.1.7.0.0 | 8.3.0.0.0 8.3.4.6.0 |
| 5.7.0 | 7.1.1.9.0 | 7.2.2.7.0 | 7.3.7.3.0 | 7.5.4.0.0 | 7.0.4.8.3 | 7.7.9.4.0 | 7.9.2.0.0 | 7.10.0.0.0 | 7.11.11.5.3 8.0.3.9.0 | 8.1.4.1.0 | 8.2.8.0.0 | 8.4.6.0.0 |
| 5.8.0 | 7.2.1.2.3 | 7.3.3.3.6 | 7.4.7.1.8 | 7.6.6.0.0 | 7.7.4.10.0 | 7.8.0.0.0 | 7.10.2.7.8 | 7.11.7.6.0 | 8.0.8.0.0 8.1.0.46 8.1.4.8.3 | 8.2.5.3.0 8.2.5.3.0 8.2.9.7.6 | 8.3.5.8.3 8.3.10.1.6 8.4.2.6.0 | 8.4.10.6.0 8.5.3.0.0 8.5.7.6.0 |
| 443 | 7.2.5.0.0 | 7.4.10.0 | 7.5.0.11.3 | 7.7.0.0.0 | 7.3.5.0.0 | 7.0.0.1.6 | 7.11.3.2.3 | 8.0.4.0.0 8.1.0.0.0 8.1.4.0.0 | 8.2.5.7.0 | 8.3.6.4.6 8.3.0.9.0 | 8.4.7.0.0 | 8.0.0.0.0 8.0.4.0.0 8.0.9.0.0 |
| 5.0.0 | 7.3.8.30 | 7.5.1.6.0 | 7.6.6.9.0 | 7.8.0.0.0 7.8.4.0.0 7.8.8.0.0 | 7.0.5.3.0 | 7.10.10.6.0 7.11.3.7.6 7.11.6.0.0 | 8.0.3.0.0 | 8.1.0.0.0 | 8.3.3.30 | 8.4.7.0.0 8.4.1110.6 | 8.6.0.0.0 | 8.7.6.0.0 |
| 5.10.0 | 7.4.7.8.3 | 7.6.5.0.0 | 7.7.0.0.0 | 7.9.0.0.0 | 7.10.5.5.3 | District of the second second second | 8.1.4.3.0 | | | 8.5.8.7.6 | 8.7.2.0.0 | 8.8.7.6.0 |
| 5.11.0 | 7.5.7.1.6 | 7.7.6.0.0 | 7.8.6.4.6 | 7.10.0.0.0 | 7.11.5.7.6 | 8.0.11.3.0 | 8.1.8.6.0 8.2.0.8.3 8.2.4.0.0 8.2.0.0.0 8.3.1.3.0 | 8.4.2.0.0 | 8.5.8.5.3 | 80.0.0.0 | 8.7.10.11.3 8.8.3.4.6 8.8.7.9.9 | 8.0.0.0.0 8.0.1.0.0 |
| Taylor 3 | 7.00.00.0 | 7.8.0.4.6 | 7.9.6.2.3 | 7.11.0.0.0 | 8.0.5.0.0 | 8.1.11.7.0 | 8.3.5.5.3 8.3.9.7.6 8.4.1.0.0 | 8.4.11.3.0 8.5.3.0.0 | 8.6.5.0.0 8.6.9.4.6 | 8.7.0.0.0 8.7.10.10.0 8.8.3.3.0 | 8.9.0.3.0 8.9.4.8.3 8.9.9.1.0 | 810.0.0.0 810.10.0.0 811.30.0 |
| 6.0.0 | 7.7.6.0.0 | 7.0.0.0.0 | 7.10.6.0.0 | 8.0.0.0.0 8.0.4.0.0 8.0.80.0 8.1.0.0.0 | 8.1.0.0.0 | 8.3.0.0.0 8.3.4.1.6 8.3.8.3.0 8.4.0.4.6 | 8.4.6.0.0 8.4.0.2.3 8.5.3.4.6 | 8.6.0.0.0 8.6.4.3.0 8.6.8.6.0 8.7.0.9.0 | 8.7.0.0.0 8.7.0.3.0 8.8.2.7.6 8.6.6.11.3 | 8.0.0.0.0 8.0.4.4.6 8.0.8.0.0 | 8.10.6.0.0 | 0.0.0.0.0 0.0.4.0.0 |
| 6.1.0 | 7.8.9.3.0 | 7.10.3.6.0 | 7.11.9.9.0 | 8.1.4.0.0 | 8.2.0.3.0 | 8.4.4.6.0 | 8.5.000.0 | | 8.8.11.3.0 8.9.3.0.0 8.9.7.10.0 | 8.9.6.9.0 8.10.5.0.0 | 8.11.11.9.0 | 9.1.1.6.0 |
| 6.2.0 | 7.9.8.8.3 | 7.11.3.1.6 | 8.0.5.7.0 | | 8.3.0.4.0 8.3.0.5.3 8.4.3.6.0 | 8.5.0.0.0 8.5.4.0.6 8.5.0.0.0 | 8.6.7.1.8 | 8.8.2.9.0 | 8.0.7.10.6 | 8.11.0.7.0 | 9.0.8.7.8 | 9.2.7.6.0 |
| 3, | B I manufaction development | 7.11.10.10.6 8.0.2.0.0 8.0.6.7.6 | 8.1.5.5.3 | 8.2.8.0.0 8.3.0.0.0 8.3.40.0 8.3.60.0 | 8.4.0.0.0 8.4.10.7.0 8.5.2.8.3 | 8.0.5.3.0 8.0.5.3.0 8.0.9.4.6 | 8.7.7.8.3 | | 810.8.0.0 811.1.6 811.5.5.3 | 9.0.3.4.6 9.0.7.9.0 9.1.6.1.6 | 0.1.0.1.3 | 9.3.0.0.0 9.3.0.0.0 9.4.1.6.0 |
| 0.3.0 | 7.11.3.0.0 | 8.1.2.4.6 8.1.6.3.0 8.1.0.1.6 | 8.2.5.3.0 8.3.1.1.0 8.3.5.0.9 | 8.4.0.0.0 8.4.4.0.0 8.4.8.0.0 8.5.0.0.0 | 8.5.0.0.0 | 8.7.5.7.6 8.7.5.7.6 8.7.9.9.0 | 8.8.8.3.0 8.9.0.5.3 8.9.4.7.6 8.9.8.9.9 | 8.10.3.0.0 | | 0.1.4.6.0 | 9.3.3.8.3 | 9.46.0.0 9.410.6.0 9.5.3.0.0 |
| 6.4.0 | 8.0.7.0.0 | 8.2.2.0.0 | 8.3.0.0.0 | 8.5.4.0.0 | | 8.8.6.0.0 | 8.10.5.2.3 | 811.8.0.0 | 0.1.3.0.0 | 9.2.10.0.0 | 9.4.0.6.9 9.4.5.0.0 9.4.0.5.3 | 9.6.0.0.0 |
| 6.5.0 | 8.1.0.5.3 | 8.3.5.6.0 | 8.4.8.0.9 | 8.0.00.0 8.0.4.0.0 8.0.8.0.0 | 8.7.7.1.2.3 | 8.9.2.3.0 8.9.6.4.6 8.0.10.6.0 | 811.1.0.0 | 9.0.4.8.0 | 0.1.11.7.6 | 9.3.0.0.0 | 0.5.9.0.8 | 0.6.0.0.0 |
| 3 | 8.2.5.0.6 8.2.0.8.3 | 8.4.1.3.0 | 8.5.8.7.6 | 8.7. 40.0 8.7. 8.0.0 | 8.8.7.30 8.8.7.4.6 8.9.3.5.3 | 8.10.2.7.6 8.10.6.9.0 8.10.10.10.6 | 811.9.11.3 | 9.1.5.30 | 9.3.0.0.9 9.3.4.0.6 9.3.0.2.3 | 9.4.7.10.6 9.5.0.3.0 9.5.4.7.0 | 0.6.3.2.3 0.6.7.7.6 0.7.0.0.0 | 9.7.10.6.0 9.8.3.0.0 9.8.7.6.0 |
| 0.0.0 | 8.3.5.3.0 | 8.4.0.0.0 8.5.0.0.6 8.5.4.0.0 8.5.8.7.6 | 8.6.4.6.0 8.6.8.5.3 8.7.0.4.6 8.7.4.3.0 | 8.8.0.0.0 8.8.4.0.0 8.8.8.0.0 | 8.0.7.6.0 | 8.11.7.1.6 | 9.0.0.6.0 9.1.2.8.3 9.1.0.0.0 9.1.11.0.0 | 9.2.6.0.0 9.2.10.3.0 9.3.2.0.0 | 9.4.1.6.0 9.4.5.0.0 9.4.0.1.0 | 9.5.9.0.0 9.6.1.4.6 9.6.5.9.0 | 0.7.4.6.0 | 0.0.0.0.0 0.0.4.6.0 0.0.0.0.0 |
| 6.7.0 | 84.4.0.0 | 8.0.0.0.0 | | 8.0.40.0 | 8.0.11.0.0 | 9.0 7.6.0 | 9.2.3.30 | 9.3.11.0.0 | 0.5.6.0.0 | 0.7.2.6.0 | 0.8.5.9.0 0.8.10.3.0 0.8.2.8.3 | 0.10.6.0.0 |
| 6.8.0 | 8.5.4.2.3 | 8.7.4.0.0 | 8.9.0.0.0 | 8.10.4.0.0 | 9.0.4.0.0 | 0.1.3.0.0 | | 9.5.4.0.0 | 0.5,11.0.0 0.0.3.4.0 0.0.7.8.3 | 9.8.3.7.0 9.8.8.0.0 | 0.0.11.6.0 | 0.11.3.0.0 |
| 6.0.0 | 8.0.3.7.0 | 8.7.5.0.0 | 8.9.7.10.0 | 8.11.4.0.0 | 0.1.0.1.6 | 0.2.8.3.0 | | 9.5.8.3.0 9.6.6.6.6.0 9.6.4.0.0 | 0.7.0.0.0 0.7.4.3.0 9.7.8.7.0 0.8.0.11.3 | 0.0.4.0.0 | 0.11.0.10.0 0.11.5.3.0 | 0.0.40.0 10.0.0.0.0 10.1.1.6.0 |
| 183 | 8.7.3.0.0 8.7.0.0.6 6.7.10.8.3 | 8.9.3.3.0 8.9.7.1.6 | 8.10.7.8.3 810.7.9.8 8.11.3.6.0 | 9.0.40.0 9.0.8.0.0 9.1.0.0 | 0.2.0.3.0 | 9.3.4.0.0 9.3.8.7.6 9.4.6.0.0 9.4.410.6 | 0.5.0.0.0 0.5.411.3 0.5.0.1.8 | 0.0 0.0 0 0.7.1.3.0 0.7.5.0.0 | 0.8.5.3.0 0.8.0.00 0.0.0.00 | 010.1.6.0 010.5.10.6 010.10.3.0 | 0.0.2.2.3 | 0.1.0.0.0 |
| 6.10.40 | 8.8.2.6.0 8.8.6.3.0 8.8.10.1.6 8.9.111.3 | 8.0.11.0.0 8.10.2.10.0 8.10.0.0.0 | 3.0.3.4.8 | 0.1.40.0 | 0.3.0.6.0 | 0.4.0.0.0 | 0.0.5.0.0 0.0.9.8.3 | 9.8.2.0.0 9.8.6.3.0 9.8.6.3.0 | 0.0.0.6.0 | 0.11.7.0.0 | 0.1.3.6.0 A 0.1.7.11.3 0.2.0.4.0 | 0.3.0.0.0 |
| 6.11.0 | 8.9.1.11.3 | 8.11.2.6.0 8.11.6.4.6 | 9.0.7.3.0 9.0.11.3.0 9.1.3.2.3 | 0.2.8.0.0 | 0.4.0.8.3 | 0.5.p.4.6 0.6.1.6.0 | 9.7.0.0.9 | 9.9.7.0.0 | 0.11.3.0.0 | 0.0.8.1.6 | 0.2.4.0.0 | 0.4.0.0.0 |
| 7.0.0 | 8.0.5.2.3 8.0.0.0.0 | | 0.2.30.0 | A. | The second secon | 0.6.0.0.0 | 9.8.0.0.0 | 9.10.3.8.0 9.10.7.9.0 | 0.0.0.4.6 | 0.1.0.30 | 0.3.6.1.6 h | 0.5.3.0.0 2.5.7.6.0 |
| 33 | 811.6.5.3 | 0.0.0.0.6 | 0.2.0.11.3 0.2.10.10.0 0.3.2.0.0 | 9.4.4.0.0 9.4.3.0.0 9.5.0.0.0 | 0.5.0.0.0 0.6.1.0.0 0.6.5.1.6 0.0.2.3 | 0.7.W.1.6 0.8.3.3.0 0.8.0.4.6 | 0.0.7.2.3 0.0.11.4.0 0.0.3.6.0 | 9.11.4.3.0 9.11.8.8.0 0.0.0.0.0.0 | 10.1.1.3.0 10.1.5.7.6 10.1.0.11.3 | 0.2.10.4.0 | 0.4.3.0.0 M 0.4.7.5.3 M 0.4.11.10.0 M 0.5.4.3.0 M | 0.6.4.6.0 |
| 7.1.0 | 0.0.0.3.0 0.0.4.0.0 0.0.7.0.6 0.0.11.8.3 | 9.1.9.6.0 9.2.1.4.0 9.2.5.3.0 9.2.9.1.6 | 0.3.0.00 0.3.0.8.3 0.4.2.7.0 | 0.5.40.0 | 0.7.1.30 | 0.00.6.0 | 9.10.7.9.0 | 0.0.5.0.0 | 10.2.2.3.0 | 0.3.11.0.0 0.4.3.0.6 0.4.8.30 | 0.5.8.0.0 M 0.6.1.2.3 M 0.6.5.7.6 M 0.6.0.0.0 M | 0.7.6.0.0 |
| 7.2.0 | 0.1.3.6.0 6.1.7.3.6 | 9.1.9.1.0.0 9.3.4.0.0 9.3.4.0.0 9.4.0.7.0 | 9.4.0.0.9 9.5.3.5.3 | 0.0. 4. 0.0 0.0.8.0.0 0.7.0.0.0 0.7.4.0.0 | 0.8.5.6.0 | 0.10.3.0.0 | 0.0.0.0.0 | 0.1.5.0.0 | 0.3.3.2.3 | 0.5.5.0.0 | 0.0.00.00 | 0.0.0.0.0 |
| . 3 | 9.2.2.11.3 | 9.4.0.7.0 | 9.0,2.3.0 | 0.7.4.0.0 0.7.8.0.0 0.8.0.0.0 | 0.9.5.8.3 | 9.11.3.4.6 | 10.0.8.10.0 | 0.2.0.0.0 | 0.4.4.1.6 | 0.6.6.1.6 | 0.7.3.0.0 0.7.0.11.4.0 0.6.3.0.0 | 2.0.0.0.0 |
| 23 | 0,2.0.0.0 0,2.10:0.0 0,3.2,4.0 0,3.0.2.3 | 9.5.4.1.6 | | 0.8.0.0.0 0.8.4.0.0 0.8.6.0.0 0.0.0.0 | | | 10.1 .0.5.3 10.2 1.7.0 10.2 5.0.0 | 0.3.7.3.0 | 10.5.5.0.0 10.5.0.4.0 10.6.1.6.3 | 0.7.2.0.6 A 0.7.7.3.0 A 0.7.11.7.6 A | 0.8.30 | 7.10.10.0.0 |
| 7.4.0 | 0.3.10.0.0 0.4.1.0.0 0.4.5.7.6 0.4.0.5.3 | 9.5.8.0.0 | 0.7.011.3 | 0.0.8.0.0 | 0.11.0.0.0 | 0.1.4.1.6 | 10.2.10.0.0 10.3.2.2.3 10.3.6.4.6 | 0.4.8.0.0 | 0.0.0.0.0 h 0.6 10.3.0 h 0.7.2.7.0 | 0.8.4.0.0 A 0.8.8.4.0 A 0.9.8.5.0 A | 0.10.2.0.0 11 | 1.0.4.0.0 |
| 7.5.0 | | | 0.8.9.0.0 0.9.5.7.0 0.9.5.7.0 0.9.0.0.9 | THE RESERVE TO THE PERSON NAMED IN | | | 10.3.10.8.0 A 10.4.2.0.0 I 10.4.0.11.3 A 10.4.11.1 B 10.5.3.3.0 A | 0.6.1.0.0 | 0.7.11.3.0 | 0.0.9.6.0 N | 0.11.3.3.0 1 0.11.7.0.0 1 1.0.0.2.3 1 1.0.4.7.0 1 1.0.0.0.0 | 1.1.6.0.0 |
| 3 | 9.8.8.83 | 9.7.11.7.6 | 9.9.9.6.9 | 9.11.80.0 | 0.1.0.5.3 | 0.3.4.10.6 | 10.4.11.1.0 k | 0.7.1.9.0 | 10,9.0,2.3 | 0.10.0.30 | 1.0.4.7.0 | 1.2.7.0.0 |

A TABLE OF FEET AND INCHES.
from 7 foot 6 inches by 1 foot 3 inches and 1 quarter to 9 foot 11 inches and 3 quarters by 1 foot 6 inches

| ElParts | EL.Parts | ELParts | ELParts | ELParts | F.I.Parts | ELParts | El Parts | FLParts | FLParis | F.I.Parts | FI.Parts | ELParts |
|---------|---|--|---|---|--|--|---|--|--|---|--|---|
| -60 | 0.0,4.0.0 | 0.8.3.0.0 | 0.10.1.6.0 | 1.4.0 | 1.44 | 10.3.0.0.0 | 1.4 \$ | 1.50 | 1.54 | 1.5 % | 1.5 4 | 1.6.0 |
| 1 | 9.6.4.6.0 9.7.3.1.3 9.7.3.1.3 | 9.8.0.00.0 | 9.10.9.4.0 9.11.1.3.9 | 10.0.4.0.0 10.0.8.0.0 10.1.0.0.0 | 10.2.2.6.7.6 10.2.6.7.6 10.2.0.8.3 | 10.4.5.3.0 | 10.6.3.10.6 | 10.7.10.3.0 | 10.10.1.1.6 10.10.5.5.3 | 10.11.7.4.0 | | 11.3.4.0.0 |
| 7.7.04 | 9.7.7.9.0 9.8.3.4.3 9.8.7.2.3 | 0.0.6.6.0 0.0.0.4.6 0.10.2.3.0 0.10.6.1.6 | 0.11.5.3.0 0.11.0.2.3 10.0.1.1.0 10.0.5.0.0 | 10.1.4.0.0 10.1.8.0.0 10.2.0.0.0 10.2.4.0.0 | 10.320.0 10.30.00 10.310.00.0 10.3211.3 | 10.5.1.6.0 10.5.5.7.6 10.5.9.9.0 10.6.1.10.6 | 10.7.0.3.0 10.7.4.3.3 10.7.8.7.0 10.8.0.0.0 | 10.8.11.0.0 | 10.10.0.0.0 10.11.2.0.0 10.11.0.4.6 10.11.10.8.3 | 11.0.8.0.0 | 11.2.7.3.0 11.2.11.8.3 11.3.4.1.0 11.3.6.0.9 | 11.40.0.0 11.4.0.0.0 11.5.3.0.0 11.5.7.0.0 |
| 7.8.0 | 0.8.11.0.0 0.0.2.0.0 0.0.0.7.6 0.0.0.5.3 | 9.10.10.0.0 9.11.1.10.0 9.11.5.0.0 | 10.0.0.0.0 10.1.0.11.3 10.1.4.10.0 | 10.2.8.0.0 10.3.0.0.0 10.3.4.0.0 | 10.4.7.0.0 | 10.6.0.0.1.6 | 10.8.5.0.0 | 10.10.40.0 | 11.0.3.0.0 | 11.2.2.0.0 | 11.4.1.0.0 | |
| 7.9.9 | 0.10.2.3.0 0.10.0.0.0 0.10.0.0.0 | 10.0.1.6.0 | 10.2.0.0.0 10.2.4.8.3 10.2.8.7.0 | 10.4.0.0.0 10.4.4.0.0 10.4.8.0.0 | 10.511.3.0 | 10.7.10.6.0 | 10.9.9.9.0 | 10.11.0.0.0 | 11.1.8.30 | 11: 3:7: 0:0 11: 3:7: 0:0 11: 4:4:30 | 11.3:0:93 11.0:3:70 11.0:8:00 | 11.7.6.0.0 |
| 7.10.04 | 9.11.1.8.3 | 10.1.1.1.0 | 10.3.0.0.9 10.3.4.6.0 10.3.8.5.3 10.4.8.4.6 | 10.5.0.0.0 10.5.4.0.0 10.5.8.0.0 10.6.0.0.0 | 10.0.11.5.3 | 10.8.10.10.0 | 10.10.10.3.9 10.11.6.8.3 10.11.10.10.0 | 11.0.0.0.0 | 11.2.9.2.3 11.3.1.6.0 11.3.5.0.0 11.3.10.1.6 | 11. 4.8.7.0 11. 5.1.0.0 11. 5.54.0 11. 5.0.0.0 | 11.7.0.6.0 | 11.9.0.0.0 |
| 7.11.04 | 10.0.4.11.3 | 10.2.47.6 | 10.4.4.3.9 | 10.0.4.0.0 | 10.8.3.8.3 | 10.10.3.4.6 | 11.0.3.0.9 | 11.2.2.0.0 | 11.4.2.5.3 | 11. 6.2.1.6 | 11.8.0.30 | 11.10.1.0.0 11.10.0.0.0 11.10.10.0.0 |
| 8.0.9 | 10.1.0.2.3 | 10.3.8.1.6 | 10.5.8.0.0 | 10.7.8.0.0 | 10.10.0.0.0 | 11.0.0.0.0 | 11.1.7.9.9 | 11.3.7.9.0 | 11.5.7.8.3 | 11.7.7.7.0 | 11.10.0.00 | 11.11.3.00 11.11.7.0.0 12.0.0.0,0 12.0.4.0.0 12.0.6.0,0 12.1:1.0.0 |
| 8.1.0 | 10.3.3.3.9.0 | 10.4.11.7.0 | 10.0.11.9.9 | 10.9.0.0.0 10.0.40.0 | 10.11.0.2.3 10.11.4.3.0 | 11.1.4.6.0 | 11.3.8.8.9 | 11.5.5.0.0 | 11.7.011.3 | 11.9.5.6.0 | 11.11.5.0.0 | 12.1.1.0.0 |
| 3 | 10.3.10.00 | 10.5.11.3.0 | 10.7.11.7.8 | 10.10.0.0.0 | 11.0.0.4.6 | 11. 2.0.0.0 | 11.4.1.1.0 | 11.6.5.9.0 | 11.8.0.2.3 | 11.10.2.3.0 | | 12.2.3.0.0 |
| 8.2.0 | 10.4.10.3.0 | 10.0 kajo.0 10.7.2.0.0 10.7.0.7.0 | 10.8.11.5.3 10.9.3.4.0 10.9.7.3.9 | 10.11.0.0.0 10.11.4.0.0 10.11.8.0.0 | 11.1.0.6.0 11.1.4.7.0 11.1.8.8.3 | 11.3.5.3.0 | 11.5.1.8.3 | 11.7.2.3.0 | 11.6.2.0.0 11.0.7.1.0 11.0.11.5.3 | 11.11.7.9.0 | | 12.3.4.0.0 12.3.0.0.0 12.4.1.0.0 |
| 8.3.9. | 10.5.0.0.0 10.6:1:6.9 10.6:5.4.6 10.6:9.2.3 | 10.7.10.6.0 10.8.2.4.6 10.8.6.3.0 10.8.10.1.6 | 10.0.11.3.0 10.10.3.2.3 10.10.7.1.6 10.10.11.0.9 | 11.0.0.0.0 11.0.4.0.0 11.0.8.0.0 11.1.0.0.0 | 11.2.0.0.0 11.2.4.0.0 11.2.8.06 11.3.0.11.3 | 11.4.1.6.0 11.4.5.7.0 11.4.9.9.0 11.5.1.0.0 | 11.6.2.3.0 | 11.8.3.0.0 11.8.7.3.0 11.9.11.0.0 11.9.3.9.0 | 11.10.3.0.0 11.10.8.0.0 11.11.0.4.0 11.11.4.8.3 | 12.0.4.6.0 12.0.8.10.6 12.1.1.3.0 12.1.5.7.6 | THE RESERVE OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN | 12.4.0.0.0 12.4.0.0.0 12.5.3.0.0 12.5.7.0.0 |
| 8.4.0 M | | 10.0.2.0.0 10.0.510.0 10.0.0.0.0 10.10.1.7.0 | 10.11.3.0.0 10.11.6.11.3 10.11.10.10.6 11.0.2.9.9 | 11.1.4.0.0 11.1.8.0.0 11.2.0.0.0 11.2.4.0.0 | 11.3.5.0.0 11.3.9.0.9 11.4.1.1.6 11.4.5.2.3 | 11.5.6.0.0 11.5.10.1.6 11.6.2.3.0 11.6.64.6 | 11.7.7.0.0 | 11.0.8.0.0 11.10.0.3.0 11.10.4.0.0 11.10.8.9.0 | 11.11.0.0.0 12.0.1.3.0 12.0.5.7.0 12.0.9.11.3 | 12.1.10.0.0 12.2.2.4.6 12.2.6.0.0 12.2.11.1.6 | 12.211.0.0 | 12.6.0.0.0 12.6.4.0.0 12.6.0.0.0 12.7.1.6.0 |
| 8.5.0 | 10.8.4.3.0 10.8.8.0.0 10.8.11.10.6 10.0.3.8.3 | 10.10.5.6.0 | 11.0.0.0.0 | 11.2.8.0.0 | | 11. 6.10.6.0 | 11.8.11.9.0 | 11.17.1.0.0 | 12.1.2.3.0 12.1.0.0.9 12.1.10.10.0 | 12.3.3.6.0 12.3.7.10.0 12.4.0.3.0 12.4.4.7.6 | 12.5.4.0.0 | 12.7.6.0.0 12.7.0.0.0 12.8.3.0.0 12.8.7.0.0 |
| 8.0.0 | 10.0.7.0.0 | 10.11.0.0.00 | 11.1.10.6.0 | 11.4.0.0.0 | 11.6.1.6.0 | 11.8.3.0.0 | 11.10.4.6.0 | 12.0.6.0.0 12.0.10.3.0 12.1.2.0.0 | 12.2.7.6.0 12.2.11.0.0 12.3.4.1.0 12.3.8.5.3 | 12.4.0.0.0 12.5.1.4.0 12.5.5.0.0 12.5.5.0.1.6 | 12.6.10.6.0 12.7.2.11.3 12.7.7.40 12.7.11.99 | 12.0.0.0.0 12.0.4.0.0 12.0.0.0.0 |
| 8.7.0 | 10.10.10.0.0 | 11.1.0.0.0 | 11.3.2.3.0 | 11.5.40.0 | 11.7.5.0.0 | 11.0.7.6.0 | 11.11.9.3.0 | 12.1.11.0.0 | 12.4.0.0.0 12.4.5.0.9 12.4.0.40 12.5.1.9.3 | 12.6.2.6.0 12.6.6.10.6 12.6.11.3.0 12.7.3.7.6 | 12 3 4 4 3 | 12.10.6.0.0 12.10.10.0.0 12.11.3.0.0 12.11.7.0.0 |
| 8.8.0 | 11.0.20.0 | 11.2.40.0 | 11.4.0.0.0 | 11.0.8.0.0 | 11.8.0.0.0 | 11.11.0.0.0 | 12.1.2.0.0 | 12.3.4.0.0 12.3.8.3.0 12.4.0.0.0 12.4.4.9.0 | 12.5.0.0.0 12.5.10.3.0 12.0,2.7.0 | 12.7.8.0.0 12.8.0.4.0 12.8.4.0.0 | 12.0.10.0.0 12.10.2,5.3 12.10.0.10.0 | 130.000 |
| 8.9.0 | 11.1.4.5.3 | | | | 11.9.10.2.3.0 11.10.0.3.9. 11.10.10.4.6 11.11.2.5.3 | 12.0.0.4.0 12.0.4.0.0 12.0.8.7.0 12.1.0.0.0 | 12.2.6.0.0 12.2.0.11.3 12.3.3.1.0 | 12.4.0.0.0 12.5.1.3.0 12.5.5.0.0 12.5.0.0 | 12.0.0.11.3 12.0.11.3.0 12.7.3.0.0 12.7.7.10.0 | 12.0.1.6.0 12.0.5.0.6 12.0.5.0.6 | 12.11.3.0.0 12.11.8.2.3 13.0.0.7.0 | 13.1.0.0.0 |
| 8.10.0 | 11.2.4.8.3 11.2.8.0.0 11.3.0.3.0 11.3.4.1.6 | | 11.0.9.0.9 11.7.1.0.0 11.7.5.5.3 11.7.9.4.0 11.8.1.3.9 | | 11.11.2.5.3 | 12.1.430.0 12.1.0.0.0 12.2.1.1.6 12.2.5.3.0 | 12.3.7.3.9 12.3.1.6.0 12.4.3.8.3 12.4.7.10.0 | 12.3.9.9.0 12.6.2.0.0 12.6.6.3.0 12.6.100.0 | 12.8.0.2.3 12.8.4.0.0 12.8.8.9.0 12.0.1.1.6 | 12.0.7.0.0, 12.10.11.4.0 12.11.3.9.0, | 13.0.9.0.0 13.1.1.11.3 13.1.6.4.6 13.1.10.0.9 | 13.3.0.0.0 13.3.4.0.0 13.3.0.0.0 |
| 8.11.9 | 11 2 7 11 2 | 11.5.0.7.6 | 11.8.1.3.0 11.8.5.3.0 11.8.0.2.3 | 11.10.4.0.0 | 12.0.0.0.0 | 12.2.9.4.6 12.3.1.6.0 12.3.5.7.6 12.3.00.0 | 12.5.0.0.9 12.5.43.0 12.5.8.5.3 12.6.0.7.6 | 12.7.2.9.0 12.7.7.0.0 12.7.11.3.0 12.9.3.0.0 | 12.0.5.5.3 12.0.2.0.0 12.10.2.0.0 12.10.6.4.0 | 13.0.0.6.0 13.0.4.0.0 13.0.9.3.0 | 13.2.3.3.0 13.2.7.8.3. 13.3.0.1.0 13.3.4.0.0 | 13.4.0.0.0 |
| 9.0.0 | 11.4.3.0.0 11.4.7.40 11.4.1.23 11.5.3.0.0 11.5.0.7.0 | 11.7.2.1.6 11.7.2.1.6 11.7.0.0.6 11.8.1.0.0 | 11.9.5.0.9 | 12.0.0.0.0 | 12.1.10.11.3 | 12.4.1.10.0 | 12.6.4.9.9 | 12.0.7.0.0 12.0.0.0.0 12.0.4.3.0 12.0.8.6.0 12.10.0.0.0 | 12.10.10.8.3 | 13.1.6.0.0 | 13.3.4.0.0 | 13.57.0.0 13.6.0.0.0 13.6.4.6.0 |
| 9.1.04 | 11.6.6.3.0 | 120000 | | | | | 12.7.9.6.9 | 12.10.0.9.0 | 13.0.3.11.3 | 13.2.7.1.6 13.2.11.6.0 13.3.3.0.6 | 13.5.20.0 | 13.7.1.6.0 |
| 9.2.0 | 11.7.6.6.0 | 11.9.9.1.0 | | | | | 12.8.0.1.0 | 12.11.1.6.0 12.11.5.9.0 12.11.0.0.0 13.0.2.3.0 13.0.6.6.0 13.0.10.9.0 | 13.1.0.2.3 | 13.4.5.0.0 13.4.5.0.0 | 13.5.20.0 13.5.72.3 13.5.11.7.0 13.0.4.0.9 13.0.80.0 13.7.011.3 | 13.7.00.0 13.8.3.00 13.8.7.00 13.0.0.0.0 13.0.4.0.0 |
| 333 | 11.8.1.3.0 | 11.11.0.7.0 | 12.0.8.5.3 | 12.3.4.0.0 | 12.4.11.6.0 12.5.3.6.9 12.5.7.7.6 12.5.11.8.3 | 12.7.31.30 | 12.10.2.10.6 | 13.0.0.0.0 | 13.2.5.3 | 13.5.10.0.0 | 13.7.5.4.0 | 13.0.0.0.0 |
| 3.3. E | 11.0.0.0.0.0 | 11.11.4.0.0 11.11.8.4.6 12.0.0.3.0 12.0.4.1.6 | 12.1.8.3.0 12.2.0.2.3 12.2.4.1.6 12.2.8.0.0 | 12.4.4.0.0 | 12.6.7.9.0 | 12.8.11.7.6 | 12.11.3.5.3 | 13.1.3.0.0 13.1.7.3.0 13.1.11.0.0 13.2.3.0.0 | 13.4.3.4.6 | 13.6.7.3.0 | 13.80.8.3 | 13.11.3.0.0 |
| 9.4.9 | 11.10.4.0.0 11.10.7.0.0 11.10.11.7.6 11.11.3.5.3 | 12.0.8.0.0 12.0.11.10.0 12.1.3.9.0 12.1.7.7.0 | 12.3.0.0.0 12.3.3.11.3 12.3.7.10.0 12.3.11.9.0 | 12.5.4.0.0 12.5.8.0.0 12.6.0.0.0 12.6.4.0.0 | 12.7.8.0.0 12.8.0.0.0 12.8.4.1.0 12.8.8.2.3 | 12.10.0.0.0 12.10.4.1.0 12.10.8.3.0 12.11.0.4.0 | 13.0.4.0.0 13.0.6.2.3 13.1.0.4.0 13.1.4.0.9 | 13.2.8.0.0 13.3.0.30 13.3.4.0.0 13.3.8.0.0 | 13.5.4.3.0 13.5.4.3.0 13.5.8.7.6 13.6.0.11.3 | 13.7.8.4.0 13.8.0.0.0 13.8.5.1.0 | 13.0.8.0.0 13.10.0.5.3 13.10.40.0 13.10.9.3.9 | 14.0.0.0.0 14.0.4.6.0 14.0.0.0 14.1.1.6.0 |
| 9.5.9 | 11.11.7.3.0 11.11.11.0.0 12.0.210.6 12.0.6.8.3 | 12.1.11.6.0 12.2.3.4.6 12.2.7.3.0 | 12.4.3.9.0 12.4.7.8.3 12.4.11.7.0 12.5.3.0.9 | 12.6.8.0.0 12.7.0.0.0 12.7.4.0.0 12.7.8.0.0 | 12.0.0.3.0 12.0.4.3.0 12.0.84.6 12.10.0.5.3 | A. H. L. | 13.1.8.0.0 13.2.0.11.3 13.2.5.1.0 13.2.9.3.9 | 13.4.5.3.0 13.4.5.3.0 13.4.5.0.0 | 13.6.5.3.0 13.7.1.0.6 13.7.6.2.3 | 13.9.10.7.0 | 14.0.30.9 | 14.1.6.0.0 14.1.10.6.0 14.2.3.0.0 14.2.7.0.0 |
| 9.0.0 | 12.0.10.60 12.1.2.30 12.1.0.1.6 12.1.0.1.3 | | AND DESCRIPTION OF THE PARTY OF THE PARTY. | 12.8.0.0.0 12.8.4.0.0 12.8.8.0.0 | 12.10.4.6.0 12.10.8.6.9 12.11.0.7.6 12.11.4.8.3 | 13.0.0.0.0 13.1.1.1.0 13.1.5.3.0 13.1.0.4.0 | 13.3.1.6.0 13.3.5.8.3 13.3.0.0.0 13.4.2.0.0 | 13.5.0.0.0 13.5.0.3.0 13.0.2.0.0 13.0.0.0.0 | 13.7.10.6.0 13.8.2.0.0 13.8.7.1.6 13.8.11.5.3 | 13.10.3.0.0 13.10.7.4.0 13.10.11.9.0 13.11.4.1.0 | 14.1.8.9.9 | 14.3.0.0.0 14.3.4.0.0 14.3.0.0.0 14.4.1.0.0 |
| 9.7.0 | 12.2.1.00 12.2.5.00 12.2.0.40 12.3.1.23 | 12.46.6.0 | 120.11.30 | 12.9.40.0 12.9.8.0.0 12.10.0.0.0 | 12.11.8.9.0 13.0.0.9.0 13.0.40.0 | 13.2.1.6.0 13.2.5.7.6 13.2.0.0.0 13.3.1.0.0 | | 13.6.11.0.0 13.7.3.3.0 13.7.7.6.0 13.7.11.9.0 | 13.0.3.0.0 13.0.0.0.0 13.0.0.4.0 13.0.4.8.3 | 13.11.8.6.0 14.0.0.10.6 14.0.5.3.0 14.0.9.7.6 | 14.2.1.3.0 | 14.4.0.0.0 14.4.10.0.0 14.5.3.0.0 14.5.7.0.0 |
| 9.8.0 | 12.3.5.0.0 12.3.6.0.0 12.3.6.0.0 12.4.0.7.0 12.4.4.5.3 | 12.5.0.0.0 12.0.1.10.0 12.0.5.0.0 | 12.7.11.0.9 12.8.3.0.0 12.8.0.11.3 12.8.10.0 12.9.2.9.9 | 12.10.8.0.0 | 13.1.1.0.0 13.1.50.0 13.1.9.1.0 13.2.1.2.3 | 13.30.0.0 | 13.5.11.0.0 | 13.8.40.0 13.8.8.3.0 13.8.8.0.0 13.0.4.0.0 | 13.10.0.0.0 13.11.1 .3.0 13.11.5.7.0 13.11.0.11.3 | 14.1.2.0.0 14.1.0.4.0 14.1.10.0.0 14.2.3.1.0 | 14.3.7.0.0 14.3.11.5.3 14.4.3.0.6 14.4.8.3.9 | 14.6.0.0.0 14.6.4.6.0 14.6.0.0.0 |
| 9.9.0 | 12.4.4.5.3 12.4.8.3.0 12.5.0.0.0 12.5.3.0.0 12.3.7.8.3 | 12.7.1.6.0 | 12.0.0.0.0 12.0.10.8.3 12.0.2.7.0 | 13.0.0.0.0 13.0.4.0.0 13.0.8.0.0 | 13.2.5.3.0 | 13.40.0.0 | 13.7.3.0.0 13.7.7.11.3 13.8.0.1.0 13.8.4.3.0 | 13.0.0.0.0 13.10:1.3.0 13.10:5.0.0 13.10:9.9.0 | 4.0.2.3.0 14.0.0.0.0 14.0.0.0.0 | 14.2.7.8.0 14.2.51.10.0 14.3.4.3.0 14.3.8.7.0 | 14.5.0.0.0 14.5.5.2.3 14.5.0.7.6 14.6.20.9 | 14.7.6.0.0 14.7.10.6.0 14.8.3.0.0 14.8.7.0.0 |
| 9.10.0 | 12.5.1.6.0 12.6.3.3.0 12.6.611.3 | 12.8.5.0.0 | 12.0.0.0.0 | 13.1.0.0.0 13.1.4.0.0 13.1.8.0.0 13.2.0.0.0 13.2.40.0 | 13.3.5.5.3 13.3.6.0 13.4.5.7.6 13.4.5.7.6 13.4.5.7.6 | | 13.8.8.6.0 13.9.0.8.3 13.9.4.0.0 13.9.9.0.0 | 13.11.20.0 13.11.0.30 13.11.00.0 14.0.20.0 | 14.1.7.6.0 | | | 14.0.0.0.0 14.0.40.0 14.0.40.0 14.0.1.0.0 |
| 9.11.04 | 12.0.611.3 12.7.3.0.0 12.7.3.0.0 12.7.10.4.0 12.8.2.2.3 | 12.9.47.0 12.9.8.6.0 12.03.4.0 12.04.3.0 12.10.5.1.0 | 13.0.3.9 | 13.2.40.0 | 13.49.83 13.5.569 13.5.569 13.5.569 13.5.569 | 13.7.3.4.0 13.7.7.0.8 13.8.3.0.0 13.8.7.0.0 | 13.10.1.3.0 | 14.0.7.0.0 14.0.11.3.0 14.1.3.0.0 14.1.7.9.0 | 4.3.0.0.0 4.3.5.0.9 4.3.9.4.6 | 4.5.0.0.0 4.5.00.0 4.0,3.3.0 | 14.8.0.3.0 14.8.4.8.3 14.8.9.1,0 14.9.1.6.9 | |
| 3 | 12.8.2.2.3 | 12.10.8:1.0 | 13.1.2.0.9 | 3.3.80.0 | 3.6.7.71.3 | 3.3.3.6 H | 1311.1.9.9 | 14.1.7.9.0 | 441.83 | 4.0.7.7.0 | 14.9.1.0.9 | 4.11.7.0.0 |

A TABLE OF FEET AND INCHES

| from | to foot by | foot 3 is | nches and | Q L.C. | OL I | a foot su | nches an | d 3 quar | ters by | foot 6 in | chas. | |
|----------|--|---|--|---|--|--|--|--|---|---|--|--|
| FIParts | DATE STREET, S | CONTRACTOR AND INCOME. | Service Control of the Control of th | FI Parts | FIParts | FI.Parts | FI Parts | FIParts | FI Paris | FI Parts | TI alts | FI Parts |
| 10.0.0 | 1.34 | 1.3 2 | 13.1.0.0.0 | 13.4.0.0.0 | 13.0.0.0.0 | 13.9.0.0.0 | 131.0.0.0 | 140 2301 | 4.4.6.0.0 | 14.7.0.0.0 | 4.0.0.0.0 | 5.0.0.0.0 |
| 李 | 12.9.5.5.3 | 12.11.3.10.6 12.11.7.9.0 12.11.11.7.6 | 13.2.1.10.0 13.2.1.10.0 13.2.5.0.0 | 13.5.0.0.0 | 13.7.0.2.3 | 13.10.0.4.0 | 14.0.2.4.0 14.0.0.0.0.0 | 4.3.0.0.0 | 161120 | 14.7.4.6 14.7.8.0.0 14.8.1.1.0 | 4.10.11.0.0 | 5.1.1.6.0 |
| 10.1.0 | 12.0.0.3.0 12.10-1.0.0 12.10.410.0 12.10.8.8.3 | 13.0.3.0.0 13.0.7.4.0 13.0.11.3.0 13.1.3.1.0 | 13.3.1.8.3 13.3.5.7.0 13.3.5.0.0 | 13.5.40.0 13.5.8.0.0 13.6.0.0.0 13.6.40.0 | 13.7.10.3.0 13.6.2.3.0 13.8.0.4.0 13.8.0.5.3 | 13.11.0.0.0 13.11.0.0.0 13.11.40.0 | 14.1.7.1.0 | 14.3.9.3.0 14.4.1.6.0 14.4.5.0.0 | 4.0.3.0.0 4.0.7.0.0 4.7.0.2.3 | 4.8.0.0.0 14.0.3.3.0 14.0.0.7.0 | 411.8.7.0 | 5.1.10.0.0 5.2.3.0.0 5.2.7.0.0 |
| 10.2.0 | 12.11.0.0.0 | 13.1.7.0.0 | 13 4 1.6.0 | 13.0.8.0.0 13.7.0.0.0 13.7.4.0.0 13.7.8.0.0 | 13.9.2.6.0 13.9.6.6.9 13.0.10.7.6 13.10.2.6.3 | 13.11.9.0.0 4.0.1.1.0 4.0.5.3.0 4.0.9.4.0 | 14.2.3.6.0 14.2.7.8.3 14.2.110.0 14.3.40.0 | 4.5.0.0.0 4.5.0.0.0 4.5.0.0.0 | 17800 | 14.0.11.0.0 14.10.3.4.6 14.10.7.9.0 14.11.0.1.0 | 15.0.011.3 15.1.2.4.0 15.1.0.9.9 | 5.3.4.6.0 5.3.0.0.0 5.4.1.6.0 |
| 10.3.9 | 13.0.3.9.0 | | 13.5.5.3.0 13.5.0.2.3 13.6.1.1.6 13.6.5.0.0 | | | 14.1.1.6.0 14.1.5.7.0 14.1.0.0.0 14.2.1.0.0 | 14.3.8.3.0 14.4.0.5.3 14.4.4.7.0 14.4.8.9.9 | 14.6.3.0.0 14.0.7.3.0 14.6.11.6.0 14.7.3.0.0 | 48.0.0.0 40.2.0.9 49.0.46 49.0.83 | 14.11.4.6.0 14.11.8.10.6 15.0.1.3.0 15.0.5.7.0 | 15. 2.3.8.3 15. 2.3.8.3 15. 3.0.0.0 | 5.4.0.0.0 5.4.0.0.0 5.5.30.0 5.5.7.0.0 |
| 10.4.0 | 13.1.3.2.3 13.1.7.0.0 13.1.10.0.0 13.2.2.7.0 | 13.4.2.0.0 | 13.6.0.0.0 | 13.0.40.0 13.0.60.0 13.0.0.0.0 | 13.11.11.0.0 | 14.2.0.0.0 14.2.10.1.6 14.3.2.3.0 | 4.5.1.0.0 | 14.7.8.0.0 14.8.0.3.0 14.8.4.0.0 | 4.10.3.0.0 4.10.7.3.0 4.10.11.7.0 4.11.3.11.3 | 15.0.10.0.0. 15.1.2.4.0 15.1.0.0.0 15.1.11.1.0 | 15.3.5.0.0 15.3.9.5.3 15.4.1.0.0 15.4.0.3.0 | 5.0.0.0.0 5.0.4.0.0 5.0.0.0.0 5.7.1.0.0 |
| 10.5.0 | 13.2.0.3.0 | 13.5.5.6.0 | 13.8.0.0.0 | 13.10.4.0.0 13.10.8.0.0 13.11.0.0.0 | 14.0.11.2.3 14.1.3.3.0 14.1.7.3.9 14.1.11.4.0 14.2.3.5.3 | 14.3.10.6.0 14.4.2.7.6 14.4.0.0.0 | 140.5.0.0 140.0.11.3 14.7.2.1.0 | 14.9.1.0.0 14.9.5.3.0 14.0.0.0.0 | 411.8.3.0 5.0.0.0.0 5.0.4.0.0 | 15.2.3.0.0 15.2.7.0.0 15.3.0.3.0 15.3.4.7.0 | 15. 5. 3. 2. 3 | 5.7.0.0.0 5.7.0.0.0 5.8.3.0.0 5.8.7.0.0 |
| 10.0.0 | 13.4.1.0.0 13.4.5.3.0 13.4.5.3.0 | 13.6.5.1.6 13.6.0.0.0 13.7.0.10.6 13.7.4.0.0 13.7.8.7.6 | 13.0.46.0 13.0.46.0 13.0.65.3 13.6.6.4.6 | 13.11.8.0.0 14.0.0.0.0 14.0.4.0.0 14.0.8.0.0 | 4.2.7.6.0 4.2.11.6.9 14.3.3.7.6 | 14.5.3.0.0 14.5.7.1.0 14.5.7.1.3.0 | 14.7.10.6.0 14.8.3.8.3 14.8.0.0.0 | 14.10.6.0.0 14.10.10.3.0 14.11.2.0.0 | 15.1.1.6.0 | 15.3.0.0.0 15.41.4.0 15.4.5.0.0 15.410.1.0 | 15.0, 40.0 15.0,811.3 15.7.1.4.0 15.7.5.0.0 | 15.0.0.0.0 15.0.4.0.0 15.0.0.0.0 |
| 10.7.0 | 13.5.0.11.3 13.5.4.0.0 13.5.8.0.0 13.0.4.0 | 13.7.8.7.0 13.8.0.0.0 13.8.4.4.0 | 13.10.8.3.0 | 14.1.0.0.0 14.1.4.0.0 14.1.8.0.0 14.2.0.0.0 | 14.3.7.8.3 14.3.11.0.0 14.4.3.0.0 14.4.7.10.0 | 14.0.3.4.0 14.0.11.7.0 14.0.11.7.0 | 14.9.3.3.0 14.9.7.5.3 14.9.11.7.0 | 14.11.10.0 15.0.3.3.0 15.0.7.0.0 15.0.11.0.0 | 15.2.0.0.0 15.2.11.0.0 15.3.3.4.0 | 15.5.2.6.0 15.5.6.0.0 15.5.11.3.0 15.6.3.7.6 | 15.7.10.3.0 15.8.2.8.3 15.8.7.1.0 | 15.10.0.0.0 15.10.10.0.0 15.11.3.0.0 |
| 10.8.0 | 13.0.4.2.3 | 13.0.40:0 | 13.11.8.0.0 | 14.2.4.0.0 14.2.8.0.0 14.3.0.0.0 | 14.4.11.11.3 14.5.4.0.0 14.5.8.0.0 14.6.0.1.6 | 14.8.0.0.0 14.8.4.1.0 14.8.8.3.0 | 14.10.3.9.9 14.10.8.0.0 14.11.0.2.3 14.11.4.4.0 | 15.1.40.0 15.1.83.0 15.2.00.0 15.2.49.0 | 15.4.0.0.0 15.4.4.3.0 15.4.8.7.0 | 15.0.8.0.0 15.7.0.+0 15.7.4.0.0 | 15.0.40.0 15.0.8.5.3 15.0.0.0.0 | 10.0.0.0,0 10.0.4.0.0 10.0.0.0.0 |
| 10.0.0 | 13.7.7.5.3 13.7.7.5.3 13.7.1.3.0 13.8.3.0.0 | 1310.7.6.0 | 14.1.3.0.0 | 14.4.0.0.0 | 4.6.4.2.3 14.6.8.3.0 14.7.0.3.0 | 14.0.4.6.0. | 15.0.0.0.0 15.0.4.11.3 15.0.0.1.0 | 15.2.0.0 15.3.1.3.0 15.3.5.0.0 15.3.9.0.0 | 15.5.5.3.0 | 15.8.1.0.0 15.8.5.0.0 15.8.0.3.0 15.8.0.3.0 | 15.11.2.2.3 | 16.1.0.0.0 |
| 10.10.0 | 13.0.2.0.0 13.0.2.0.0 13.0.0.3.0 13.0.0.1.0 | 13.11.7.1.0 | | STREET, SHIPPING SHIPPING SHIPPING | 14.7.8.5.3 14.8.0.6.0 14.8.4.6.9 14.8.8.7.6 14.9.8.8.3 | | THE RESERVE AND PARTY AND PARTY. | | 15.0.0.2.3 15.0.0.6.0 15.7.2.9.9 15.7.7.1.6 | 15.0.7.0.0 | The same of the sa | 16.3.0.0.0 |
| 10.11.0 | 13.10.5.0.0 | 14.1.2.0.0 | | 146000 | 40400 | 15.0.1.6.0 | 15.2.10.3.0 | 15.5.2.0.0 15.5.7.0.0 15.5.11.3.0 | 15.7.11.5.3 15.8.3.0.0 15.8.8.0.0 15.0.0.4.0 | 15.11.0.0.0 | 10.1.4.9.9 10.2.1.8.3 16.2.6.1.6 16.2.10.6.9 | 10.40.0.0 |
| 11.0.0 | 1311.0.0.0 | 14.2.2.1.0 | 14.5.3.0.0 14.5.611.3 14.5.000 14.5.000 14.6.2.9.9 | 14.8.0.0.0 14.8.4.0.0 | 14.0.0.0.0 14.10.0.0.0 14.10.4.11.3 14.10.0.0.0.0 14.11.1.0.0 14.11.5.1.0 | 15.1.60.0 | 15.4.3.0.0 | 15.7.0.0.0 15.7.0.0.0 15.7.4.3.0 15.7.8.6.0 15.8.0.9.0 | 15.9.4.8.3 15.0.0.0.0 15.10.1.3.0 15.10.5.7.0 | Miles Committee of the | 10.3.3.0.0 10.3.7.5.3 16.3.11.0.6 10.4.4.3.9 | 10.0.0.0.0 10.0.4.0.0 10.0.9.0.0 |
| 11.1.0 | 14.0.4.7.0 | 143060 | 146.00.0 | 14.0.4.0.0 | 15.0.1.3.0 | 15.2.10.6.0 | 15.5.7.0.0 | 15.8.5.0.0 | 15.10.9.11.3 15.11.0.0.9 15.11.10.10.0 15.11.10.10.0 10.0.3.2.3 | 10.1.11.0.0 | 10.4.4.3.9 10.5.1.2.3 10.5.5.7.0 | 10.7.1.0.0 16.7.10.0.0 16.3.3.0.0 |
| 11. 2.0 | 14.1.7.10.0 | | 14.0.10.8.3 14.7.0.6.9 | | 15.1.5.6.0 | 15.4.3.0.0 | 15.7.0.6.0 | 15.0.5.0.0 | 16.0.3.2.3 | | 10.3.10.0.9 | 10.8.7.0.0 10.9.0.0.0 10.9.4.0.0 |
| * 33 | 14.2.7.3.6 | 14.5.4.0.0 | 14.7.10.6.0 14.8.2.5.3 14.8.0.4.0 14.8.10.3.9 | 14.11.0.0.0 | 15.2.1.7.6 | 15.5.7.6.0 | 15.8.5.3.0 | | 6.2.0.9.0 | 16.3.5.0.0 16.3.9.4.0 16.4.0.1.0 16.4.0.0.0 | 0.0.2.0.0 0.0.0.11.3 10.0.11.4.0 10.7.3.9.0 10.7.8.3.0 | 16.10.6.0.0 |
| 11.3.0 | 14.3.10.6.0 | 14.0.8.4.0 14.7.0.3.0 14.7.4.1.0 | | 15.0.4.0.6 | 15.3.1.0.0 | | THE RESERVE AND ADDRESS OF THE PARTY OF THE | 15.11.7.3.0 | 6.2.9.4.6 16.3.1.8.3 16.3.0.0.0 | 16, 5, 2,10.6 16, 5, 7, 3, 0, 16, 5, 11, 7, 6 | 16.8.5.1.6 | 16.11.3.0.0 16.11.7.0.0 |
| 11.4.0 | 14.4.10.0.0 14.5.1.0.0 14.5.5.7.0 14.5.0.5 | 7 14.7.11.0.0 7 14.8.3.9.0 3 14.8.7.7.0 | 6 14.11.5.9.6 | 15.1.8.0.0 | | 15.7.4.1.0 | 15.10.2,2.3 16.10.0.4.0 15.10.10.0.0 | 16.1.0.3.0 | 10,3.10.3.9 10,4.2.7.6 10,4.0.11.3 16,4.11.3.0 | 10:311.7.0 10:0.40.0 10:0.0.40 10:7.0.9.0 10:7.5:1.0 | 16.0.0.5.3 16.0.10.10.6 16.10.3.3.9 | 17.0.0.0.0 |
| 11.5.0 | 14.6.1.3.0 14.6.5.0.0 14.6.8.0.0 14.7.0.8 | 14.8.11.6.0 14.0.9.4.0 14.0.7.3.0 14.0.11.1.0 | 14.11.0.0.0 15.0.1.8.3 15.0.5.7 15.0.9.0 | 15.2.8.0.0.0 15.3.0.0.0 15.3.4.0.0 15.3.8.0.0 | 15.5.0.3.0 15.5.10.3.9 15.6.2.4.0 15.6.6.5.3 | 15.8.46.0 15.8.8.7.0 15.00.00 15.0.40.0 | 15.11.631.3 | 16.2.5.3.0 16.2.0.0.0 16.3.1.9.0 | 10,5.3.6.0 10,5.7.10.0 10.6.0.2.3 10.6.4.6.0 | 16.8.10.0 | 10,11.0,2.3 | 7.1.10.0.0 17.2.3.0.0 17.2.7.6.0 |
| 11.0.0 | 14.7.4.6.0 14.7.8.3.9 14.8.0.1.1 14.8.3.11. | 14.10.3.0.0 14.10.6.10.0 14.10.10.9.0 3 14.11.2.7.0 | 15.1.1.6.0 15.1.5.5.5 15.1.0.4.6 15.2.1.3.6 | 15.4.4.0.0 | 15.7. 2.6.0 | 15.0.0.0.0 15.10.1.1.0 15.10.5.3.0 15.10.9.4.0 | 10.0.7.0.0 10.0.11.8.3 10.1.3.10.0 10.1.8.0.9 | 10.3.10.3.0 10.4.2.0.0 16.4.6.9.0 | 10.0.8.9.9 10.7.1.1.0 10.7.5.5.3 | 10.0.7.4.0 | 17.0.5.11.3 | 7.3.4.0.0 17.3.0.0.0 17.4.1.0.0 |
| 11.7.0 | 14.8.7.9.0 14.8.11.0.0 14.0.34.0 14.0.7.2. | 0 14.11.0.6.0 0 14.11.10.4.0 15.0.2.3.0 3 15.0.0.1 | 15.2.5.3.0 15.2.0.2.3 0 15.3.1,1.0 0 15.3.5.0.6 | 15.5.4.0.0 | 15.8.0.9.0 15.8.0.9.0 15.8.0.0.0 | 15.11.1.6.0 15.11.5.7.0 15.11.0.0.0 16.0:1.10.0 | 10.2.0.3.0 10.2.4.5.3 10.2.6.7.0 10.3.0.0.0 | 10.5.3.3.0 | 10.7.9.9.0 10,8.3.0.0 10,8.6.4.0 10.8.0.8.3 | | | 7,400.0 |
| 11.8.0 | 14.0.11.0.0 | 0 15.0.10.0. | 0 15.3.0.0. | 15.6.8.0.0 15.7.0.0.0 15.7.4.0.0 15.7.8.0.0 | 0 150.7.0.0 0 150.11.0.9 0 150.7.2.3 | 10.0.6.0.0 10.0.0.1.0 10.1.2.3.0 10.1.6.4.0 | 16.3.5.0.0 16.3.9.2.3 16.4.1.4.6 16.4.5.6.9 | 10.6.40.0 10.6.8.3.0 10.7.0.6.0 10.7.49.0 | 0.3.0.0 | 7.0.2.0.0 | 17.4.2.3.9 | 7.6.4.6.0 |
| 11.9.0 | 14.11.2,3. | 0 15.2.1.0.1 | 0 15.5.0.0.0 0 15.5.4.8 0 15.5.8.7 0 15.0.0.0 | 15.8.0.0. | 2 15.10.11.3.0 | 16.1.10.6.0 16.2.2.7.0 16.2.6.0.0 16.2.6.0 | 10.5.7.71.3 | 10.7.0.0.0 10.8.1.3.0 10.8.5.0.0 10.8.9.0.0 | 10,10.8.3.0 10,11.0.6.9 10,11.4.10.0 10,11.9.2.3 | 7.1.7.0.0 | 7.3.3.0.0 | 7.7.10.6.0 17.8.3.0.0 17.8.7.0.0 |
| 11.10.0 | 15.0.5.6. | 0 15.3.5.0. 0 15.3.8.10. 0 15.4.0.0. 3 15.44.7. | 0 15.6.4.6. | 15.0.40. 15.0.8.0. 15.10.0.0. | 0 10.0.3.6.0 0 10.0.7.6.6 0 10.0.11.7.0 0 10.11.3.8.3 | 10.3.3.0.0 | 0 10.6.2.6.0 10.6.6.6.3.3 10.6.10.10.0 10.7.3.0.0 | 16.9.0.3.0 16.9.0.3.0 16.10.2.9.0 | 17.0.1.6.0 17.0.5.9.6 17.0.10.1.0 17.1.2.5.3 | 7.3.1.0.0 | 17.6,0.0.0 17.6,411.3 17.6,0.4.6 17.7.1.0.0 | 17.0.0.0.0 17.0.4.0.0 17.0.0.0.0 |
| 11.11.0 | | | 0 15.7.8.3. 0 15.8.0.2. 0 15.8.4.1 | 0 15.10.8.0. 15.11.0.0. 15.11.4.0. | 0 16.1.7.9.0 0 16.1.11.9.9 0 16.2.3.10.0 0 16.2.7.11.3 | Bank | 10.7.7.3.0 10.7.7.3.3 10.8.3.7.0 10.8.7.0.9 | 16.10.7.0.0 | 17.1.6.9.6 17.1.11.0.6 17.2.3.4.6 17.2.7.8.3 | 7.4.0.0.0 | | 7,100.00 7,11,30,0 17,11,7.0.0 |
| 12.0.0 | 15.30.0. 15.3.3.0. 15.3.7.7. | 0 15.0.0.0. | | 0 16.0.00 | 0 10 3.0.0.0 | 16.6.00.0 | 10.0.0.0.0 | 170.00.0 | 17. 3.0.0.0 | 7.0.4.4.6 | 7.0.0.0.0 7.0.45.3 17.0.45.3 17.0.4.3.9 | 19.00.00 19.00.00 19.00.00 19.00 |
| 12.1.9 | 15.4.3.3. | 0 15.7.3.6. | 0 15.10.3.0. | | 0 16.4.4.3.6 | 16.7.46. | | | 17.49.3.0 | | 17.0.5.0.0 | 18.1.0.0.0 18.2.3.0.0 18.2.7.0.0 |
| 12. 2. 0 | 15.5.2.8. 15.5.6.6. 15.5.10.3. 15.6.3.11 | 0 15.8.7.0. | 0 15.11.7.0. | 0 10.2.8.0. | | | | 17.20.0.0 | 17.5.10.0.0 | 0 17.811.0.0 | 17.11.11.0.0 18.0.311.3 18.0.3.4.0 18.0.8.4.0 | 18.3.0.00 18.3.400 18.3.0.00 |
| 12.3.9 | 15.6.0.0. | - | | | | | 0 17.1.2.3.6 | | 17.7.3.0 | 0 17.10.40.0 | 18.1.5.3.0 18.1.0.8.3 18.2.2.1.8 18.2.0.0.9 | 18.40.00 18.40.00 18.3.3.00 |
| 12.4.0 | 15.7.0.2 15.8.1.0 15.8.4.0 15.8.8.7 15.9.0.5 | 0 15.11.2.0 | 0 10.2.3.0. | 0 10 5. 40. | 0 10.8.5.0.0 0 10.8.9.0.3 0 10.9.1.1.3 0 10.9.5.2. | | The same of the sa | | 17.8.9.0. | 0 17.11.10.0.0 | | 18.0.0.00 18.0.0.00 18.0.0.00 18.7.1.00 |
| 12.5.0 | | | 0 10.3.2.9. | 0 10.6.4.0. 0 10.6.6.0. 3 16.7.0.0. 0 16.7.40. 0 16.7.40. | | | 0 17 311.0.1 | | | 0 18.1.30.0 0 18.1.20.0 0 18.2.5.3.0 | 13.4.49.6 | 12.7.000.0 |
| | 15.10.3.8. | 3 10.1.5.1 | .0 10.4.6.0. | 9 10.7.8.0. | 0 10.10.9.5. | 3 17.1.10.10. | | | ARE, APRICO DE SERVIZIONES ANTICADOS | S CONTACTORIL | | |

| | | | | 10.00 | | |
|------|-------------------|------|------|----------|--|------|
| dant | - | IDIT | AFT | EET A | ATT | |
| | A | AKIF | CH F | H. H. A. | | TIN. |
| | BY OF CARRIES AND | | | | HARDON STREET, | |

to 3 foot it inches and 3 quarters by 2 foot. 2.00 2.10 2.10 2.10 4455 6689 99,00 3333 3.0007 3333 3333 4.1 3333 33333 0077 4444 4.1224.3 4444 3.11 3.11 4444 3.10.10.11 3.00 66607 3333 3333 33333 4.3 4444 4.4 0077 4444 4444 3.11 2223 8000 70000 4.6 4.5667 4.5550 2.5.0 4444 4444 4444 4.2223 4455 4444 3.11 4.0 4.0 4.0 3773 0000 4444 4.8899 4444 4.77.88 5000 4444 4.4 4.5 4.5 4.6 0778 4.3 4444 4.2233 4444 4.1 4444 4444 1223 1001 4.00 80000 4.07 4444 4.66 4444 4444 4.4 4444 4444 4.1 4444 4.014.9 3.1000 4.1.6 4.10 4.11 4444 4.00 4444 4.6 7000 4.5 4.4453 4444 4444 5.001 4.10 4444 4.8000 4.7788 4.5500 40007 4444 4.4.5.5.4.5 5.3444 5007 5.2233 4.11 4555 4.00 4.1100 1122 4.7.888 4.7774 4.500 7000 5.0 1223 4.00 4.0 4.0 4.7 4.7 4.7 100 4.00 2334 1000 4.00.00 7,880 0000 5.5500 5555 4455 5555 4.11 5.0 5.0 5.1 5.6778 6677

A TABLE OF FEET AND INCHES

from 4 foot by 1 foot 6 inches and 1 quarter to 6 foot 5 inches and 3 quarters by 2 foot.

| | F.I.Parts | F.I. | FI | F.I | FI | F.I | FI | EI | FI | FI | F.I | F.I | FI | FI | FI | FI | FI | FI | F.I. | FI | FI | FI | F.I. | F.I. | F.I. |
|--|--|--------|---------------------|----------------|---|--------------------|----------------------|-------------|------------|--------|-----------------|----------------------|----------------------|------------------------------|--|--------------|--|-------------------|-------------------------------------|------------------------|----------------------|--|--|---|--|
| | 4.0.0 | 6.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.0 | 8.3 | 0.8 | 0.0 | 0.10 | 8:11 | 7.0 | 1.04 | 3.3 | 7.3 | 7:10 | 3.5 | 3:8 | 3:3 | 7:8 3:8 | 3:0 | 7.10 | 7:11 | 8.0 |
| | 34 | 6.3 | 0:3 | 0.4 | 0.0 | 0.0 | 0.7 | 0.8 | 0.0 | 0.10 | 7.0 | 7.0 | 3:1 | 7.3 | 7.3 | 7.5 | 7.3 | 7.8 | 7.7 | 7.8 | 7.10 | 7.10 | 7.11 | 8.0 | 8.1 |
| | The state of the s | 0.3 | 0.4 | 0000 | 0.0 | 0.7 | 0.3 | 0.90 | 0.10 | 7.0 | 7.1 | 7.2 | 7.3 | 7.3 | 7.5 | 7.0 | 7.7 | 3.8 | 7.00 | 7.10 | 7.0 | 8.0 | 8.1 | 89.2 | 8993 |
| Second | 4.2.0 | 00.5 | 0.5500 | 00007 | 00.00 | 0000 | 0.00 | 0.00 | 3.00 | 7.0 | 3.33 | 777 | 77.5 | 33.3 | 7.7 | 7.8 | 777 | 7.00 | 7.11 | 8.0 | 00000 | 0888 | 8888 8888 8888 8888 8888 8888 8888 8888 8888 | COCOCOCO COCOCOCOCO COCOCOCOCOCOCO CO | G0000 |
| Second | 4.3.0 | 0.00 | 0.7 | 0000 | 0.00 | 6.10 | 6.11 2.03 2.03 | 3.00 | 3.3 | 7777 | 7.3 | 7.3 | 7.5 | 7.07 | 333 | 7.8 | 7.00 | 7:11 | 888 | 90000 1,02 | SCHOOL STATE | STORES A ACTION | 84455 | 0.0000 | 8888 |
| | 4.4.9 | 0.7 | 0000 | 6.00 | 0.10 | 3.9 | 7.0 | 777 | 7.9 | 4 4 | 7.5 | 70 | 7:3 | | | 7.10 | 79.00 | 8000 | 80000 1223 | 8. 33. 4 4. 6. 6. 4 | 00000 | BOOK S | 9007 | 100000 100.73 | SCORCE SC |
| | 4.5.04 | 0.0 | 0.0 | 0.10 | 3:0 | 7:12 | 7.23 | 7.3 | - | - | 3:3 | 2.8 | | | 3.11 | 8.0 | Same of the same o | Sagara Suivini | Samo | 00000 | 8007 | 8000 | andri Solate | 00000 | 8:40 |
| | 4.0.0 | 0.10 | 6.11 7.00 7.0 | 7.0 | 7.13 | 7.3 | 7.4 | 7.5 | - | | | - | - " | 0.0 | _ | | | 0.0000 | o o o o | 8000 | O GOOD O | 0.0000 | 0.90000 | 88900 | 0000 |
| | 4.7.0 | 2:0 | 7.0 | 7.2 | 7.3 | 7.4 | 7.5 | 7.0 | 7.7 2.8 | 7.8 | - | Y | 8:0 | - | 8.3 8.3 8.3 | 8.3 8.445 | 8:530 | 8.00 | 8.7 7.000 7.000 | 8.80 | 8.00 | 8.11 | 0.00 | 9.0 | 0000 |
| | 4.8.0 | 7.1 | 7.2 | 7.3 | 7.4 | 7.3 | 7.7 | 7.8 | 7.9 | 7.10 | 3.11 | 0 1 | | | 8.4 | 8:3 | 8.0 | 8.7 | 8.9 | 8.10 | 8.11 | 9.0 | 9.1 | 9.2 | 0.4 |
| Column C | 4.9.0 | 7.3 | 7.3 | 7:3 | 7:3 | グラ | 7.8 | 7.00 | 7:11 | 8.0 | 8:1 | 88.3 | 8 4 | | - | | | | 8.10 | | | 9.2 | 9.3 | 9.5 | 9.5 |
| | 4.10.0 | 7.4 | 7.5 | 7.8 | 3:5 2.8 | 7.3 | 7:10 | 7:11 | 01 | | | 89.44 | 8.3 | 2 - | 4.4 | | | 8:11 | 9.0 | | MATERIAL STATES | 9:34 9:45 | 9.0 | 9:0 | 9:3 |
| State Stat | 4 | 7.5 | 7.8 7.7 Z.Z | 7.8 | 7.0 | 7.10 | 3.11 | 8.10 | | | - | 8.0 | 8.7 | 8.8 | 8.0 | h-drameter. | | 9.10 | 00.3 | 9.3 | 0.5 | 9.0 | 9.7 | 9.8 9.9 | 9.10 |
| Column C | 5.0.0 | 7.7 | 7.8 7.8 | 7.10 | 7:19 | 8.0 | 8.4 | 8:3 | 8:3 | 8.5 | 8.0 | 8.7 | 8.9 | 8.10 | 8.11 | 9.0 | 0.2 | 0.3 | 0.4 | 9.0 | 9.7 | 9.8 9.8 | 000 | 9.11 | 9.11 |
| Column C | 1 4 | 7.8 | 7.00 | 7:10 | 8.00 | - | 888 A | 34 4 9 4 | 8.5 | - | - | Act (Registration to | | | | 0.2 | 0.4 | 0.5 | 0.0 | 0.8 | 9.8 | 9.00 | 9.11 | 10.0 | 10.1 |
| Column C | 7 | 7.10 | 7.10 | 8.00 | 800 | | 0000 444 | 550 | 8007 | 888 | 8000 | 8.10 | 8000 | 999.1 | 0003 | 0000 | 0.55 | 000 | 0000 | 000 | 9.00 | 0.0 | 10.0 | | |
| Company Comp | 5.2.0 | 7.11 | 0001 | 00000 | Caracas Caracas | 4445 | 3000 | 0077 | Sapara, | 0000 | 0000 | | | 0000 XXXXX | 0000 | 0000 | 0000 | 0000 | 0000 | 0.00 | 0.00 | 0.1 | 10.2 10.2 10.3 | 10.33 10.44 | 0.4 |
| Column | 5.3.0 | 9.001 | 1222 | 99999 45.60 | BBBB | 8.3 | 8888 | 80000 | 0000 | 8.11.0 | 00001 | 0000 | 0000 4 WWW | 0000 | 0000 | 00000 | 7000 | 00000 | 9990 | 0.00 | 10.1 10.2 10.2 | 0.33 0.33 0.00 0.00 0.00 0.00 0.00 0.00 | 10.34 | 10.23 10.00 | 0.0 |
| Column | 1/2 | Same. | 4.000 | BBBB | 5007 | 277.0 | 90000 | 8.0001 | 8000 | 0000 | 0000 | 0000 | 0000 | 2000 | 77.000 0,000,0 | 00000 | 0,000 | 9.11 | 0011 | 00000 | 3344 | 0000 | NO.50 NO.7 | 10.77 10.00 | 0.0000 |
| Column | 5.5.0 | 9.334 | 45,55 | 8888 | 77,88 | 0,0,00 | 8.10 | 8.1100 | 00000 | 0000 | 00000 4 4 CE | 0000 | 00007 | 00000 00000 00000 | 0000 | 0.10 | 1001 | 10.1 | 8000 8000 | 0.3445 | 00000 | 00077 | 00.00 00.00 00.00 00.00 | 0.00 | 0.10 |
| The control of the | 5.6.9 | 3.5 | 3:0 | 7,000 | 8:8 | 8:18 | 8000 | 00000 | 0000 | 9.3 | 8.5 | 8.9 | 8:3 | 00,000 | 0.10 | 0.0 | D. 1 D. 2 D. 2 | 10.2 | NO. 4 NO. 5 NO. 5 | 5000 | 00.7 00.7 0.8 | 00000 | 0.0 | 10.11 | 11.0 |
| 5.8 - Q | | 3.0 | 3:8 | 8.0 | 8.10 | 8.16 | 9:1 | 9:3 | 0.4 | 9.5 | 9.0 | | 9.90 | 8:11 | 10.0 | | | | 10.0 | 10.7 | 2.8 | 0.0 | 0.11 | 11.1 | 11:33 |
| 9 9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 1 2 12 | 3.7. 6 | 3.0 | 8.11 | 9.0 | 0.1 | 0.2 | 0.4 | 0.50 | 9.7 | 0.8 | 0.10 | 0.11 | 10.0 | 10.2 | 0.3 | 10.5 | 10.0 | 0.7 | 0.00 | 10.10 | 1.0 | 11.2 | 11:33 | 11.4 |
| ### ### ### ### ### ### ### ### ### ## | | 000 | 10 | 0.0 | 9:12 | 9.3 | 0.4 | 0.0 | 8:3 | 8:8 | 0.10 | 0.11 | 10:1 | 10.2 | 10.4 | 0.5 | 10.0 10.7 10.7 | 0.000 | 0.0 | 0.11 | 11.0 | 1.30 | 11.3 | 1.5 | 1.0 |
| | 9.10.0 | 10 4 | 3.0 | 0.1 | 9.3 | 0.4 | 0.0 | 0.7 | 0.0 | 0.10 | 0.0 | 10.1 | 0000 | 10.4 10.4 | NO. 50 | 0.7 0.8 | 0.800 | 0.10 | 0.11 | 11.1 | //. a | 1.4 | 1.30 | 1.7 | 1.8 |
| 6.1. Q 0.3 0.5 0.6 0.8 0.0 0.1 0.1 0.2 0.2 0.3 0.5 0.6 0.8 0.0 0.1 11.0 11.2 11.3 11.5 11.6 11.8 11.0 11.1 12.0 12.2 12.3 12.3 12.3 12.3 12.3 12.3 12.3 | 5.11.0 | 0.0 9 | 122 | 0.3 | 0.4 | 0.0 | 9.7 9.7 9.8 | 0.00 | 9.10 | 0.00 | 0.12 | 0.3 | 0.4 | 10.5 10.6 10.0 10.7 | 0.7 0.8 0.8 | 0.0 | 0.10 | 11.0 | 11.2 | 1.33 | 11.5 | 1.0 | 1.7 | 1.000 | 1.10 |
| 6.1. Q | 0.0.0 | 123 | .3 : | 0.4 | 0.0 | 9.7 9.7 90.8 | 0.0 | 0.10 | 0.0 | 0.1 | 0.3 | 0.4 | 0.0 | 10.7 | 0.9 | 0.10 | 11.0 | 11.1 | 11.3 | 1.4 | 1.0 | 1.7 | 1.0 | 1.10 | 2.0 |
| | 6.1.0 | 3 5 | | | 9.7 9.8 9.8 | 0.9 | | | | 0.3 | 0.4 | 0.0 | 0.7 | 10.00 | D.10 1 | 0.11 | | 1.3 | 11.4 | | | | 11.11 | | |
| | 0.2.0 | 500 | 00 | 0.7 | 0.9 | 0.10 | 0.0 | 0.1 | 0.3 | 0.4 | 0.0 | 0.8 | 0.0 | | | 1,2 | PERSONAL IN | 11 6 | | | | CONTRACTOR OF | | SECURIOR AND ADDRESS OF THE PERSON NAMED IN | 2.3 |
| 0.4.0 9.8 9.9 9.1 10.0 10.2 10.3 10.5 10.2 10.8 10.10 11.1 11.3 11.5 11.5 11.5 11.5 11.5 11.5 | | | 7 3 | 0.0 | 0.10 | | | | | 0.0 | 0.8 | | | | | | 11 6 | 12 7 | | | | | | | 2.5 |
| THE PARTY OF THE P | 0.4.0 9 | -A | | 0.10 | | | | 0.5 | 0.0 0.0 | 0.8 | 0.0 | 0.11 | | | 11.4 | 110 | 1191 | 10 | 11.10 | | | 2.3 | | | |
| \$ 5.00 0.0 0.1 0.3 0.5 0.0 0.8 0.0 0.1 11.0 11.3 11.3 11.3 11.3 11.3 1 | 0.5.0 _k 0 | 9 0 | | - | CONTRACTOR OF THE PARTY OF THE | 0.4 | 0.5 | 0.7 | 0.8 | | | | PERSONAL PROPERTY OF | 11.4 | SEASON SE | 1.3 | COMPAN-ALONE DA | APPENDENCE TO SEE | MEDICAL STATE OF THE PARTY NAMED IN | | | 23 | DESCRIPTION OF THE PERSON OF T | | |
| | * SOOO | 0000 | 0 10 | 0.1 | 0.3 | 8.5 | 0.0 | 0.8 | 0.90 | 0.10 | 100 | 222 | 11.4 | 130 | 11.3 | 1.00 | 11.10 | 2.0 | 2 /2 /2 | 33 | 22.55 | 2.0 | 2.8 | 200 | 211 |

A TABLE OF FEET AND INCHES from 6 foot 6 inches by 1 foot 6 inches and 1 quarter to 8 foot 11 inches and 3 quarters by 2 foot.

| FIPar | ts F.1 | E | E | I F | E | E | E | EI | EI | EI | | F.I | | F.I | FI | E1 | F.I | FI | F.I | EI | EI | F.I | FI | EI |
|----------|--------------------------------------|-------|--|--|--|------------------------------------|-------------------------|----------------------|----------------------------------|----------|---------|--|-------------------|---------------------------|-------------------------|----------------------------------|----------------------|--------------|--|--------------|------------------------------------|----------------------|-------------------------------|--|
| 6.0. | 1.6 | 1 10. | 0 10. | 2 10. | 7 1.7 | \$ 1.7 | 7 10.1 | 3 1.8 | 1.8 | 1.8 | 21.8 | 3 1.0 | 1.04 | 1.9% | 1.03 | 1.10 | 1104 | 1.10% | 1104 | 1.11 | 1.114 | 1.112 | 1.114 | 2.0 |
| | 3 10.0 | 10. | 1000 | 3 10. | # 10.0 5 10. | 000. | 7 10.0 | 0 10.1 | 11.0 | 11. | 2 //. 3 | 11.3 | 11.77 | 11.0 | 11.10 | 12.0 | 12.1 | 12.3 | 12.5 | 12.0 | 12.0 | 12.10 | 12.11 | 13.0 |
| 0.7.4 | 3 10.1 | 0000 | 2000 | 3 10 10 10 10 10 10 10 10 10 10 10 10 10 | 55000 | 7 10.00 10.00 10.00 10.00 | 0 10. N | | 11.2 | # | | 5 11.67 | 11.11.11 S0000 | 11.10 | 12.0 | 12.1 | 8888 8688 | 12.5 | 12.0 | 13:3 | 12.10 12.10 12.10 | 12.11 | 13.73 | 33333 |
| 6.8.4 | 10.9 | 10. | 3 10. | 5 10. | 7 10.6 | 0 10.10 | 0 11.0 | 2 11.1 | 11.3 | 11:3 | 5 11.0 | 11.88 | 11.9 | 12.0 | 12.1 | 12.33 | 12.4 | 12.6 | 12.8 | 12.00 | 12.11 | 1993 | 13:33 | 13.445 |
| 6.9.4 | 3 10.3 0 10.3 1 10.4 | 10. | 5 10. | 7 10.8 | 3 10.16 3 10.16 3 10.16 | 0 10.1 | 2 11.1 | 11.3 | 3 11.5 | 11.0 | 611.6 | 3 11.9 | 11.11 | 12.1 | 12.3 | 12.4 | 12.6 | 12.7 | 12.10 | 12.11 | 13.0 | 13.2 | 13.4 | 13.6 |
| 6.10 | 34 10.4 0 10.5 | 10.6 | 0 10. | 3 10.11 | 0 10.1 | 211.1 | 11.3 | 3 11.4 | 11.0 | 11.8 | 3 11.10 | 3 11.10 | 12.0 | 12.2 | 12.4 | 12.0 | 12.8 | 12.0 | 12.11 | 13.0 | 13.2 | 13.4 | 13.6 | 13.7 |
| 3 | 3, 10.0 | 10.8 | 7 10.9 | 0 10.1 | 111.5 | 7 11. | 2 // | | 11.7 | 11.9 | 91.16 | 12.0 | 12.2 | 12.4 | 12.5 | 12.7 | 12.0 | 12.10 | 13.00 | 3333 | 13.34 | 13.50 | 33.8 | 33.8 |
| 0.11.4 | 10.7 10.7 34 10.7 | 10.00 | 10.10 | 0 11.0 | | | 11.6 | 5 11.7 | 11.00 | 11.10 | 12.0 | 12.1 | 33,44 | 72.73.00 | 12.77 | 12.00 | 12.10 | 3333 | Section Sectio | 33445 | 2500 | 3333 | 33.00 | 13.11 |
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| 7.1.6 | | | | | | | | | | | | 12:5500 | | 12.8 | 12.10 | 13.0 | 13.22 | 3.3 | 13.5 | 3.0 | 13.00 | | 14.0 | 14.2 |
| 7.2.6 | | 11:1 | 11:3 | 2 11.3 | 11.6 | 5 11. 8 | 11.10 | 2 11.11 | 12.1 | 12.3 | 12.5 | 12.6 | 12.8 | 12.10 | 13.0 | 13.1 | 13:3 | 13.5 | 13:7 | 13:8 13:8 | 13.11 | 14.0 | 14.2 | 14.4 |
| 7.3.0 | 11.0 | 11.2 | THE RESIDENCE OF THE PARTY OF T | \$ 11.0 | 511.7 | 11.9 | 11.10 | 12.0 | 12.3 | 12.4 | 12.0 | 12.6 12.7 12.8 12.8 12.90 12.00 | 12.10 | 13.0 | 13.1 | 13.3 | 13.5 | 13.7 | 13.0 | 13.10 | 14.0 | 14.2 | 14.4 | 14.5 |
| a don's | 11.1 | 11.3 | 11.3 | 11.7 | 11.6 | 11.10 | 12.0 | 12.2 | 12.3 | 12.5 | 12.7 | 12.10 | 13.0 | 333.1 | 3333 | 33333 | 3.0 | 33.3 | 33.00 | 14.0 | 14.1 | 14.3 | 14.5 | 14.7 |
| 7. 4. 4. | 11.3 | 11.4 | 11.0 | | 11.10 | 12.0 | 12.1 | 2223 | 12.550 | 12.7 | 12.00 | 12.10 | 300 · | 3333 | 33333 | 3007 | 3333 | 33,000 | 13.11 | 14.1 | 4444 | 14.5 | 14.7 | 44.000 |
| 7.5.0 | 11.3 | 11.0 | 11.7 | 11.00 | 11.11 | 12.1 | 18.00 | 12.4 | 12.6 | 12.8 | 12.10 | 13.00 | 3333 | 3344 | 3.50 7 | 13:78:85 | 30000 | 13:11 | 14.1 | 14.3 | 445 | 14.6 | 14.8 14.9 14.9 14.10 | 14.10 14.10 14.11 |
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| 7.7. | 11.6 | | | | | | 12.0 | 12.7 | 12.10 12.10 12.10 12.10 | 12.11 | 13.1 | 13.3 | 13.5 | | | | | | | | | 14.10 | 15.0 | 15.2 |
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| 3 | - | | | | Name and Address of the Owner, where the Owner, which the Owner, where the Owner, which the | 12.0 | 12.8 | NAME AND ADDRESS OF | 13.0 | 3333 | 3.44 | 13.50 | 3.788 | 13.10 | 14.0 | 14.1 | 14.4 | 14.5 | 14.7 14.8 | 14.90 | 14.11 | 25.12 | 13.33 | 15.5 |
| Z. 9. 0 | 11.10 | 12.0 | 12.2 | 12.4 | 12.0 | 12.8 | 12.10 | 13.00 | 3000 | 7575 | 75,00 | 7,000 | 3333 | 33.100 | 14.1 | 4444 | 45.50 | 7778 | 14.8 14.0 14.10 | 14.11 | 15.12 | 1334 | 15.55 | 15.6 |
| 7.10.40 | 11.11 | 12.1 | 12.3 | 12.5 | 12.7 | 12.10 | 13.0 | 3333 | شاساسان ساساسان | 3333 | 13:3 | 10000 00000 | 13.10 | 14.0 | 4.333 | 14.45 | 14.67 | 14.800 | 14.10 | 15.0 | \$15,515 \$1.00.00 \$1.00.00 | 15.55 | 15.07 | 55.50 |
| 7.11.0 | 12.0 | | | Dell'arriver dell' | | - | _ | 13:33 | 13.5 | 13.6 | 13.80 | 13.10 | | | | | | | | 15.23 | 15.4 | 15.0 | 15.80 | 15.10 15.10 |
| 8.0.0 | 12,2 | 12.4 | 12.0 | 12.8 | 12.10 | 13.0 | 13.2 | 13.4 | 13:50 | 13.8 | 13.10 | 14.0 | 14.2 | 14.4 | 14.6 | 14.8 | 14.10 | | 15.2 | 15.4 | 15.0 | 15.8 15.8 15.8 | 15.10 15.10 | 16.0 |
| 8.1.0 | 12.2 12.3 12.3 | 12.0 | 12.8 | 12.10 | 13.0 | 13.2 | 13.4 | 13.5 | 13.7 | 13.0 | 13.11 | 14.1 | 4.3 | 14.5 | 14.7 | 14.9 | 14.11 | 15.1 | 15.3 | 15.5 | 15.7 | 15.0 | 6.0 | 16.1 |
| 3 | 12.4 | 12.0 | 12.2.0 | 12.10 | 13.0 | 3333 | 13:45 | 13.0 | 3330 | 13.10 | 14.0 | 14.22 | 4.5 | 14.7 | 4.80 | 14.11 | 15.1 | 5.33 | 15.5 | 5.7 | 15.00 | 16.0 | 6.1 | 16.3 |
| 40 | 12.5 | 14.19 | 12.10 | 11.2.0 | 33333 | 38.00 34.44.4 | 33337 | 73333 | 13.10 | 14.0 | 444 | 14.3 14.4 14.5 | 4.0 | 4.80 | 14.10 14.11 14.11 | 15.0 | 15.2 15.3 15.3 | 5.4 | 15.0 15.7 15.7 | 5.00 | 15.10 | 16.0 | 6.3 | 16.4 |
| 8.3.0 | 12.7 | 12.0 | 12.11 | 33330 | 13000 A | 33330 | 13:77.80 | 13.0 | 13.11 | 14.2 | 14.4 | 14.5 14.0 14.7 | 4.8 | | 15.0 | 15.12 | 15.4 | 5.00 | 5555 | 5.00 | 0000 | 00000 | 00.4 | 0.0 |
| 8.4.0 | 12.8 | | - | 3.33 | 3.4 | 13.0 | 3.000 | 13.11 | 14.1 | 14.3 | 4.5 | 14.7 | 4.0 | 14.11 | 15.1 | 15.3 | 15.50 | 5:78 5:88 | 15.10 | 0.0 | 0.2 | 0.4 | 6.6 | 6.8 |
| 8.5.0 | | 13.0 | 月.1 | 13.4 | 13.6 | 13.8 13.8 13.8 | 13.10 13.10 13.11 | | 14.2 | 4.5 | 14.7 | 14.8 | 4.11 | 5.1 | 5.3 | 15.5 | 3.7 3.7 3.8 | 5.0 | 15.11 | 0.2 | 0.3 | 0.5 | 0.7 | 16.10 |
| 8.6.0 | 12.11 | 13.1 | 13.3 | 13.5 | 13.7 | 13.0 | 13.11 | 14.2 | 4.4 | 4.6 | 4.8 | 14.10 | 5.0 | 5.3 | 5.4 | 15.7 | 15.0 | 5.11 | 6.1 | 0.3 | 0.6 | 6.7 | 6.9 | 17.0 |
| 453 | 13.00 | | | | | 12.11 | 14.2 | | 14.5 | 4.7 | | | - | - | | 5.0 | | | | 0.4 | | | 6.11 | 17.1 |
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| 8.8.0 | 10 0 | 13.4 | | | | 14.1 | 4.4 | 4.500 | 7,000 | 4.10 | 15.0 | 55555 | 5.4 | 5.07.78 | 5.800 | 5.11 | 6.11.20 | 0.3 | 0.50 | 00000 | 0.000 | 7.0 | 7.27.33 | 7.4 |
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34 10 0 3 10 0 3 10 0 3 10 0 3 10.1 10.10 16.11 16.11 16.11 10.10 10.11 17.0 17.77.77 18.11 18.00 4 0.07 9 0.7 9 0.8 7.67 20.0 20.1 20.1 20.2 77.00 Suna 20.1 20.2 20.2 20.3 10.5 10.5 10.6 17.11 20.3 20.4 20.4 20.5 20.0 20.7 20.7 20.8 20.1 20.1 20.2 20.2 (2) 2 2 8445 12:11 20.0 20.1 20.1 20.2 20.2 20.2 20.3 20.3 20.4 20.1 20.3 20.6 20.8 21.0 20.1 20.4 20.6 20.0 21.0 20.2 20.4 20.7 20.00 21.1 20.2 20.5 20.8 20.1 21.1 20.3 20.6 20.9 21.0 21.2 20.3 20.6 20.9 21.0 21.2 20.4 20.7 20.0 21.1 21.3 20.4 20.7 20.0 21.1 21.3 20.4 20.7 20.0 21.1 21.3 20.5 20.8 20.11 21.1 21.3 20.5 20.8 20.11 21.1 21.4 20.5 20.8 20.11 21.1 21.5 20.6 20.0 21.0 21.3 21.6 20.7 20.00 21.1 21.3 21.6 20.7 20.00 21.1 21.3 21.6 20.7 20.00 21.1 21.3 21.6 20.7 20.00 21.1 21.3 21.7 20.8 20.11 21.2 21.5 21.8 20.0 20.0 21.3 21.5 21.8 20.0 21.0 21.3 21.5 21.8 20.0 21.1 21.2 21.5 21.8 20.0 21.1 21.2 21.5 21.8 20.0 21.1 21.2 21.5 21.8 20.0 21.1 21.3 21.6 21.9 20.1 21.2 21.5 21.8 20.1 21.3 21.5 21.8 20.1 21.3 21.5 21.8 20.1 21.3 21.5 21.8 17.4 | 7.7 | 7.10 17.5 | 7.7 | 7.10 17.6 | 7.8 | 7.10 17.6 | 7.8 | 7.11 17.6 | 7.9 | 18.0 17.7 | 7.10 | 18.1 17.8 | 7.10 | 18.1 17.8 | 7.10 | 18.2 17.9 | 18.0 | 18.2 17.9 | 18.0 | 18.3 17.10 | 18.3 17.10 | 18.3 17.10 | 18.3 17.11 | 18.3 | 18.4 17.11 | 18.1 | 18.4 18:11 18.67 (8.7/ 10.8 10.00 1 18.3 18.4 18.5 10.53.50.0 21.5500 19.5 19.89 19.50 19.00 10.00 1 10.77.08 20.0 20.1 20.1 20.2 9999 22.0 22.0 22.1 22.1 9.00 9.80 9.7 9.00 9.7 9.00 9.8 9.10 9.9 20.0 8.77 18.00 10.0 10.3 10.0 10.3 10.7 10.4 10.7 20.2 20.2 20.3 20.3 19.55 80 80 9 19.05 80 9 10.05 80 9 10.05 80 9 10.05 80 9 10.05 80 20.4 20.5 20.5 20.6 20.0 20.7 20.7 18.6 18.6 18.7 22.2 22.3 22.3 22.3 22.4 22.4 22.5 22.5 18.80 18.00 19.00 10.00 18.11 Q.23 Q.03 Q.03 Q.03 20.1 20.2 20.2 20.2 8.2.33 19.6 19.7 19.8 20.3 20.3 20.4 20.4 10.1.2 20.0 20.1 20.1 20.1 22.0 22.0 22.7 22.7 22.7 20.2 20.3 20.3 8.34 18.6 9.00.1 9999 9000 10.11 20.0 20.0 20.0 20.5 20.5 20.6 20.6 20.7 20.8 20.8 20.9 20.0 20.3 20.1 20.0 20.0 21.0 20.7 20.0 21.1 20.7 20.0 21.1 20.8 20.11 21.2 20.8 20.11 21.2 20.9 21.0 21.2 20.9 21.0 21.3 20.0 21.1 21.3 21.3 21.6 21.9 21.1 21.3 21.6 21.10 22.0 21.4 21.7 21.10 22.1 21.3 21.8 21.11 22.2 21.3 21.8 21.11 22.2 21.3 21.8 21.11 22.2 21.3 21.8 21.11 22.2 21.3 21.8 21.11 22.2 7 10 10 व्यक्तिक विश्वतिक विश्वतिक विश्वतिक विश्वतिक विश्वतिक 5500 Q.122 Q.23 Q.3 20.1 20.1 20.2 20.2 18:11 9999

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A TABLE OF FEET AND INCHES.

| | NAME OF THE PARTY | en ju | 000 | Jugue | | 7500 | o ar | vies | ana | 194 | arcer | to | 2 100 | t 5 1 | inch | es an | d3 | quai | ters | · vy | 2 100 | <i>t</i> . | / | |
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| 1113 | FI | FI | | FI | FI | FI | FI | F.I | EI | Water Committee of the | E | M Chambaltaneria | DI | OI | EU | FI | FI | FI | FI | FI | FI | FI. | FI. | F.I. |
| FI Parts | 72.9 | 12.9 | 18.4 | 2 18.2 | 10.5 | 18.8 | 18.11 | 10.2 | 1.8 | 1.8 | of markets | 1.0 | | | | | | 21.7 | 21.10 | 22.0 | 22,3 | 1.112 | 1.114 | 2.0 |
| 3 | 7.7 | 17:10 | 18:0 | 18.3 | 18.9 | 8.9 | 9.00 | 0000 | 9.0 | 20.5 | 0.10 | A HANGESTATION | | 20000 | | 21.1 | 21.5 | 21.78 | 21.10 | 22.1 | 22.4 | 22.7 22.7 22.8 | 22.10 22.10 22,11 | 23.0 |
| 11.7.0 | 7.3 | 7.19 | | 18.3 | 18.7 | 18:40 | 00000 | 9999 | 10.7 | 10.10 | 20.0 | 20.3 20.4 20.4 | 20.6 20.7 20.7 | 20.0 20.0 20.10 | 21.0 | 21.33 | 21.6 | 21.00 21.10 21.10 | 22.0 22.0 22.0 22.1 | 22,2 22,3 22,3 22,4 | 22.5 22.6 22.6 22.7 | 22,8 22,0 22,0 22,0 | 22.11 23.0 23.0 | 23.2 |
| 11.8.9 | 7:9 | 18:0 | 18.3 | 18.0 | 18.9 | B:11 | 10:3 | 18:3 | 18:8 | 19.1 | 20.2 | 20.5 | | | | | | 21,10 | 22.1 | 22,4 | 22.7 | 22.10 | 23.1 23.1 23.2 | 23.4 |
| 400 | 17.10 | 18.1 | 18. 4 VA. 4 | 18:7 | 18.10 | 19.1 | 10.4 | 10.7 | 10.10 | 20.0 | No. of Concession, Name of Street, or other Persons, Name of Street, or ot | 20.6 | 20.9 20.9 20.9 | | | 21.5 | | | | 22.5 | 22.8 22.8 22.8 | 22,11 | 23.3 | 23.5 |
| 3 | 18.0 | 18.2 18.3 | 18:3 | 1000 | A SECTION ASSESSMENT | 10,000 | \$000 9 | 70.70.8 | 0.10 | 20.1 20.1 20.2 20.2 | 20.4 20.4 20.5 20.5 | 20.7 20.8 20.8 | 20.10 | 21.1 | 21.4 | 21.7 | 21.10 21.10 21.10 21.11 | 22.0 22.1 22.1 22.2 | 22.4 22.4 22.5 | 22.7 22.7 22.8 | 22.10 22.10 22.11 | 23.1.23.2 | 33.4 33.4 35.5 | おりつつ |
| 11.10.0 | 194.0 | 1888 | 18:00 18:07 | 19.00 | 0000 | 10.33.4 | 0077 | 0000 | 20.0 20.0 20.0 | 20.2 20.3 20.3 | 20.0 20.0 20.0 20.7 | 20.8 20.0 20.0 20.0 | 20.11 21.0 21.0 | 21.2 | 21.5 | 21.8 | | 22 2 | 22.5 22.6 22.6 22.7 | 22 0 | | 23,33,34 | 23.5 23.6 23.6 | 23.8 23.8 23.8 |
| 11.11.0 | 18.1 | 18.4 | 18:3 | 18.10 | 10.1 | 10.4 | 10 7 | 19.10 | 20.1 | 00 | 00- | 20.10 | 21.1 | 21.4 | 21.7 | 21:10 | 22.1 | 22 4 | 22 7 | | | 23.4 23.4 23.5 | 23.7 | 23.9 23.10 23.10 |
| 12.0.0 | 18.3 | 18.0 | 18.9 | 10.0 | 200 | - | 0000 | - | | | | 20.11 | 21.3 | 21.5 | | TO STATE OF THE PARTY OF THE PA | - | 22.5 | 22.8 22.8 22.9 | 22,10 22,11 22,11 23.0 | 23.2 | 23.6 | 23.8 | 23.11 |
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| 12.1.0 | 18.35 S | (B) | 18.11 | 00000 | 10.55 | 00000 | 19.11 | 20.2 20.2 20.2 20.3 | 20.5 20.5 20.6 20.6 | 20.8 20.8 20.9 | 20.11 20.11 21.0 21.0 | 21. 2 21. 3 21. 3 | 21.5 | 22222 | 21.11 | 22.2 22.3 22.3 22.3 | 22.5 22.5 22.6 22.6 | 22.8 | 22.11 23.0 23.0 | 333333 | 23.55.00 | 23333 | 23.11 24.0 24.0 | 24.2 |
| 12.2.8 | 18.0 | 18.9 | 19.0 | 19.3 | 19.67 | 10.00 | | | | | | 21.3 | 21.7 | 21.10 | 22.1 | 22.4 | 22.7 | 22.10 | 22.0 | 23.4 | 23.7 | 23.10 | 24.1 | 24.4 24.4 |
| 12.3.8 | 18.8 | 18.10 | 19.1 | 10.4 | 19.7 | - | 20.2 | | 000 | 001 | 21.2 | 21.5 | 21.8 | 21.10 | 22.2 | 22.5 | | | | 23.6 | 23.8 23.8 23.9 | 23.11 | 24.2 | 24.5 24.5 24.6 |
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| 12.5.0 | 18.11 | 10.22 10.22 10.22 | 9000 | 19.88 | 10.11 | 20.2 | 20.5 20.6 20.6 20.6 | 20.8 | 2011 | 21.3 | 21.6 | 21.0 | 22.0 | 22.3 | 22.6 | 22.0 | 220 | 23.3 | 23.6 | 23.10 | 24.1 | 24.4 | 24.7 24.7 24.7 | 24.10 24.10 24.10 |
| 3 | 19.0 | 19.3 | 19.6 | 19.9 | 20.0 | 20.3 | 20.6 | 20.10 | 21,1 | 21.4 | 21.7 | 21.10 | 22.0 | 22.4 | 22.7 | 22.11 | 23.2 | 23.5 | 23.8 | 23.11 | 24.2 | 24.5 | 24.8 | 24.11 |
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| FI Parts | F.I. 2.05 | F.I. 2.1 | FI. 2.12 | F.I. 2.2 | F.I. | FI. | FI. | FI. | F.I. 2.45 | 2 You F.I. 2.5 | FI. | FI. 2.6 | FI. | FI. | FI. 2.7½ | F.I. 2.8 | F.I. 2.8½ | F.I. 29 | F.I. 295 | FI. 2.10 | FI. | FI. 2.// | FI. | FI. 3.0 |
| FI Parts 2 0 12 2 2 14 2 2 14 | F.I. 2.05 | F.I. 1100 7000 | FI. 2.13 | F.I. 2.2 4.8 4.90 5.00 | F.I. 2.2½ | F.I. | F.I. 2.35 | FI. | 6y F.I. 2.45 | 2 you F.I. 2.5 | FI. 25% | FI. 2.6 | FI 26% | F.I. 2.7 | FI. 2.7% | F.I. 2.8 | FI. 2.8½ | F.I. 29 | F.I. 295 | FI 2.10 | FI. | FI. 2.11 | FI. | FI. 3.0 |
| FI Parts 2.01/2 2.93/8 2.93/8 2.95 | F.I. 2.052 | F.I. 2.1 440 1000 10 | F.I. 2.12 167 188001 12 | F.I. 2.2 | F.I. 2.2½ | FI. | FI. | FI. 2.4 | F.I. 2.45 | 2 you FI. 2.5 | FI. | FI. 2.6 | FI. 26% | FI. 2.7 | FI. 2.72 | F.I. 2.8 | FI. 2.8½ | F.I. 29 | FI. | FI. 2.10 | FI | FI. 2.// | F.I. 2.1/2 | FI. 3.0 |
| FI Parts 2 0 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | F.I. 2.052 97.05 07.00 0 | FI 2 110 1000 20.00 1 | FI 2.15 67 88801 1999 6 | F.I. 2.2 | F.I. 2.2% | F.I. 2.3 | FI. 2.35 00 10000 00 | FI. 2.4 | F. I. 2.45 | FI. 2.5 | FI. 252 | 6.3 | FI. 26% | F.I. 2.7 | FI. 2.72 | FI. 2.8 | 700 F.I. 2.8 2 | FI. 29 | FI. | FI. 2.10 | FI | FI. 2.11 | FI. 2.1/2 | FI. 3.0 |
| FI Parts 2 0 12 42 42 42 42 42 42 42 42 42 42 42 42 42 | FI 2.0% 2000 0000 0000 00000 00000 00000 | FI 2 144 144 1500 5000 | FI 67 8001 -1994 5078 | F.I. 2.2 + 8 000 - 2345 0780 | F.I. 2.25 10.2 7450 7001 | F.I. 2.3 1957 0010 | F.I. 2.35 NO 19019 1900 | FI. 2.4 5.5 000000 0000000000000000000000000000 | F. I. 2.45 5,5,5,5 0000 | FI. 2.5 | F.I. 252 | 6.3 6.3 6.3 6.5 6.8 | FI. 26% | F.I. 2.7 | F.I. 2.75 | FI. 2.8 | 7000 8 F.I. 2.8 ² 2 | FI. 29 | FI. | FI. 2.10 | FI | FI. 2.11 | FI. | FI. 3.0 |
| FI Parts 2 0 12 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 | FI 2.0% **** **** **** 500 000 0000 0000 | FI 2 +++ ++++ +500 5000 5000 | FI. 2. 67 8502 - 197 15018 0023 | F.I. 2 # ##55 5555 5555 5566 | F.I. 2.252 Frank Shan Shan Society | F.I. 2.3 199 1997 9020 1991 | FI. 2.35 90 1000 0000 00000 | FI. 2.4 5.50 0000 00000 00000 00000 | FI. 2.48 | F.I. 2.5 | FI. 252 00007 00007 | 6.3 6.3 6.3 6.3 6.3 6.3 6.3 6.3 | FI. 26% | F.I. 2.7 | F.I. 2.752 | F.I. 2.8 | 7.4 7.5 7.7 | F.I. 2.9 | F.I. 295 | FI. 2.10 | FI | FI. 2.11 | FI. | FI. 3.0 |
| FI Parts 2 12 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 | FI 20 19 19 19 19 19 19 19 19 19 19 19 19 19 | FI 2 *** *** **** **** **** **** **** ** | F. 1. 67 88.62 . 19 190 90 90 00 000 000 | F. I. 2 # ## 55 5555 5755 5755 5755 5656 566 | FI 2.2 10 . 2 74 56 74 50 000 000 000 | FI. 3 199 1997 9010 1994 000 | FI. 2.35 35 3500 0000 0000 0000 0000 | FI. 2.4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 | F.I. 2.45 | FI. 2.5 | FI. 252 00007.0007.0007.0007.0007.0007.00 | 6.3 6.3 6.3 6.3 6.0 6.0 7.1 7.3 8 | FI. 26% | F.I. 2.7 | F.I. 2.7% | F.I. 2.8 | FI. 2.8½ | F.I. 20 | F.I. 2.95 | FI. 2.10 | FI | FI. 2.// | FI. 2.1/2 | FI. 3.0 |
| FI Parts 2 0 12 42 42 42 42 42 42 42 42 42 42 42 42 42 | FI. 20 19 19 19 19 19 19 19 19 19 19 19 19 19 | F 2 114 1144 1999 9999 9999 9999 9999 999 | FI 2 67 8862 1994 1000 0000 0000 00 | F. I. 2 # ## 55 5555 5755 5755 5755 565 5656 56 | FI 2.25 ** 10.00 may 0 0000 0000 0000 0000 0000 0000 0 | F.I. 23 1997 9010 1994 0100 000 | FI. 33 34 MONO 0200 0000 0000 0000 0000 0000 0000 0 | FI. 2. 4 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | F. I. 2.45 SANDE ON STANDER STANDER STANDERS STA | FI 2.5 | FI. 252 0000 0007 1234 07 | 6.3 6.3 6.3 6.3 6.3 6.3 6.3 6.3 7.7 7.7 7.7 | FI. 26% | F.I. 2.7 | F.I. 2.7 2 7.7.7. 7.7.7. 88.00 0. | F.I. 2.8 | FI. 2.8 ² 2 | F.I. 29 | F.I. 2.9% | FI. 2.10 an anama an | FI 200 mylor og | FI. 2.// | F.I. 2.1/2 | FI. 3.0 |
| FI Parts 2 0 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | FI 20 0 may 0 0 may 0 0 may 0 0 may 0 0 0000 000 | FI 2 *** *** *500 5000 5000 0000 0000 0000 | TI 07 0002 - 19 19000 0000 0000 0000 0000 0000 000 | F. I. 2 + ** 55 5555 5555 5556 5566 5566 5566 5 | FI 2.25 Finn non non 0000 0000 0007 | F.I. 3 199 1997 9010 1994 0700 0077 7 | FI. 35 10000 0000 0000 0000 0000 0000 0000 | FI. 4 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | FI. 2.48 1999 0000 0000 0000 0000 0000 0000 000 | FI. 2.5 | FI. 25 2 0000 000 7 23 7 7777 7777 7777 7777 7 | 6.3 45,78 0,001 73,50 73,77 7,777 7, | FI. 26% | F.I. 2.7 | F.I. 2.7% | F.I. 2.8 | F.I. 2.8 2 2 3 3 5 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 | F.I. 20 | F.I. 295 | FI. a. to an anoma | FI 200 major 000 - 0 | FI. 2.11 | F.I. 2.1/2 | FI. 3.0 |
| FI Parts 2 19 19 19 19 19 19 19 19 19 19 19 19 19 | FI 20 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | F. 2 *** *** **** **** **** **** **** ** | FI 2 67 80.02 . 1974 150 18 19 00 00 00 00 00 00 00 00 00 00 00 00 00 | F. 2 # ** 55 5555 5755 5755 5755 5556 5556 555 | FI 2.25 10.2 9450 7000 0000 0007 0000 1094 | FI. 3 . ימש אישט ספים ספים פים שאישט אישט אישט אישט ספים ספים שאישט אישט אישט אישט ספים פים אישט אישט אישט אישט אישט אישט אישט אישט | FI 33 5000 0000 0000 0000 0000 0000 0000 | FI. 4 5 00000 0000 0007 7777 7777 7777 | FI. 2.48 5995, 0000 0000 0077 7777 7777 | FI. 2.5 | FI. 25 2 0000 0007 7777 7888 10.2 | FI. 2.6 | FI 26 % 07,000 07,77 77,77 77,78 00000 07,77 77,77 77,78 00000 | FI 2 7 2000 2000 2000 2000 2000 2000 2000 | F.I. 2.752 6.7. 7.7.7. 7.7.7. 90000 00000 | F.I. 2.8 | F.I. 2.8 2 2 3 2 3 3 5 7 5 7 | F.I. 2 9 | F.I. 2.9% 7.7. 00000 00000 00000 00000 00000 | FI. a. to among among again | FI 200 mylo 7 000 - mylo 7 | FI. 2.11 | F.I. 2.1/2 | 0,0000 |
| FI Parts 2 19 49 49 49 49 49 49 49 49 49 49 49 49 49 | FI 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | F 2 114 1144 1999 9999 9999 9999 9999 999 | F. 2 4+ +++ nynn nynn nynn odog ogg og | F. 2 # ## 55 5555 5555 5555 5555 5555 555 | FI 2.25 FOND NOND NOND 0000 0000 0000 1294 574 | FI. 3 1997 9010 1994 0000 0000 9450 7000 | FI 33 34 36 30 0000 0000 0000 0000 0000 00 | FI. 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 | | FI 2.5 | FI 25 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | 6 0000 0000 0000 0000 0000 0000 0000 0 | FI 26 % 1012 4507 7777 7777 7777 7777 9000 07777 7777 | FI 2 7 2000 2000 2000 2000 2000 2000 2000 | F.I. 2.7% | F.I. 2.8 | FI. 2822 | F.I. 29 | F.I. 2.9% F.I. 2.9% 7.7. \$\frac{1}{2} \text{ \$\frac{1}{2} | FI 2.10 B BOOM TO | FI 22 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | FI. 2.11 | F.I. 2.182 | 0,0000 |
| 3.45 | FI 20 0 mm by 0 0 mm 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Z-0 7-2 7-3 | FI 37 85/22 - 1994 15078 0/20 - 1994 0788 220 1 19945 | F. 2 # # # 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 | FI 2.25 1000 9450 7000 0000 0007 7177 7577 77 | FI. 3 199 1997 9010 1994 0780 0101 3450 7800 01 | FI 33 19070 0000 0000 7777 7778 88 | FI. 4 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 8.00 | FI 25 | FI 25 25 25 25 25 25 25 25 25 25 25 25 25 | FI. 2.6 | FI. 26 % O 0000 0 777 7777 7778 annum annum annum | FI 2 7 | 8.00 | 0000 | 00000 | 9999 | 9999 | 2000 | 9000 | 90.0 | 10.0 10.0 10.3 10.4 | 0.0000 00000 00000 00000 00000 00000 00000 |
| 3.000 | 0777 7777 | 7777.3 | F1 3 67 80/21 - 197 5/078 0/20 - 197 0780 0200 0000 0007 7777 7777 7777 777 | F. 2 # ** 55 5555 5555 5556 5566 5566 5575 7577 7777 8001 0 | - | 0.0 | Caronio Caroni | 0.1 | OLUN NOVO | FI 5 | FI 25 00 0000 0007 NAAA 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 | FI. 2.6 | FI 26 % 07.000 10.2 4507 0000 0000 0000 0000 0000 | FI 7 000 7777 7777 7000 0000 0000 0000 | 80000 V507 | 0000 0000 | 00000 7000 | 33507 0000 | 9999 9099 | 000000000000000000000000000000000000000 | 000000000000000000000000000000000000000 | 90.0 | 10.0 10.0 10.3 10.4 | 0,0000 |
| 3,000 00000 | 0777 7777 7 | 7777.3 | FI 37 85/22 - 1994 15078 0/20 - 1994 0788 220 1 19945 | F. 2 # # # 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 | 03,40 | 8888 | | OMA | OLAH MONE STOR | FI 5 | FI 25 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 | FI. 2.6 | FI 26 10 10 10 10 10 10 10 10 10 10 10 10 10 | FI 2 7 2000 0124 5000 0012 3507 0010 2350 7001 | 8000 0000 0000 0000 0000 0000 0000 000 | 000000000000000000000000000000000000000 | 23 NO 7801 1935 | 3507 0000 2450 | 9999 9099 | 0000 00000 00000 00000 | 9000 | 90.0 | 10.0 10.0 10.3 10.4 | 0.0000 00000 00000 00000 00000 00000 00000 |
| 3,000 00000 | 0777 7777 7870 7890 7877 7777 7777 7777 | 7777 7777 7778 | F 2 47 4744 55555 5555 5555 5555 5555 555 | F. 2 # # # 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 | 03,40 | 8888 | Caronio Caroni | 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 | OLAH MONE STOR | FI 5 | FI 25 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 | FI. 2.6 | FI 26 10 10 10 10 10 10 10 10 10 10 10 10 10 | FI 2 7 2000 0124 5000 0012 3507 0010 2350 7001 | 8000 0000 0000 0000 0000 0000 0000 000 | 000000000000000000000000000000000000000 | 23 NO 7801 1935 | 3507 0000 2450 | 9999 9099 | 9000 1000 35 07 000 000 000 000 000 000 000 000 000 | 90000 11 1 10 2 4 50 10 10 10 10 10 10 10 10 10 10 10 10 10 | 0.10 10.0 10.2 10.4 10.5 10.8 10.10 10.10 11.12 | 10.0 10.3 10.7 10.7 10.7 10.7 10.7 11.3 | 0.0000.0000.0000.0000.0000.0000.0000.0000 |
| 3. 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 0777 7777 | 7777 7777 7778 | F. 2 ** *** none none one oco oco oco oco oco oco oco oco oco oc | F. 2 # ##55 5555 5555 5556 0506 0506 0577 7777 3000 0500 0500 | Company Company | 90000 90000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Carlos cacas castas | 10000 0000 0000 0000 0000 0000 0000 00 | ONTH NOVO STON WAND | FI 5 | FI 25 00 0000 0007 1277 7777 70000 00000 00000 00000 | FI. 2.6 | FI. 65% | FI 2 7 200 7777 7777 7888 8888 8888 9889 9899 989 | 8000 0000 0000 0000 00000 00000 00000 0000 | 00000 4 | 00000000000000000000000000000000000000 | 33507 0000 | 9999 9000 9000 9000 9000 9000 9000 900 | 00000 0000 0000 0000 0000 0000 0000 0000 | 90000 00000 00000 00000 00000 00000 00000 | 9.10 10.0 10.2 10.2 10.5 10.6 10.10 10.10 10.11 11.2 | 10.0 10.3 10.6 10.6 10.6 10.6 10.6 10.6 10.6 10.6 | 0,0000 |
| 3,000 00000 | 0777 7777 7870 7890 7877 7777 7777 7777 | 7777 7777 7778 | F 2 47 4744 55555 5555 5555 5555 5555 555 | F. 2 4 4455 5555 5555 5555 5550 5550 5550 | COOR BOOK TONE | 1507 0010 1994 1507 0010 1994 | 100 0000 cacco cacco | Sold Alano Sold | CONTRACTOR OF THE PROPERTY AND | FI 5 | FI 25 00 0000 0007 NAAA 78000 0000 0000 0000 0000 0000 0000 | FI. 2.6 3 45,78 0,001 23,45 78,01 0. 34 5,000 0 | FI 26 07.00 11012 1907 0011 1000 0000 0000 0000 0000 0000 | FI 7 2006 7777 7777 7888 8888 8889 0000 2000 2000 2000 | 8000 0000 0000 0000 7000 9000 0000 0000 9000 7000 | 00000 4 | 23 x6 7 3001 1 2 3 5 0 7 0 0 0 1 1 2 3 | 9507 9501 9750 8020 1975 | 9000 0000 0000 0000 0000 0000 0000 000 | 00000 0000 0000 0000 0000 0000 0000 0000 | 90000 00000 00000 00000 7000 | 9.10 10.0 10.0 10.0 10.0 10.0 10.0 10.0 | 10.0 10.3 10.6 10.6 10.6 10.6 10.6 10.6 10.6 10.6 | 0,0000,0000,0000,00 |

A TABLE OF FEET AND INCHES from 4 foot 4 inches and a half by two foot and half an inch to 9 foot 4 inches by 3 foot.

| FIPa | rts F.I | FI | FI | FI | FI | FI | FI | FI | FI | FI | FI | FI | FI | FI | FJ | EI | FI | FI | EI | F.I | FI | F.I | F.I | F.I |
|--------------------------|---|-------------------|--|--|---|--------------|---|-------------------------------|------------------------------|----------------------------|------------------------------|-------------------------------|---|--------------------------------|--|---|---|------------------------------------|--------------------------------|--|--|--|---|-------------------|
| 7.43 | 2.0% | 2.1 | 2.14 | 2.2 | 0.0 | 2.3 | ed blockeds | of Britisher | 2.4 | OF BRIDGE | 2.5 | ESS URESCONDENS | 26 | 4 2.7 | 27 | 2.8 | 2.8 | 2.9 | 2.0 | 2:10 | 2.10 | 2.11 | 2115 | 3.0 |
| 550 | 0000 | 9.3 | 9.50 | 10.7 | | 9.1 | 10.0 | 10.4 | 10.0 10.7 10.8 | 10.8 | 10.10 | 11.6 | 3 //. | 11.5 | all individue | 的 的复数克莱斯姆斯 | 12.2 | 12.3 | 12.5 | 12.0 12.8 12.9 | 12.8 | 13.0 | 1333.4 | 3 × 6 |
| 7.0 | 9000 | 9999 | 999 | 0.10 | 10.0 | 10.5 | 10.0 | 10.7 10.8 10.0 | 10.0 | 11.0 | 71. | 11.9 | 11. | 1/18 | 12.2 | 12.13.45 | 12.9 12.9 12.0 12.8 | 12.0 | 12.0 | 12.10 | 13.0 | 33.60 | 357.8 | 13.70 |
| 4.8 | CONTRACTOR | N. CARRON, CARRON | 10.0 | 10.2 | 10.5 | 10.7 10.8 | 10.0 | 11.0 | 11.2 | 11.0 | #: 7 #: 8 | 11:10 | 2 /2.0 | 12.2 | 12.0 | 12.7 | 12.00 | a management of | 13.2 | 13.4 | 3.0800 | 13.00 | 13.11 | 14.1 |
| 4.10 | 9.10 | 10.2 | 10.4 | 10.7 | 10.9 | 10.10 | 11.1 | 11.3 | 11.7 | 11.0 | 12.0 | 12.1 | 12.5 | 12.7 | 12.10 | 13.0 | 13:2 | | 13:3 | 13.0 | 13:11 | 4.3 | 14.4 | 14.0 |
| 5.0 | 10.2 | 10.4 | 10.6 | 10.8 | 10:10 | 11.2 | 11.5 | 11.7 | 11.60 | 12.0 | 12.3 | 12.5 | 12.7 | 12.10 | 13.0 | | | B AND AND | 300 | 14.2 | 14.3 | 4.6 | 4.8 | 4.00 |
| 5.0 % | 10.5 | 07.80 | 10.10 10.11 11.0 | 11.0 | 11.3 | 11.5 | 11.8 | 11.10 | 12.1 | 12.3 | 12.0 | 12.10 | 12.11 | 13.99.3 | 13.3 | 13.57.89 | 03334.0 | 13.001.2 | 14.2 | 4444 | 14.70 | 14.10 | 15.0 | 5.3 |
| 5. 2. 4 | 10.8 | 10.10 | 11.1 | 11.3 | 11.0 | 11.10 | 11.11 | 12.2 | 12.4 | 12.7 12.8 12.9 | 12.10 | 13.0 | 13.3 | 13.5 | 13.8 | 13.11 | | | 14.0 | 14.0 | 15.0 | 15.2 15.4 15.5 | 15.5 15.5 15.8 | 15.70 |
| 5.4 3 | 11.0 | 11.2 | 11.5 | 11.8 | 11.10 | 12.1 | 12.3 12.4 12.5 12.6 12.7 | 12.0 | 12.9 | 13.0 | 13.3 | 3.4 | 13.8 | 13.11 | - | A Revision of the | - | DESTRUCTION OF | 15.0 | 15.3 | 15.5 | 15.8 | 15.11 | 10.0 |
| 5.0 % | 11.3 | | | | | 12.4 | 12.7 | 12.10 | 13.2 | 13.5 | 3.7 | 13.00 | | 14 | 14 2 | 14 0 | 15.0 | 15.3 | 15.0 | 15.7 15.8 | 15:11 | 16.0 | 0.3 | 0.6 |
| 5.8 5 | 11.4 | 11.30 | 11.11 | 12.3 | 12.5 | 12.8 | 12.11 | 33.3 | 33.5 | 3.8 | 33.11 | 14.2 | 14.4 | A Commission of the last | 4.8 | 15.0 | 15.3 | - | 3.8 | 18:1 | 16:3 | 18:3 | 6.8 | 0.10 |
| 5.80 % | 11.8 | 12.0 | 12.3 | 12.57 | 12.80 | 13.0 | 33334 | 3888 | 3333 | 13.11 | 4.0234 | 14.6 | 14.7 | 15.0 | 15.54 | 15.54 | 7.80 | 15.80 | 1000 | 350 | 0000 | 16.3 | 7.0 | 7.3 |
| 6.4 5 | | 12.3 | 12.6 | 12.0 | 13.0 | 13.3 | 13.0 | 13/3/10 | 13.11 | 14.2 | 14.5 | 14.8 | 14.11 | 15.53 | 15:55:85 15:55:85 | 15.80,10 | 15:11 | 00356 | 10000 1000 1000 | 80,00 | 16.11 | 77.35 | 7.5 | 7.7 |
| 6.0 % | 12.4 | 12.7 | 12.10 | 19.1 | 19.4 | 19.7 | - | | | | | | | - | 15:10 | 10.1345 | 10.4 | 10.7.00 | 16.10 | 17:13 | 77.8 | 7:70 | 7.10 | 8.3 |
| 6.2 % | 12.7 | 12.10 | 13.2 | P-CHICAGO | North Designation | - | 14.2 | COMMENTS AND | 14.0 | 15.0 | 15.2 | 15.6 | GALDEN TRANSPORT | Distance Management | BOOK MARKET | 16.7 | 16.10 | 17.1 | 17.4 | 7.6 | 17.0 | 18.0 | 8.2 | 8.8 |
| 6.4 % | 12.11 | 13.2 | 13.4 | 13.8 | 19.11 | 14.2 | 14.5 | 14.8 | 15.0 | 15.2 | 15.6 | 15.00 | 16.0 | 16.3 | 16.0 | 16.6 | 17.0 | 17.3 | 17.7 | 17.10 | 18.2 | 8.0 | 8.9 | 9.0 |
| 550 | 13.2 | 13.50 | 333 | 13.11 | 14.2 14.3 14.4 | 14.5 14.7 | 14.10 | 15.0 | 15.3 | 15.6 15.7 15.8 | 15:01 | 16.02 | 10.5 | 10.7 | 16,11 | 17.13 | 7.0 | 7.8 | 17.11 | 18.2 18.4 18.5 | 8.5 | 8.0 | 0.0 | 0.3 |
| 6.6 % | 13.4 | 13.80 | 13.11 | 14.2 14.3 14.4 | 4.5780 | 14.0 | 15.0 | 15.345.7 | 15.00 | 15.10 | 00000 | 16.4 | 10.80 | 17.0 | 7.2 | 7.5 | 17.00 | 18.0 | 83507 | 18.6 18.6 19.6 19.6 19.6 19.6 19.6 19.6 19.6 19 | 18.10 | 0000 | 0.070 | 0.7 |
| 6.8 % | 13.8 | 4.0 | 14.3 | 14.6 | 14.10 | 15.1 | 15.4 | 15.8 15.10 | 15.11 | 16.3 | 10.0 10.7 10.8 | 16.00 | 17.1 | 77:3 | 17:30 | 17.11 | 18.33 | 18.57 | 18.00 | 10.0 | 10.3 10.3 10.3 | 9.7 9.8 9.80 2 | 0.0 | 20.1 |
| 0.10 % | 13.11 | 4.4 | 4.7 | 14.10 | 15.2 | 15.6 | 15.0 | 10.0 | 10.4 | 10.7 | 16.11 | 17.2 | 17.6 | 17.00 | 17.11 18.1 18.2 | 18.4 | 18.0 | 18.0 | 9.1 9.2 9.4 | 9.6 | 9.8 | Q.11 2 20.1 2 20.2 2 | 0.3 | 0.0 |
| 7.0 2 | 14.4 | 4.8 | 15.0 | 15.2 | 15.5 15.7 15.8 | 15.0 | 16.0 | 16.4 | 16.7 | 17.0 | 17.3 | 17.0 | 7.9 | 18.2 | 18.5 | 18.9 | 18.11 | 19.3 10.4 | 19.6 | 930 | 20.1 | 0.5 2 | 0.02 | 1.0 |
| 7.2 1/2 | 4.8 | 4.11 | 15.3 | 15.5 | 15.10 | 16.0 | 16.5 | 16.7 | 17.0 | 17.4 | 17.0 | 17.10 | 18.3 | 18.5 | 18:10 | 10.0 | 19.5 | 10.10 | 20.0 | 20.4 | 20.0 | 0.0 2 | 1.1 2 | 1.6 |
| 33 4 | 15.0 | 5.2 | 13.7 | 15.10 | 10.0 | 10.4 | 16.70 16.10 | 17.0 | 7.3 | 7.0 | 17.10 | 18.1 | 18.50 | 18.00 | 00.23 | 0057 | 6.8 6.0 6.0 | | 20.3 | 10.6 10.8 10.9 | 20.10 2 | 1.3 2 | 1.5 2 | 1.00 |
| 7. 4 4 | 15.03.4 | 5.507 | 5.8 | 0.0 | 0.3 | 10.7800 | 17.0 | 77.77.0 | 7.07 | 17.10 17.11 18.0 | 8888 888 | 15/6 BO | 00011 | 0000 | 9.9078 9.90.78 | 10.11 | 20.0 20.1 20.2 20.4 | | 20.7 20.8 20.10 20.11 | 20.11 21.0 21.2 21.3 | Children with the | 1.0 2 | 1.10 2.1 2.1 2.2 | 2.3 |
| 7.6 % | 15.5 | 5.0 1 | 6.0 | 6.4 | 16. B | 17.0 | 7.5 | 7.7 | 17.11 | 8.3 | 18.60 | 18.10 | 10.03 | 10.6 10.7 10.8 | 20.0 | 20.3 | 20.5 20.6 20.8 | 20.0 | 11.2 | 21.6 | | 2.02 | 2.4 2 2 2 2 2 2 2 2 2 2 | 2.7 |
| 7.8 % | 15.00 A | 0.0 | 0.5 | 6.8 | 7.0 | 7.3 | 7.7 17.8 17.9 | 8.0 | 8.4 | 8.8 | 18.11 | 19.2 19.3 19.3 | 10.0 10.7 10.8 | 10.11 | 20.3 | 20.5 20.7 20.8 | 20.10 | 21.22 | 1.8 | 11.9 2 11.10 2 11.11 2 | 22.0 2 22.2 2 2.3 2 | 2.4 2 2.6 2 2.7 2 | 2.8 2 2.10 2 2.11 2 | 3.1 |
| 7.10 % | 16.0 11 16.1 N | 6.4 A | 6.8 | 7.0 | 7.4 | 7.7 | 17.11 | 8.3 | 8.8 | 19.0 | 9.3 | | | | 20.5 | 21.0 | | | PRODUCTION OF THE | | 2.6 2 | 3.02 | 3.4 2 | 3.7 |
| 8.0 2 | 10.3 10 10.4 10 | 5.9 | 7.2 | 7.3 | 7.8 | 18.0 | B. 3 B. 4 | 8.7 | 9.0 | 10.3 10.4 | 0.7 9.8 0.0 | 20.0 | | 20.7 20.8 20.0 | 20.71 | 21.3 | NO STATE OF THE PARTY OF | | SECOND AND DES | 44 M | 2.71 2 13.0 2 | 3.3 2 3.4 2 3.5 2 | 3.7 2 3.8 2 3.0 2 | 3.0 4.0 4.1 |
| 2. 4 | 10.8 17 | 7.0 | 7.3 | 7.0 | 7.10 | 8.3 | 18.07 | 8.00 | 0.2 0.4 0.5 | 00.00 | 20.0 | 20.2 20.4 20.5 | 20.7 20.8 20.9 | 20.11 21.0 21.1 | 21.4 | | | 2.4 2 | 2.8 2 | 2.71 3.0 3.2 2 | 3.3 2 3.6 2 | 3.7 2 3.8 2 3.0 2 | 35, 2. 2.0 2.2 2.2 | 4.0 |
| 0.334 | 10.10 17 | 10 mg | 7:07 | 7.00 | 345 | 7.80 | 8000 | 0.3 | 0.78 | 0.10 0.11 0.0 0.2 | 10.2 10.3 10.3 10.6 | 20.0 20.7 20.0 20.10 | 20.10 21.0 21.1 21.2 | 21.2 | 21.7 | 22.0 | 2.5 | 2.70 | 3.02 | 3.3 | 3.7 2 3.8 2 3.0 2 3.11 2 | 3,11 2. 4,1 2. 4,2 2. 4,4 2. | 2.32 2.02 2.03 2.03 2.03 2.03 | 4.0 |
| 8. 4 4 | 7:23 | 5078 | 7.10 18 7.11 18 8.0 11 | 8.2 1.3 1.5 | 8.6 8.7 8.8 8.9 | 18.10 | 23,40 | 0.0000 | 0.11 20.0 20.1 20.2 | 20.3 20.5 20.5 | 0.7 0.8 0.9 | 20.11 | 21.3 | 21.8 21.0 21.10 21.11 | 22.0 22.1 22.2 | 22.4 22.5 22.7 22.8 22.8 | 2.8 2 2.10 2 2.11 2 3.0 2 | 3333 | 3.5 3.6 3.7 3.9 2 | 3.0 2 3.0 2 4.0 2 4.1 2 | 4.1 2 2 2 2 2 4.5 2. | 4.5 2. 4.7 2. 4.8 2. 4.9 2. | 4.0 2 4.11 2 5.0 2 5.2 2 | 5.1 |
| 8.6 4 7 4 8 | | | | | B.10 B.11 0.1 | 9.3 | 0.7 0.0 0.0 0.0 0.0 0.0 0.0 | 0.01 | 20.3 | 0.8 | 21.0 | 21.4 | 21.0 | 22./ | 22.5 | 22.02 | 3.2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | 3.0 2 | | 4.2 2222 | | 4.9 2 4.11 2 5.0 2 5.3 2 5.3 2 | 5.3 20 5.3 20 5.5 6 20 5.6 8 20 | 5.7000 |
| 8 8 2 9 4 | | | 3.5 18 3.0 18 3.7 18 3.9 19 | 3.9 kg | 0.3 | 9.0 | 9.10 2 10.11 2 10.2 2 20.3 2 | 0.4 0.5 0.6 0.7 2 | 0.7 | 1.0 | 11.5 | 21.0 | 22.0 22.2 22.3 22.4 22.5 | 22.6 | 22.9 22.10 23.0 | 3.3.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2 | 3.6 2 3.7 2 3.8 2 | | | | 4.11 2. 5.0 2. 5.2 2. | 5.3 2 | 5 0 20 5 0 0 20 5 0 0 20 5 0 0 20 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 5.0 |
| The second second second | | 0 16 | | | 0.0 | 0.0 | | 0.7 2 | 1.02 | 1.5 | 1.6 | 2.2 | 22.5 | 22.0 | 23. + 2 | 3.5 | 4.0 2 | 7.3 2 7.5 2 | 1.8 2 1.9 2 | 4.8 2 4.5,1 2 5.0 2 5.2 2 | 5.0 2 5.3 5.5 2 5.0 2 5.0 2 | 5. 5. 2. 5.08 2.0 5.09 20 5.11 20 | | |
| 9.0 % | 18 1 18 18 18 18 18 18 18 18 18 18 18 18 | 07899 | 0.0 14 | 7.3 14 10.5 16 10.5 16 10.7 2 | 0.7 2 2.8 2 2.10 2 0.0 2 | 0.2 2 | 0. 4 2 10. 5 2 10. 6 2 10. 7 2 | 0.51 2 | 1.3 | 1.00 | 2.0 | | | 22 40 | | | 4.0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | # 50 22 # 80 22 # 80 22 | 6.2 2 | 5.7 2 | | | 20 27 27 | 7000 |
| 2 2 | | 10:00 | 3 50 | 7890 | 0.1 2 2 0.3 2 | | 0.00 2 | | | | 2.50 | | 23.1 23.2 23.4 | - | | Both all thi | | | 5.07 | - | | .9 47 | 0000 | 3.0 |
| 9. 40. W. 40. | 10000 | 5 4 6 to | .7 Kg .8 20 .9 20 .10 20 | 2.0 2 | 0.4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | 0.0 2 | 1.42 | 1.0 222 | 2.0 2 | 2.345 | 2.0 | 30134 | 3.5 | 3.0 | 4 (2 (2 (2 (2 (2 (2 (2 (2 (2 (2 (2 (2 (2 | 7 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 | 5.00 | 5. 4 2 5. 5 2 5. 5 2 5. 8 | 8000 1 2000 1 2000 1 | 20000 | 0.0 20 | 340 37 10 37 13 37 | 3 20 3 | 7000 |
| | (Acade (Inc. of Inc. | | 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | I HE KOL | 11/1/20 | - (K) 11 - 1 | the same | 2 72 % | | 1000 | 1 1 4 2 | | | 2- 3-1 | NE ANNUAL TO MA | 1 | | ACCOMPANIES | AND DESCRIPTIONS | mer in | winter da | | | Service a |

| Leave success | | from | g foot 4 | inch | es ar | nd a | by s | foot | and | ź an | inci | r to | 12 ft | rot b | inci | res l | 431 | oot. | | 類似 | |
|---------------------------------------|--|--|--|----------------------------------|--------------------------------|--|--|--|---|--------------------------------|--------------------------------|----------------------------------|------------------------------|--------------------------------|--|--------------------------------|--------------------------------|--------------------------------|--------------------------------|-------------------------------|-------------------------------|
| | F.I F | FI | F.1 F.1 | F.I | F.I | F.1 1 | F.I F | I F.I | F.I | F.I | F.I | F.I | F.I | F.1 | F.I | F.I | F.I | F. 1 | F.I | F.I | F.I |
| F.I.Part | 2.02 2. | 2.12 | 2.2 2.2 | 2 2 3 | 2.35 | 2.4 2 | 1.45 2. | 5 2.52 | 2-6 | 265 | 2.7 | 2.72 | 2.8 | 2.8 2 | 2.9 | 2 92 | 2.10 | 2 10 2 | 2.11 | 2.11 2 | 3.0 |
| 9.43 | 83% | 20.0 | 0. 5 20.1 | 21.3 | 21.7 | 22.0 | 2.3 2.4 2.0 2.0 2.7 2.7 | 0 23.2 | 33.35 33.35 33.35 33.35 33.35 33.35 33.35 33.35 33.35 33.35 33.35 33.35 33.35 33.35 33.35 33.35 33.35 33.35 33.35 34.35 36 34.35 34.35 34.35 34.35 34.35 34.35 34.35 34.35 34.35 34.35 34. | 23.11 | 24.3 24.4 24.5 24.0 | 24.7 | 15.1 | 25.5 | 25.9 | 20:3 | 20.7 20.8 20.10 | 27.1 | 27.0 | 27.00 | 28.3 |
| 6 | 10.5 10. | 20.2 2 | 0.7 21.0 | 21.4 | 21.0 | 22.2 2 | 2.7 22 | 1 23.4 | 23.8 | 24.2 | 24.6 | 24.11 | 25.4 | 25.9 | 20.1 | 26.6 | 20.11 | 27.4 | 27.8 | 28.1 | 28.0 |
| 3.5 | 8.8 % | 20.5 | 0.00 21.3 | 21.8 | 22.0 | 22.4 | 2 8 23 210 23 | 2 23.7 | 23.11 | 24.0 | 24.0 24.10 | 25.2 25.3 | 25.8 | 26.1 | 20. d 20. 6 | 20.10 20.10 | 27.2 | 27.7 | 27.11 | 28.4 28.6 | 28.70 |
| 285 | 19.10 20. | 2 20.8 2 | 1.0 21.4 | 21.10 | 22.3 | 22.7 2 | 3.1 23 | 6 92 11 | 24.2 | 24.7 | 25.1 | 25.6 | 25.11 | 26.2 26.4 | 26.8 | 27.0 | 27.5 27.6 | 27.9 | 28.2 28.4 | 28.7 28.0 | 20.1 |
| 9 5 | 20.0 20. | 20.02 | 1. 3 21. | 22.0 | 22.4 | 22.00 22.10 22.11 22.11 | 3.2 3.3 3.4 23 3.4 | 7 24.0 8 24.1 0 24.2 | 24.6 24.0 24.7 | 24.0 | 25.2 25.4 25.5 | 25.7 25.8 25.10 | 26.0 26.1 26.3 | 26. 5 26. 0 | 26.10 | 27.3 | 27.7 | 28.0 | 23.5 | 28.10 29.0 | 20.3 |
| 0.10 % | 20.7 20. | 21.02 | 1.5, 21.1 | 22.7 | 22.8 | 23.02 | 3.4 23 | 10 24.9 | 24.8 | 25.1 | 25.0 | 25.11 | 20.3 | 20.8 20.9 | 27.2 | 27.7 | 28.0 | 28.5 | 28.10 | 29.3 | 29.7 |
| 115 | 20.3 20.4 20.4 20.4 20.5 20.7 | 21.22 | 1.7 22.6 | 22.5 | 22.70 | 23.3 | 3. 7 24 | 24.5 | 24.9 | 35.2 | 25.7 | 20,0 20,2 20,3 | 20.5 | 20.10 27.0 | 27.3 | 27.8 | 28.1 28.3 | 28.0 28.8 28.8 | 20.1 | 20.6 20.6 | 20.0 20.10 |
| 10.0 2 | 20.0 20.1 | 21.42 | 1 0 22 | 2227 | 23.0 | 23.5 | 3.10 24 | .3 24.8 | 25.1 | 25.0 | 25.11 | 26.4 | 26.9 | 27.2 | 27. 7 | 28.0 | 28.5 | 28.10 | 29.3 | 29.8 | 30.1 |
| 1 2 | 20.8 21. | 21.7 2 | 1.10 22 3 | 22.8 22.70 | 23.4 | 23.7 2 | 4.2 24 | 7 25.0 | 25.4 | 25.70 | 26.3 | 20. 7 20. 8 | 27.0 | 27. 5 27. 6 | 27:10 | 28.3 28.5 | 29.10 | 20.3 | 20.0 | 20.11 | 30.0 |
| 10.2 2 | 20.10 21. | 21.8 2 | 2.1 22.7 | | | 23.10 2 | 4.3 24 | 8 25.0 | 25.0 | 25.11 | 20.4 | 26.10 26.11 | 27. 3 | 27.8 | 28.1 | 28.6 | 28.11 | 20.4 | 20.0 | 30.2 | 30.7 |
| 3 5 | 21.0 21. | 21.50 21.50 21.50 21.11 | 2 1 22 2 2 2 22 3 2 4 22 4 2 5 22 4 | | 23.6 | 24.0 | 4.5 24 | 0 25.5 | 25.00 | 26.2 26.3 | 26.8 | 27.0 | 27.5 | 27.10 28.0 | 28.4 | 28.70 28.70 | 20.2 | 20.7 | 30.0 | 30.5 | 30.10 |
| 10.4 2 | 21. 3 21. | 22.1 | 2.0 22.1 | 23.4 | 23.0 | 24.2 2 | 4.8 25 | 2 25.7 | 25.11 | 20.4 | 26.10 26.11 | 27.3 | 27.8 | 28.3 | 28.6 28.8 | 20.0 | 20.5 | 20.10 | 30.3 | 30.8 | 31.1 |
| 35 | 21.5 21.7 | AND STREET, AND SEC. | 2.7 23.0 2.8 23.1 2.9 23.1 | 23.0 | 24.1 | 24.5 | 4.10 25 | 2 25.7 25.8 4 25.8 | 26.2 | 26.8 | 27.0 | 27.5 | 28.0 | 28.4 28.5 | 28:50 | 29.4 | 29.8 | 30.2 | 30.0 | 30.11 | 31.6 |
| 10.6 2 | 21. 0 22. 21. 8 22. 21. 8 22. | 22.5 22.6 22.7 22.8 22.8 | 2.10 23. 2.11 23. 3.0 23. 3.1 23. | 23.0 | 24.2 | 24.7 24.8 | 5.0 25 | 7 20.0 | 20.4 | 20.10 | 27.3 | 27.8 | 28.3 | 28.7 28.8 | 20.0 | 20.5 | 20.10 30.0 | 30.4 | 30.10 | 31.4 | 31.7 |
| 8 | 21.9. 22. | 22.8 2 | 3.0 23.0 | | 24.4 24.5 | 24.11 | 5. 3 25 | 9 26.3 | 26.8 | 27.1 | 27.7 | 28.0 | 28.5 | 28.11 | 29.4 | 29.9 | 30.1 | 30.8 30.0 | 31.1 | 31.7 | 32.0 |
| 10.8 5 | 21.10 22.1 | 22.0 22.10 22.11 23.0 | 3 9 23 8 3 5 23 7 | 24.2 | 24.0 24.8 24.0 | 25.1 | 2 0 20 5 0 20 | 0 20. | 26.10 | 27.4 | 27.0 | 28.3 28.5 28.5 | 28.8 | 20.1 | 20.0 | 30.0 30.2 30.3 | 30.5 30.7 30.8 | 30.11 | 31.6 | 31.10 | 32.3 |
| 10 | 22.7 22. | 23.02 | 3.6 23.1 | 24.4 | 24.10 | 25.3 2 | 5.9 20 | 2 26.8 | 27.1 | 27.0 | 28.0 | | 28.11 | 20.4 | 29.9 | | | | 31.7 | 32.1 | 32.0 |
| 10.10 5 | 22.3 22.7 | 3 23 2 2 0 23 3 2 | 3 8 24 | 24.7 | 25.0 | 25.0 | 7.11 20 0.0 20 | 3 20 k | 27.3 | 27.70 | 28.2 28.4 | 28.7 28.9 28.10 28.10 | 29.3 | 20.7 29.8 | 30-0 30-2 30-3 | 30.6 30.7 30.8 | 30.10 30.11 31.1 31.2 | 31.5 | 31.10 32.0 32.1 | 32.4 32.5 32.0 | 32.0 |
| 11.0 2 | 22.5 22.1 | 23.4 2 | 3.10 24.3 | 24.9 | 25.2 | 25.8 2 25.0 2 | 6.3 26 | .7 27.0 | 27.7 | 27.11 | 28.5 28.6 | | 29.4 | | | | 31.3 | | | 32.8 | 33.1 |
| 1 5 | 22.8 23. | 23.7 2 23.8 2 23.8 2 | 4.0 24.0 4.1 24.0 | 24.10 | 25.5 | 7510 2 2511 | 0.5 20 | 9 27. | 27.80 | 28.2 | 28.8 28.0 | 20.0134 | 20.78 | 30.0 | 30.4 30.6 30.7 | 30.11 | 31.5 | 31.10 | 32.2 32.4 32.5 32.7 | 32.0 32.11 33.0 | 33.3 |
| 11.2 2 | 22.// 23.4 | | -700 | 25.3 | 25.8 | 26,2 2 | 26.7 27 | 1 27.7 | 28.0 | 28.6 | 28.11 | | - | 0-10-Table | SPECIAL PROPERTY. | - | PRINCEPT. | | - | _ | 33.7 |
| 3 4 | 22 // 23 23 0 23 23 1 23 23 2 23 | 23.10 23.11 24.0 24.1 24.1 | 4.3 24.6 4.4 24.6 4.0 24.1 4.7 25.0 | 25.5 | 25.8 25.0 25.11 26.0 | 20.3 20.5 20.5 | 0.0 27 0.00 27 0.11 27 | 2 27.6 | 28.3 | 28.7 28.8 28.10 | 28.11 20.2 29.3 | 20.50 20.00 20.00 20.00 | 30.0 | 30.4 30.6 30.7 30.8 | 30.11 31.0 31.2 | 31.508 | 31.10 32.0 32.1 | 32.3 32.4 32.6 32.7 | 32.8 32.10 32.11 33.1 | 33.3 33.50 33.50 | 33.7 33.10 33.10 |
| 11.4 5 | 23.3 23.8 | | | 25.7 | 26.1 | 20.0 2 | | | | 28.11 | 29.5 | 29.10 | 30.4 | | | 31.0 | 32.3 | 32.8 | 33.2 | 33.8 | 34.1 |
| 35 \$ | 23.3 23.4 23.4 23.5 23.7 23.7 23.7 23.7 | 24.2 24.3 24.4 24.5 24.5 2 | 4.8 25.1 4.0 25.3 4.10 25.3 4.11 25.3 | 25.7 25.0 25.0 25.0 | 26.1 26.2 26.3 26.4 | 20.0 20.0 20.0 20.0 20.0 | 7.0 27 7.1 27 7.3 27 7.4 27 | | 28.5680 28.8880 28.8880 | | 20.56 20.78 20.78 | 29.10 30.0 30.1 30.2 | 30.4 30.5 30.7 30.8 | 30.10 30.11 31.0 31.2 | 31.3507 | 31.00 | 32.3 32.6 32.6 32.7 | 32.8 32.10 32.11 33.1 | 33.4 33.5 33.5 | 33.11 | 34.1 34.3 34.4 34.0 |
| 11.6.5 | 23.7 24. | 24.0 2 | 5.0 25.0 | 26.0 | 26.5 | 26.11 2 | 7.5 27 | .0 28.4 | 28.10 | 20.4 20.5 20.7 20.8 | 20.10 20.11 30.0 30.2 | 30.4 30.5 30.6 30.7 | 30.0 30.1 31.0 | 31.3 | 31.10 31.10 32.0 32.1 | 32.3 32.4 32.5 32.7 | 32.8 32.10 32.11 33.1 | 39.2 33.4 33.50 | 33.8 | 34.2 34.3 34.5 34.6 | 34.7 34.0 34.0 35.0 |
| · · · · · · · · · · · · · · · · · · · | 23.7 24. 23.0 24. 23.0 24. 23.0 24. | 24.0 24.7 24.8 24.8 24.9 2 | 5.0 25.7 5.1 25.7 5.3 25.8 5.3 25.8 | 26.0 26.1 26.2 26.3 | 26.5 26.7 26.8 26.9 | 26.11 27.0 27.1 27.3 | 7.5 27 7.6 28 7.7 28 7.8 28 | 2 28.8 | 28.10 28.11 20.1 20.2 | 29.8 | 30.0 30.2 | 30.0 | 31.1 | 31.7 | 32.1 | 32.5 | 33.1 | 33.0 | 34.0 | 34.0 | 35.0 |
| 11.8 2 | 23.// 24 24.0 24 24.1 24 24.2 24.8 | | STREET PROPERTY | 20.4 20.5 20.7 | 26.10 26.11 27.0 27.1 | 27.4 27.5 27.6 27.7 | 7.10 28 8.0 28 8.1 28 | 4 28 0 28 0 28 0 29 0 7 29 0 | 20.3 20.6 20.6 20.7 | 20.00 20.10 30.0 30.1 | 30.3 30.6 30.7 | 30.0 30.10 30.11 | 31.3 | 31.90 | 32.2 32.4 32.5 32.6 | 32.8 32.10 32.11 33.0 | 33.3 | 33.8 | 34.2 34.3 34.5 34.0 | 34.8 34.9 34.11 35.0 | 35.1 35.3 35.6 35.6 |
| 94 | 24. 2 24. | 25.2 2 | | | 27.0 | 27.7 | 8:0 28 | 7 39.9 | 29.7 | 30.1 | 30.7 | 31.1 | 31.7 | 32.1 | 32.6 | 33.0 | 33.6 | 34.0 | 34.6 | 35.0 | 35.6 |
| 11.10 2 | 24.3 24.1 24.5 24.1 24.5 25.0 | 25.3 25.5 25.5 25.6 | 5.0 26.4 5.10 26.4 6.0 26.6 | 26.0 26.10 26.11 27.0 | 27.3 27.5 27.5 27.6 | 27:80 27:10 27:11 28:0 | 8.2 28 8.4 28 8.5 28 8.6 29 | 8 20. 20. 10 20. 10 20. | 20.8 20.8 20.0 20.0 | 30.2 30.3 30.5 30.6 | 30.8 | 31.2 31.3 31.56 | 31.8 | 32.3 | 32.0 | 33.3 | 33.8 33.9 33.11 34.0 | 34.3 | 34.0 | 35.1 35.3 35.6 35.6 | 35.7 35.0 35.10 36.0 |
| 12.0 | 24.6 25.0 | 23:8 2 | | 27.0 | 27.6 | 28.0 | 862 | 0 20.0 | 30.0 | 30.6 | 31.0 | 31.6 | 32.0 | 32.6 | 33.0 | 33.6 | 34.0 | 34.0 | 35.0 | 35.0 | 36.0 |
| 12.05 | 24.7 25. 24.8 25. 24.0 25. 24.0 25. | 25.7 25.8 25.0 25.0 25.0 25.0 | 6 1 26.7 6 2 26.8 6 3 26.6 6 4 26.6 | 27. 1 27. 2 27. 3 27. 3 | 27.7 27.8 27.9 27.11 | 28.1 28.2 28.3 28.5 | 8.7 20 8.8 20 8.0 20 8.11 20 | 1 20.5 2 20.5 4 20.6 5 20.1 | 30.1 30.2 30.4 30.5 | 30.7 30.0 30.10 30.11 | 31.1 31.3 31.4 31.5 | 31.7 31.90 31.10 | 32.1 32.3 32.4 32.5 | 32.7 32.0 32.10 32.11 | 33333333333333333333333333333333333333 | 33.70 33.70 34.0 | 34.1 34.3 34.4 34.6 | 34.0 | 35.1 35.3 35.4 35.6 | 35.7 95.0 35.10 36.0 | 36.1 36.3 36.4 36.6 |
| 2 | 24.10 25 | 25.10 2 | 6. 4 26.10 | 27.4 | 27.11 | 28.5 2 | 8.11 29 | 6 201 | 30.5 | 30.11 | 31.5 | 32.1 | 32.5 | 33.1 | 33.5 | 34.1 | 34.0 34.7 | 35.0 | 35.7 | 30.0 | 36.7 |
| 12.2 2 | 24.11 25.0 25.0 25.0 25.1 25.0 25.2 25.0 | 25.11 26.0 26.1 26.2 20.2 | 6. 5 27. 6 6. 8 27. 6 6. 8 27. 9 | 27. 6 27. 8 27. 8 27. 8 | 28.0 28.1 28.3 28.3 | 28.6 28.7 28.8 28.9 28.9 | 9.0 20 9.1 29 9.3 29 | 0 30.0 7 30.0 30.4 | 30.0 30.7 30.0 30.10 | 31.0 31.3 31.4 | 31.6 31.8 31.10 | 32.1 32.2 32.3 32.4 | 32.8 | 33.1 33.3 33.5 33.5 | 33.7 33.8 33.10 33.11 | 34.4 | 34.7 34.8 34.10 34.11 | 35.3 | 35.0 | 30.1 30.3 30.4 30.6 | 36.7 36.0 36.10 37.0 |
| - ' | 25.2 25. | 26.4 2 | 6.10 27. 4 | 27.0 | 28.3 28.4 | 28.9 2 28.10 2 | 9.3 29 | 11 30.4 | 30.10 | 31.4 | 32.0 | 32.6 | 33.0 | 33.6 | 34.0 | 34.7 | 35.1 | 35.7 | 30.1 | 36.7 | 37.1 |
| 12.4 \$ 55 \$ | 25 3 25 3 25 4 25 3 25 5 25 6 | 26.4 26.5 26.0 26.7 26.7 | 6.10 27.4 6.11 27.5 7.0 27.6 7.1 27.7 | 27.10 27.11 28.0 28.1 | 28.4 28.5 28.7 28.8 | 28.10 2 20.0 2 20.1 2 20.2 2 | 0 5 20 0 6 30 0 7 30 9 8 30 | 0 30.6 0 30.6 1 30.8 2 30.6 | 30.11 | 31.5 | 32.0 32.1 32.2 32.3 | 32.6 32.7 32.8 32.10 | 33.0 33.3 33.4 | 33.6 33.8 33.0 33.0 | 34.0 34.2 34.3 34.4 | 34.7 34.8 34.0 34.0 | 35.4 | 35.60 | 36.4 | 30.10 | 37.1 37.3 37.0 |
| 0 | 25.0 26.0 | 20.7 2 | | | 28.8 | 20.2 | 4.8 30 | | 37.3 | 2.9 | | | 5 | 3 | É | 1 | 7.7.1 | ~ 1 | | | ,, - |
| * N. S. C. S. S. C. C. C. | 1 1 | | Mar | J. HAR | 1 | The state of the s | -6 | The state of the s | W HILLIAM W | 1 | Charles | | N. C. | LA | NA | | | | | | |



| 1 14 14 1 | F.I | F.I | F.I | F.I | F. | I | F.I | F.I | F. I | F.I | F.I | F.I | F.I | F.I | F.I | F.I | F.I | F.I | F.I | F.I | | | F. I | | |
|-----------------|-------|-------|-------|-------|----------|-------|--------|------------------------------|----------|--------------------------------|----------|-------|----------|-------|-------|------------|-----------------------|-------|-------|-------|-------|----------------------|---------------|-------|-------|
| LParts | | _ | 3.12 | 3.2 | 3.2 | 2 2 | 3.3 | 3.32 | 3.4 | 3.4 2 | 3.5 | 3.5 2 | 3.6 | 3.62 | 3.7 | 3.72 | 3.8 | 3.82 | 3.9 | 3.9 4 | 3.10 | 3.10 2 | 3.11 | 3.112 | 4. |
| 0 5 | 0000 | 9.68 | 9.91 | | | | | | | | | | | | | | | | | | | | | | |
| # 100 m | 9.9 | 0.000 | 10.02 | 10.3 | 10000 | 4578 | 0.780 | 10.10 | 11.1 | | · | | | | | | 105 - 7 - 1 10 - 3 | | | | | de a | | | |
| 4550 | 10.3 | 10.5 | 10.78 | 10.10 | 10. | 10013 | 11.0 | 11.356 | 11.35.08 | 11.50 | 11:30 | 12.0 | 12.3 | | | | | * - | | | | | | | |
| 6 1 7 1 8 | 10.0 | 10.11 | 11.12 | 11.3 | 11: | | 1.0 | 11.80 | 11.10 | 112.3 | 12.19.50 | 12.3 | 12.5080 | 12.7 | 12.10 | 13.3 | 13.5 | | | | | | | | |
| 8 1. 9 1. | 11.35 | 11.5 | 11.70 | 11.00 | 12. | 1001 | 2.12.2 | 12.2 12.4 12.6 12.7 | 12.000 | 12.6 12.8 12.10 12.11 | 12.80 | 13.10 | 13.35 | 13.35 | 3579 | ろうり | 13.70 | 13.9, | 1444 | 14.5 | 14.8 | | | | |
| のなり | 11.0 | 11:11 | 12.3 | 12.9 | 12.12.12 | 57,80 | 270 | 12.01 | 12.11 | 13/3/8 | 13,370,8 | 19.57 | 13.78.00 | 13.90 | 13.11 | 14.12 14.6 | 14.408 | 440 | 44450 | 4455 | 14.00 | 15.0 15.4 15.6 | 15.60 15.8 | 15.80 | 16 |
| 0 5 | 12.4 | 12.0 | 12.8 | 12.14 | 经 | 013 | 3000 | 13.5 | 13.0 | 13.8 | 13.10 | 14.0 | 4.9 | 14.00 | 14.8 | 14.80 | 14.10 | 经是 | 5555 | 55.50 | 15.00 | 5500 | 15:18 | 10.02 | 56.66 |

A TABLE OF FEET AND INCHES from 4 foot 2 inches and a \$ by 3 foot and \$ an inch to 9 foot 2 inches by 4 foot.

| | FIFIEI | Fil | F.I F.I | F.I.F. | (F.I | F.I | F.I | F.I | F.I | F.I | F.I | F.I | F.I | F.I | F.I | F.I | F.I | F.I | F.I | F.1 |
|-----------|--|----------------------------------|---|---|------------------------------|--------------------------------------|-----------------------------|-------------|-----------------------|------------------------------|-----------------------|-------------------------|------------------------------|-------------------------|---|--------------------------|---------------------------|------------------------------|-----------------------|-----------------------|
| F. I. Par | ts 3.02 3.1 3.1 | 232 | 3.22 3.31 | 3.32 3. | 3.45 | 3.5 | 3 55 | 3.6 | 3.65 | 3.7 | 3.75 | 3.8 | 3.82 | 39 | 3.92 | 3.10 | 3-10 | 3.11 | 3 112 | 4.0 |
| 4.2 5 | 12.10 13.0 19.5 | 333 | 3.6 13.8 | 13.10 14. | 0 14.2 | 14.6 | 4.7 | 4.00 | 15.2 | 15.3 | 15.3 | 30 | 15.71 | 3000 | 36.3 | 10.3 | 0000 | 1000 | 10.10 | 17.0 |
| 4.4 5 | 13.2 /3.4 /3.0 | 3 13.10 | 4.0 14.3 | 14.5 14 | 7 14.9 | 14.11 | 15.2 | 19.4 | 15.0 | 15.90 | 15.10 | 16.0 | 10.3 | 16.3 | 16.7 | 10:91 | 16.11 | 17:2 | 7.8 | 7.0 |
| 35 | 13.7 13.9 13.1 | 14.3 | 4.4.6 | 14.8 14. | 0 13.1 | 15.3 | 15.5 | 15.3 | 15.0 | 10.1 | 10. 4 | 10.0 | 10.0 | 10.90 | 17.0 | 17.3 | 17.7 | 7.7 | 17.10 | 18.0 |
| 7 5 | 13.11 14.2 14.4 | 14.8 | 4.10 15.0 | 15.3 | 3 13.6 | 15.80 | 15,00 | 10.0 | 10.3 | 10.5 | 10.7 | 10.10 | 7.0 | 77.0 | 17:3 | 77 | 17.91 | 731 | 2 40 | \$ \$60 B |
| 4.8 % | 14.4 14.0 14.9 | 14.11 | 5.1 15.4 | 15.0 15. | 8 15.0 | 10:1 | 10.3 | 10.0 | 10.8 | 16.11 | 17:3 | 7:3 | 7.0 | 7.80 | 7.9 | 18.2 | 18.3 | 18:5 | 18.8 | 18.10 |
| 4.10 % | 14.8 14.11 15.1 | 15.4 | 5.6 15.8 | 15.71 10. | 3 10.6 | 16.8 | 16.0 | 16.11 | 17.3 | 17.0 | 17.8 | 17.10 | 17.11 | 18.3 | 18.3 | 18.8 | 18.11 | 19.1 | 19.4 | 19.4 |
| 11/2 | 15.1 15.3 15.0 | 15.7 | 5.0 10.0 | 10. 2 16. | 5 16.6 | 16:10 | 7.02 | 77.8 | 7.5 | 7.3 | 7.10 | 8.4 | (8:3 18:3 18:3 | 18.5 | 18:3 | 10.00 | 10:3 | 90.3 | 9.389 | 10.8 20.0 |
| 5.0 % | 15. 6 15. 7 15. 9 | 16.0 | 6.2 10.5 | 16.7 16. | 0 17.0 | 7.3 | 17.5 | 7.8 | 17.10 | 18.1 | 18.3 | 18.6 | 18.8 | 18.11 | 10.0 | 10.4 | 10.0 | 10.0 | 20.1 | 20.2 20.4 20.8 |
| 5.24 | 15.0 15.11 10.2 | 16.4 | 0.9 10.11 | 17.0 17. | 3 17.5 | 17.10 | 17.11 | 18.3 | 18.4 | 18.8 | 18.11 | 19.11 | 10.4 | 19.0 | 19.8 | 20.0 | 20.2 | 20.3 | 20.5 | 20.10 |
| 33 4 | 10.1 10.4 10.0 | 10:70 | 7.0 7.2 | 7.3 7.7 | 8 72.10 | 8.3 | 18.4 | 8.6 | 18:00 | 18.0 | 10.2 | 10.3 | 10:30 | 10.10 | 20.0 | 20.3 20.5 | 20.0 20.8 | 20.9 | 20.11 | 21.2 |
| 5.4 5 | 10.4 10.7 10.10 | 77.0 | 7.3 17.6 | 7.8 77.8 | 18.33 | 18.508 | 18.7 | 18.10 | 10.2 | 00.7 | 0.00 | 0.00 | 20.3 | 20.4 20.6 | 20.6 20.7 20.7 | 20.0 | 21.0 | 21.3 | 21.7 | 21.60 |
| 5.6 4 | 10.19 17.1 17.2 | 17.3 1 | 7.8 17.10 | 18.3 18. | 0 18.8 | 19.0 | 19.0 | 19.3 | 19.8 | 19.10 | 20.1 20.3 | 20.4 | 20.5 20.7 20.8 | 20.0 | 20.11 | 21.3 | 21.0 | 21.8 | 21.4 | 22.2 |
| 8 5 | 17.3 77.8 17.8 | 77:10 15 | 8:2 18:3 | 18.8 18. | 18.0 | 19.3 | 19.5 | 19.80 | 20.1 | 20.4 | 20.5 | 20.7 | 20.10 | 21:3 | 21.3 | 31.3 | 22.0 | 22.2 | 22.3 | 22.0 22.8 |
| 5.80 5 | 7. 0 7.0 18.0 | 18: 2 18 | 18.80 | 10.1 | 10.75 | 10.00 | 10.0 | 20.1 | 20.4 20.6 20.8 | 20.7 20.9 20.11 | 20.10 21.0 21.2 | 21.3 | 21.6 | 21.70 | 21.10 | 22.0 22.2 22.4 | 22.2 22.5 22.7 | 22.8 22.8 22.10 | 22.71 | 23.0 23.2 23.4 |
| 5.10 % | 17.10 18.1 18.4 | 18:3 18 | 3.10 10.1 | 19. 4 19. | 10.10 | 20.1 | 20.4 | 20.7 | 20.10 | 21.1 | 21.4 | 21.0 | 21.0 | 22.0 | 22.3 | 22.8 | 22.9 | 23.0 | 23.3 | 23.6 |
| 6.0 \$ | 18.3 18.0 18.9 | 19.0 19 | 2.5 10.8 | 19.9 20. | 20.3 | 20.6 | 20.9 | 21.0 | 21.3 | 21.6 | 21.0 | 22.0 | 22.3 22.5 | 22.6 22.8 | 22.0 | 23.0 23.2 | 23.3 23.5 | 23.6 23.8 | 23.9 23.11 | 24.2 |
| 1 4 | 8.8 8.0 10.2 | 10.3 10 | 0.0 | 20. 0 20. 20. 2 20. 20. 4 20. | 20.6 20.8 20.10 | 20.0 | 21.0 | 21.3 | 21.7 21.3 21.10 | 21.10 | 22.1 22.2 22.4 | 22.4 | 22.7 22.0 22.0 | 22.10 23.0 23.1 | 23.3 | 233.8 23.8 | 23.7 | 23.10 24.0 24.2 | 24.3 24.5 | 24.6 24.6 24.8 |
| 8.2 5 | 18.11 10.2 10.5 | 10.8 20 | 0.11 20.2 | 20.5 20. 20.7 20. | 20.11 | 21.3 | 21.6 | 21.10 | 22.0 22.2 23.4 | 22.3 22.5 22.7 | 22.6 22.8 22.6 | 22.0 | 23.0 23.2 23.4 | 23.3 | 23.6 23.8 23.10 | 23.10 | 24.9 | 24.4 24.6 24.8 24.8 | 24.7 | 24.10 25.0 25.2 |
| 6.4 2 | 18:3 19:8 19:3 | 20.1 20 20.2 20 20.4 20 | | 20.10 21. | | | | | | | | 23.3 23.4 23.6 | 23.8 23.60 | 23.11 | 24.2 24.4 24.4 | 24.5 24.7 | 24.8 24.90 | 25.0 25.2 | 25.3 25.5 | 25.6 25.8 |
| 0.6 \$ | 10.8 10.11 20.2 20.4 | TO SHARE MANAGEMENT AND ADDRESS. | 0.10 21.1 | | | | 22.6 | 22.0 | 23.0 23.2 | 23.3 23.5 | 23.7 23.9 | 23.10 24.0 | 24.3 | 24.4 24.6 | 24.8 24.10 | 35.1 | 25. 2 25. 4 | 25.7 25.7 | 25.0 | 26.0 |
| 7 5 | 20.2 20.5 20.8 20.3 20.7 20.10 | | | | 22.6 | | 23.1 | | 23.6 23.6 23.7 | 23.70 | 23.10 24.0 24.2 | 24.3 24.5 | 24.0 | 24.00 25.0 | 25.3 | 35.3 25.3 | 25.B 25.60 | 2531 | 20.3 20.5 | 20.0 |
| 6.84 | 20.5 20.8 21.0 20.0 20.0 21.1 20.8 20.11 21.3 20.0 21.1 21.4 | 21.4 2 | 1.8 21.11 | 22.3 22. | 22.9 | 23.4 | 3 5 | 3.2 | 23.11 | 24.2 24.4 24.6 | 24.6 | 24.0 | 25.0 25.2 25.4 | 25.4 25.6 25.7 | 25.7 | 25/0 20.0 20.2 | 26. 2 26. 4 20. 6 | 26.5 26.7 26.9 | 20.0 20.11 27.1 | 27.0 27.2 27.4 |
| 6.10 % | 20.11 21.2 21.0 | 21.0 2 | 2.1 22.4 | 22.8 22.1 22.0 23. | 23.4 | 23.6 | 23.0 | 24.1 | 24.4 24.6 24.8 | 24.8 24.0 24.11 | 24.11 25.1 25.3 | 25.2 25.8 25.8 | 25.0 25.8 25.80 | 25.0 | 26.1 26.3 26.5 | 26.4 26.6 26.8 | 26.8 26.10 27.0 | 20.11 | 27.3 | 27.6 |
| 7.0 % | 21. 3 21.7 21.10 | 22.4 22 | | 23.0 23.4 23.2 23.6 23.4 23. | | 24.1 24.1 24.2 | 24.2 2 24.4 2 24.0 2 | 24.8 | 24.11 25.1 | 25.3 25.5 | 25.6 25.8 | 25.10 25.00 | 26.1 | 26.5 | 26.8 26.10 | 27.0 27.2 | 27.3 27.5 | 27.7 27.9 | 27.10 28.0 | 28.2 28.3 |
| 2 2 | 21.6 22.0 22.3 22.5 | 22.8 2 | 23.2 | 23.4 23.9 | 24.1 | 24.6 | 24.8 g 24.8 g | 25.1 | 25.3 25.3 | 25.0 25.8 | 25.10 | 26.3 | 26.7 | 20.0 | 27.0 | 27. d 27. d | 27.7 | 27.77 28.7 | 28.7 28.4 28.7 | 28.3 28.8 |
| 7.25 | 22.1 22.4 22.8 22.2 22.0 22.0 22.4 22.7 22.7 | 22.11 23 | 23.7 | 23.10 24 24.0 24 24.2 24 | 24.5 24.7 24.8 | 24.8 24.71 25.1 | 5.3 | 5558 | 15.8 15.00 16.0 | 26.0 26.2 26.3 | 26.3 26.5 26.6 | 26.7 | 26.11 27.0 27.2 | 27. 2 27. 4 27. 6 | 27.6 27.8 27.10 | 27.0 27.11 28.1 | 28.3 28.3 28.5 | 28.5 28.9 | 28.8 28.0 29.0 | 20.0 20.2 20.4 |
| 7.4 1 | 22.5 23.0 23.2 22.7 23.0 23.2 22.8 23.0 23.4 | 23.4 23.6 23.7 | 3.8 24.0 3.10 24.1 3.11 24.3 | 24.3 24. 24.3 24.6 24.7 24.6 | 24.11 25.0 25.2 | 25.2 25.4 25.0 | 15.6 2 15.8 2 15.10 2 | 15.10 | 26.3 | 26.5 26.7 26.9 | 26.9 26.11 27.0 | 27. Q 27. 2 27. 4 | 27. 6 27. 6 27. 8 | 27-8 27-80 28-0 | 28.0 29.1 28.3 | 28.3 28.7 28.7 | 28.7 | 28.11 | 20.2 20.6 20.6 | 20.0 20.0 20.0 |
| 7.6 % | 22.70 23.1 23.5 22.11 23.3 23.7 23.1 23.3 23.8 | 23.0 24 | 2 24.4 2 2 24.6 4.4 24.8 | 24.8 25.0 24.10 25.3 25.0 25.3 | 25.5 25.5 | 25. 0 2 25. 0 2 25. 7 1 2 | 0.3 | 0.5 | 26.0 | 27.0 | 7.0 | 27.0 27.8 27.10 | 28.0 | 28.3 28.2 | 28.7 28.9 | 28.11 | 20.3 | 20.6 | 20.10 | 30.4 |
| 7. 8 4 | 23.2 23.0 23.10 23.4 23.8 23.11 23.5 23.9 24.1 | 24.3 24 | 1.0 25.1 | 25. 4 25.8 | 25.10 | 20.4 | 0.6 2 | 7.0 | 27.3 | 27. 6 | 7.9 | 28.3 | 28.7 28.7 | 28.9 | 29.1 | 29.7 | 20.10 | 30.0 | 30.4 | 30.10 30.10 |
| 9 \$ | 23.7 23.1 24.3 23.8 24.0 24.4 23.10 24.2 24.0 | 24.0 24 | 5.0 25.4 5.2 25.5 | 25.8 26.0 25.9 26.0 | 20.4 20.5 | 26.7 26.9 | 0.10 0.11 2.1 2.1 | 7.3 | 27.0 | 28.1 | 28.3 28.5 | 8.9 | 28.11 | 20.3 | 29.7 | 30.0 | 30. 2 30. 4 | 30.6 30.8 | 30.10 | 31.2 |
| 7.10 % | 23.11 24.3 24.7 24.1 24.5 24.0 24.2 24.6 24.10 24.4 24.8 25.0 | 25.1 24 | 3 35 7 | 20:0 20:1 20:1 26:1 20:2 20:0 | 20.7 20.0 20.10 | 27.1 | 7.5 2 | 7.8 | 27.11 | 8.0 | 8.8 28.50 | 19.0 | 20.0 | 2000 | 30.0 30.2 30.4 | 30.0 | 30.30 | 31.0 | 31.00 | 31.80 |
| 8.0 5 | 24.0 24.0 25.2 24.7 24.0 25.3 | 25.6 25 25.7 25 | 5.10 26.2 | 26.6 26M 26.7 26M | 27.2 | 27. 6 2 27. 7 2 | 7.8 2 7.10 2 7.11 2 | 8.2 | 28.6 | 28.10 | 20.2 | 20.6 | 20.10 | 30.2 | 30.0 30.8 | 30.10 | 31.4 | 31.6 | 31.10 | 32.2 32.4 32.6 |
| 8.2 5 | 24.0 25.1 25.5 24.10 25.2 25.6 25.0 25.4 25.8 | 25.10 20 | 6.2 26.6 24 26.8 | 27.0 27. | 27.5 | 28.1 2 | 8.3 2 | 8.9 | 28.11 | 29.5 | 20.7 20.0 | 30.1 | 30.3 30.5 | 30.7 | 31.0 | 31.4 | 31.10 | 32.0 | 32.4 32.6 | 32.8 32.10 |
| 8.2 \$ \$ | 25.0 25.4 25.8 25.3 25.5 25.0 25.4 25.8 26.0 | 20.3 20.3 20.5 | 6.9 27.1 | 27. 2 27. 4 27. 5 27. 5 | 28.0 28.0 28.1 | 28.2 28.4 28.6 2 | 8.8 8.10 | 8.00 9.2 | 10.6 | 19.10 | 30.2 | 30.5 | 10.5 10.7 10.7 10.7 | 31.3 | 31.3 | 31.0 | 12.2 12.3 | 32.6 32.8 | 32.70 | 33.4 33.4 |
| 8.4 5 | 25.0 25.0 26.2 25.7 25.1 26.4 25.7 26.1 26.5 25.70 20.2 26.7 | 20.0 20 20.8 27 20.9 27 | 5.10 27.3 7.0 27.4 7.2 27.6 7.3 27.7 | 27.70 27.70 27.70 28.40 28.40 28.4 | 28.3 28.5 28.7 28.8 | 28.7 28.9 28.7 28.7 20.0 | 0.013 | 9570 | 10.10 | 30.4 | 0.6 | 0.00 | 1.3 | 3,00 | 32.3 | 2.3 | 27 | 3.0 3.2 3.3 | 33.4 33.6 33.8 | 33.8 93.10 34.0 |
| 8.0 2 | 26.7 26.4 26.8 26.7 26.6 26.60 26.3 26.7 26.7 26.4 26.9 27.1 | 27: 1 27 27: 2 27 27: 4 27 | 5 27 0 | 28. 1 28. 7 28. 3 28. 7 | 28.0 | 20. 2 2 | 0.0 9 | 0.0 | 0.3 10.3 30.7 | 0.7 | 1.0 | 1.8 | 1.80 | 32.0 | 32.5 32.5 32.8 | 12.0 12.11 13.3 | 3.1 | 3.5 | 3.10 | 34.2 34.4 34.0 |
| 8.8 4 | 26.0 26.0 27.3 | 27. 5 27 27. 7 27 | 1 28.4 | 28.6 283 28.8 20.0 | 20.5 | 29.7 3 29.0 3 | 0.0 3 | 0.0 | 30.10 | 1.2 | 1.3 | 1.9 | 2.4 | 32.6 | 32.10 | 33.3 33.5 | 3.7 | 3.71 | 4.0 | 34.10 |
| 90 \$ | 26.0 26.0 27.3 26.7 27.0 27.4 26.0 27.3 27.7 20.0 27.3 27.7 | 27.10 28 28.0 28 | 28.7 | 28.11 20.4 20.1 20.5 | 10.8 | 30.0 3 | 0.5 | 0.0 | 30.10 | 1.0 | 2.0 | 2.3 | 2.5 | 33.0 | 33.0 33.2 33.6 | 33.50 | 4.3 | #.3 #.57 | 35.0 | 5.4 |
| 8.10 \$ | 27.0 27.4 27.0 27.1 27.6 27.6 27.3 27.7 28.0 27.4 27.0 28.1 | 28.4 28.4 28.6 28.6 | 0 28 10 7 20 0 10 20 3 | 20.3 20.3 20.0 20.0 20.0 30.0 | 30.3 30.4 | 0.01 | 0000 | 1.0 | 1.5 | 1.10 3 1.11 2.1 2.3 | 2.0 | 2.8 2.70 3.0 | 2.11 3.3 3.4 | 3.5 | 3 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 | 4.0 | 200 | 5.3 | 5.0 | 15.80 15.00 |
| 9.0 3 | 27.0 27.11 28.3 27.8 28.0 28.3 27.8 28.2 28.0 27.11 28.3 28.8 | 28.8 20 28.8 20 28.9 20 | 20.5 | 20.0 30.2 | 30.0 30.8 | 30.11 3 | 1.35 | 1.8 | 2.2 | 2.5 | 2.0 | 3.2 | 3.0 | 3.11 | 4.3 | 4.8 4.8 5.0 5.2 | 5.0 | 5.5 | 5.91 | 0.2 0.4 30.6 |
| 2.2 | 27.11 28.3 28.8 | 20.0 29 | 3 29.8 | 30.2 30.7 | 30.11 | 31.43 | 1.83 | 2.13 | 2.03 | 2.10 | 3.3 | 3.7 3 | 4.0 3 | 4.4 | 34.9 | 5.2 | 5.00 | 5.11 | 0.3 | 0.8 |

A TABLE OF FEET AND INCHES from 9 foot 2 inches and a ty 3 foot and a an inch to 12 foot & inches by 4 foot 30.0 30.10 31.9 31.8 32.1 32.5 32.10 33.3 33.8 34.0 34.5 34.10 35.3 30. 7 31. 0 31. 5 31. 10 32.3 32.7 33. 0 33.5 33.10 34.3 34.8 35.0 35.5 35.10 36.3 36.8 37.1 37.5 31.7 31.7 32.7 32.8 33.2 33.7 34.0 34.3 34.8 35.3 35.8 36.1 36.6 36.6 37.3 37.8 38.7 38.6 3 30.60 31.3 31.8 32.0 32.0 33.4 33.0 34.7 35.0 35.3 36.8 37.1 37.6 37.0 38.4 38.9 30.2 30.7 31.0 32.2 33.7 33.0 33.0 33.7 34.2 34.7 35.2 35.7 36.0 30.3 36.7 37.8 38.7 38.8 30.8 30.8 40.3 32.4 32.4 32.0 33.2 33.7 34.0 34.5 34.7 35.4 35.0 30.2 36.7 37.0 37.5 37.0 38.3 38.8 30.2 30.7 40.0 40.5 31. 6 32. 0 32. 2 33. 2 33. 2 34. 5 34.0 35. 2 35. 7 30. 0 37. 0 37. 0 37. 0 38. 2 38. 7 30. 0 30. 5 30. 1 40. 4 40. 0 4 32. 5 32. 7 33. 4 33. 9 34. 3 34. 8 35. 7 36. 6 36. 5 36. 7 36. 6 36. 7 37. 4 37. 8 38. 9 38. 8 38. 7 30. 7 40. 6 40. 5 40. 7 40. 6 32.11 33.3 33.6 34.4 34.0 33.2 33.8 36.1 36.7 37.0 37.0 37.1 38.3 38.8 36.3 39.7 40.2 40.5 40.5 41.0 42.0 42.3 35.0 36.2 36.8 37.1 37.7 38.0 38.0 38.1 39.5 39.10 40.4 40.9 41.3 41.8 42.2 42.7 33.0 34.5 35.3 35.8 36.3 36.3 37.3 37.8 38.2 38.7 38.1 30.7 30.0 40.6 20.9 41.3 41.70 42.4 42.80 43.3 34.0 35.0 35.3 30.0 30.4 30.0 37.4 37.0 38.3 38.0 30.2 30.8 40.0 40.0 40.7 41.5 41.7 42.0 42.0 43.0 43.5 35.0 35.5 30.0 30.5 30.1 37.4 37.10 38.4 38.0 30.3 30.0 40.3 40.9 41.2 41.8 42.2 42.8 43.1 43.7 44.1 44.7 45.0 45.0 35. 6 36. 0 30.5 30.11 37. 5 37.11 38. 5 38.11 30. 4 30. 10 40. 4 40. 10 41. 4 41. 10 42. 3 42. 0 43. 3 43. 0 44.3 44.0 45. 2 45. 8 46. 30.0 30.0 37.0 38.0 38.5 38.11 39.5 38.11 40.3 40.5 41.5 41.5 42.5 43.5 43.7 44.4 4410 45.4 45.10 40.8 47.2 30.0 37.0 37.0 38.0 38.0 30.0 30.0 40.0 40.0 41.0 42.0 42.0 43.0 44.0 44.0 45.0 45.0 45.0 45.0 47.0 47.0 12.0 2 37.0 37.0 38.0 38.0 38.0 30.0 40.7 40.7 41.1 41.7 42.7 43.7 44.7 44.7 45.7 45.7 40.2 40.8 47.2 47.8 37. 5 37. 7 38. 5 38. 7 30. 5 30. 7 40. 7 41. 0 41. 0 42. 0 42. 0 43. 0 43. 0 44. 7 45. 1 45. 7 40. 7 47. 1 47. 8 48. 2 48. 37. 0 38. from 4 foot and 2 an inch by 4 foot and & an inch to 5 foot by 5 foot.

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A TABLE OF FEET AND INCHES from 5 foot and half an inch by & foot and half an inch by & foot and half an inch to 10 foot by 5 foot.

| | | / / | rom | 15 1 | ove | ana | vay (| ur er | un e | 4 4 | 1000 | anu | reces of | ave | 10000 | processors | and district | CONCOR | PORTON | A-M-1007/M | 4 7 | T T | F - |
|----------------|--|--------|------------------------------|--------------------------------|--------------------------------------|--|-------------------------------|--------------------------------|------------------------------|---|------------------------------|-------------------------------|---------------------------------------|---|-------------------------------|--|-------------------------------|--------------------------------------|-----------------------|-----------------------|------------------------------|------------------------------|------------------------------|
| I. Parts | F.I F | .I | F.I | F.I | F.1 | P.1 | F.I | F.1 | F.I | F.1 | F.1 | F. I | F.I | F.I | P.I. | E.I. | 1.82 | F.I | 4.95 | 4.10 | 4.102 | F.1 | 4.112 |
| . 0 £ | 20. 4 20 20. 7 20 | 7.7 | 20.10 | 21.0 | 21.3 | 21.5 | 21.8 | 21.00 | 22.3 | 23.5 | 22.6 | 22.8 | 22.// 23./ | 25. / 25. / 25. / 25. / 26. / | 23.0 | 300 300 300 300 300 300 300 300 300 300 | 23.0 | | 24.4 | 24.4 | 25.00 | 24.0 | 25.0 |
| 2 5 | 20.0 20 | 3 | 21.0 | 21.8 | 21.0 | 21.71 | 22.6 | 22.5 | 22.9 | 23.0 | 23.0 | 23.3 | 33 G | 23.8 | 33.6 | 24.4 | | 24.0 | 25.0 25.0 | 25:0 25:2 26:4 | 25.2 25.4 26.7 | 25.5 25.70 | 25.7 25.00 20.0 |
| 34 | 24.7 | 30 | 22.0 | 21.10 22.1 22.3 | 22.3 22.3 22.3 | 22.6 22.6 22.8 | - | 22.0 | 29.4 | 20 2 | | 24.0 | 243 | 24 g | 24.8 24.8 | 24.9/ | 25.1 | 25.4 | 35.5 | 36.0 | 20.0 | 26.9 | 20.3 |
| 45 5 | 21.0 | 11,35 | 22.2 22.4 22.6 22.8 | 2222 | 22.7 22.00 23.00 29.2 | 22.00 23.03 23.4 | 23.3 23.5 | 23.3 23.0 23.0 23.0 | 23.0 | 23.01 | 24.2 | 24.2 24.4 24.7 24.9 | 37.00 | 245 O | 25.3 | 25 A | | 25.0 | 28.4 | 2000 | 20.5 20.70 | 20.6 20.6 27.0 | 20.0 |
| .0 5 | 22.5 22 | . 8 | 22.40 | 23.1 | 23.4 | 23.7 | 23.0 | 24.0 | 040 | 24.0 24.0 24.0 25.0 | 240 | 24.11 | 25.2 | 25.5 25.5 25.7 25.7 | 25.600 | 25/0 | 26 1 20 3 20 0 | 26.4 20.0 20.0 | 26.7 | 20.0 | 27.0 | 27.3 27.5 27.8 | 27.0 |
| 8 2 | 22.0 23 | 02 | 23.4 | 23.7 | 23.10 | 24.1 | 24.6 24.6 24.8 | 24.4 24.7 24.0 24.11 | 24.0 25.0 25.2 | | | 25.80 25.80 | 3511 | 26.0 26.2 26.4 | harabadhanal | 20.5 20.8 20.6 | 26.11 | 27:4 | 27.2 | 27.5 27.6 | 27.7 | 27.10 28.1 28.3 | 28.1 28.6 |
| 90 \$ | 23.5 23.7 23.7 | 80 | 2331 | 24.2 | 24.4 24.7 | 24.7 | 24.10 | 25.1 | 25.6 | Annual Column Street or other Designation of the last | | 26 6 | 26.0 | 26.4 26.4 26.9 | CONTRACTOR OF STREET | 27.0 | 27.3 | 27.8 | 27.91 | 28.5 28.5 | 28.2 28.5 | 28.0 28.8 28:11 | 28.0 28.11 20.2 |
| 10 1 | 24.3 | 2 46 | 4.5 | 24.8 24.10 25.0 | 24.11 | 25.0 | 25.5 25.7 25.7 25.9 | 25.5 25.80 25.00 20.0 | 26.1 | 25.14 20.4 20.6 | 20.2 20.5 20.7 20.9 | 26.10 26.10 27.0 | 20.10 | 27.4 | 27.2 | 27.0 | -02 | 28.4 28.6 | 28.4 | 25.8 | 28.49 | 20.0 | 20.4 |
| 0 5 | 24.5 | 8002 | 15.1 15.3 15.5 | 25.2 25.36 25.80 25.8 | 25.5 25.0 25.11 | 25.8 23.0 20.0 | 25,10 | 20.2 20.4 20.7 20.9 | 20.5 20.7 26.6 27.0 | 20.8 20.10 27.3 | 27.1 | 27.2 27.4 27.9 27.9 | 27.5 27.7.8 27.7.8 28.0 0 | 27.8 27.8 28.3 | 27:1/2 28:46 28:60 | 29.7.9 29.85 20.85 | 28.5 28.6 28.6 29.0 | 28 8 28 1 29 3 | 28500 297 | 20.2 20.5 20.60 | 20.5 20.0 20.0 30.0 | 20.81 30.4 | 30.1 30.4 30.7 |
| 2 4 | 25.1 25 | 6 | 5.7 | | 20.0 20.0 20.0 20.0 20.0 | | | | 27.77.00 | 27.5 | 27.8 | 27:11 28:0 28:0 | 28.5 | | | 20.0 20.2 20.7 | 20.3 | 20.6 20.8 20.11 | 20.0 | 30.0 30.2 30.5 | 30.3 30.0 30.8 | 30.0 30.0 30.1 31.2 | 30.0 |
| 4 5 | 25.0 20 | 0.0 | 26.4 | - | Alle Carlette L. S. Seller | | | | | 28.2 | 28.5 28.5 | | 28.11 28.11 | 29.0 29.3 20.5 | 29.3 20.6 20.8 | 29.7 20.9 20.1 30.2 | | | 30.7 30.7 30.11 | 30.10 31.0 | 31.1 | 31. 4 | 31.70 |
| | | 7 | 6.6 6.8 6.6 | 26.11 | 27.2 | 27.5 | - | 28.0 | 28.3 28.3 | 28.35.85 28.28.50 29.47 | 28.5 28.7 28.0 20.0 | 28.80 28.7 29.3 | 20.4 29.6 | | 30.1 | | | | 31.2 | 31.3 31.5 | 31.11 | 31.9 | 32.3 |
| 0778 | 20.5 20.7 20.0 20.0 27 | 3 | 7.0 | 7.57.9 | 27.0 | 27.00 28.00 28.00 28.00 28.00 28.00 | | | 28.70 28.00 29.2 | | - | CONTRACTOR OF THE PARTY OF | 30.3 | 30. 2 30. 4 30. 7 | 30.5 | 30.0 | 31.2 | 308 | | | 32.0 | 32.7 | 32.8 |
| 8 4 | 27. 1 27 27. 3 27 27. 3 27 | 570 | 7.8 7.10 8.0 | 27.11 28.1 28.4 | 28.3 28.5 28.7 | 28.6 28.8 28.0 | 28.00 20.0 20.2 20.4 | | 20.0 | 20.80 20.00 30.0 | 30.3 | 30.2 30.4 30.7 | 30.6 30.8 30.0 | 30.0 30.11 31.2 31.4 | 31.03 | 31.0 | 31.00 | 32.0 | 32.4 32.4 32.6 | 32.0 | 33.4 | 33.5 | 33.3 |
| 10 | 27.71 27 27.71 28 | .11 | 8.4 8.6 | 28.8 28.0 | 28.11 29.1 | 20.3 | 20.6 | 20.10 | 30.1 | 30.4 | 30.8 30.10 | 30.11 | 31.3 | 31.8 | 31.10 | 32.1 32.3 32.6 | 32.7 | 32.8 | 32.11 33.2 33.4 | 29.3 39.3 39.9 | 33.0 | 33.40 34.0 34.3 | and the same of the same of |
| 02 | 28.3 28 28.0 26 | 9 2 | 8.6 | 20.2 | 29.3 29.8 | 29.9 | 30.0 | 30.4 | 30.5 | 30.0 | 31.2 | 31.8 | 32.0 | | 32.7 32.7 32.7 | 32.8 32.10 | 33.2 | 33.3 33.5 | 33.0 33.0 | 33.10 34.0 34.3 | 34.1 | 34.7 | 34.8 |
| 2 2 | | .3 | 9.3 9.5 9.7 | 20.8 20.10 | 30.0 | 30.3 | 30.5 | 30.10 | 31.2 | 31.8 | 31.0 | 32.3 | 32.4 | 32.8 | 33.2 | 33.3 33.5 | 33.7 | 33.10 | 34.3 | 34.5 34.8 34.10 | 34.91 | 35.0 35.3 35.5 | 35.4 35.0 35.0 |
| 2 42 | 20. 2 20 20. 4 20 20. 6 20 20. 8 20 | 27.01 | 0.1 | 30.2 30.4 30.6 | 30.6 30.8 30.10 | 30.10 | 31.40 | 31.5 | 31.11 | 32.0 32.2 32.5 | 32.4 32.6 32.8 | 32.7 32.10 33.0 | 32.11 33.1 33.4 | 23.2 | 33.6 | 33.0 34.0 34.3 | 34.2 34.6 34.6 | 34.5 34.6 34.6 | 34.0 | 35.0 | 35.4 | 35.8 | 3531 36.2 36.4 |
| 4550 | 20.10 30 30.0 30 30.2 30 | 2.3 | 0.7 | 3011 | 31.02 | 31.0 | 31.00 | 32.2 | 32.35.80 | 32.7 32.0 32.11 33.1 | 3211 | 33.2 33.4 33.7 33.0 | 33.80 | 33.10 | 34.4 | 34.5 34.0 34.0 | 34.0 | 35.03 | 35.0 | 35.80 | 30.2 30.4 30.7 | 30.3 30.8 36.8 36.8 | 30.7 30.0 37.0 37.0 |
| 0 5 | 30.4 30 30.6 30 30.8 30 | 2.10 3 | 1.1 | 31.5 | 31.0 | 32.0 | 32.4 | 32.8 | 33.0 | 33.4 33.0 | 33.7 | 33.11 | 34.350 | 34.7 | 34.11 | 35 2 35.5 35.7 | 35.0 35.8 35.8 | 35.10 30.0 30.3 | 36,2 36,4 36,6 | 36.5 36.8 36.10 | 30.9 37.0 37.2 | 37.3 | 37.5 |
| 8 2 | 31.0 31 | .0 3 | 1.7 | 32.0 | 32.3 | 22 0 | 23 / | 33.5 | 33.8 33.9 | 33.18 | 34.4 | 34.8 34.8 | 35.0 | 35.2 35.4 35.6 | 35.5 35.8 35.40 | 35.0 36.0 30.2 | 30.1 30.4 30.6 | 30.7 36.10 | 30.9 36.11 37.2 | 37.1 37.3 37.3 | 37.7 | 37.11 38.1 | 38.0 38.3 38.5 |
| 90 2 | 31.8 32 | 200 | 2.2 | 32.3 32.5 32.8 | 32.0 | 33.3 | 33.5 | 33.0 | 34.1 | 34.7 | 34.11 | 35.3 35.5 | 35.5 35.7 35.0 | 35.0 35.11 | 36.5 36.5 | 36.7 36.9 | 30.81 30.11 | 37.0 37.5 | 37.0 | 37.80 | 38.0 38.2 38.5 | 38.6 38.0 | 38.50 |
| 11 5 | 32.0 32.2 32.4 32.4 | 8 | 2.B 2.0 3.0 | 33.0 33.2 33.4 | 33.6 33.8 | 33.8 33.0 34.0 | 34.0 34.2 34.4 | 34.4 34.0 34.8 | 34.8 34.10 35.0 | 35.0 35.4 35.4 | 35.6 35.6 35.8 | 35.7 35.00 30.0 | 36.2 36.4 | 36.3 36.6 36.8 | 30.7 30.0 37.0 | 30.11 37.2 37.4 | 37.3 37.0 37.8 | 37.70 37.10 38.0 | 38.4 | 38.3 38.8 38.8 | 30.0 | 30.2 | 30.8 30.8 |
| 05 | 32.0 32 32.8 33 32.0 33 | 1000 | 3.2 | 33.0 33.8 33.0 | 33.10 34.0 34.2 | 34.2 34.4 34.0 34.0 | 34.8 | 34.10 | 35.4 | 35.8 | 35.0 30.3 30.3 | 36.2 36.4 36.7 36.7 | 30.0 | 30.10 37.13 37.5 | 37.2 37.4 37.7 37.0 | 37.0 37.0 37.11 38.1 | 37.10 38.1 38.3 38.5 | 38.5 38.5 38.5 38.5 38.5 | 38833 | 30.3 | 30.4 | 30.0 | 40.3 40.3 |
| 2 5 | 33.2 33 33.4 33 | 0.03 | 3.10 4.0 34.0 | 34.2 | 34.7 | 34.11 | 35.3 35.5 | 35.7 | 3511 | 30.3 | 30.7 36.9 | 30.11 | 37.3 37.0 | 37.70 | 38.0 38.2 38.4 | 38.4 38.6 38.8 | 38.8 38.0 30.0 | 30.0 | 30.4 30.0 30.0 | 30.8 | 40.0 40.3 40.5 | 40.4 40.7 40.9 | 40.8 |
| 4 4 5 | 33.8 34 33.10 34 | 1.2 | 4.4 | 34.11 | 35.1 35.3 | 35.5 35.7 35.0 | 35.9 | 36.1 | 30.5 30.8 30.0 | 36.10 37.0 37.2 | 37.2 37.4 37.6 | 37.8 37.8 37.80 | 37.10 38.0 38.3 | 38.0 38.5 38.5 | 38.0 38.0 38.11 | 38.11 30.1 39.3 | 30.3 30.5 30.8 | 39.7 30.0 40.0 | 40.2 40.4 | 40.6 40.8 | 40.7 | 41.2 | 41.0 |
| 356 6 t | 34.2 34 34.4 34 | .6 3 | 5.1 | 35.3 35.3 35.7 | 35.0 | 30.1 | 36.4 36.6 | 36.8 | 37.0 37.2 | 37.6 37.0 | 37.0 | 38.1 38.3 38.5 | 38.5 38.7 38.10 | 38.9 38.11 39.2 | 30.4 30.6 | 39.8 39.10 | 40.0 40.3 | 40.4 | 40.6 | 41.3 | 41.8 | 42.0 | 42.4 |
| 7 5 | 34.8 34.10 35.0 35.0 | 5.35 | 5.5 | 35.0 35.11 30.1 | 30.4 30.6 | 30.6 30.8 36.10 | 36.10 37.0 37.2 | 37.2 37.4 37.7 | 37.7 37.9 37.91 | 37.11 38.1 38.3 | 38.3 38.5 38.8 | 38.7 38.0 39.0 | 39.0 39.2 39.4 | 30.6 30.6 39.0 | 30.8 | 40.3 40.5 | 40.5 | 41.0 | 41.6 | 41.8 | 42.1 | 42.5 | 42.0 |
| 00000 12 12 | 35.2 33 35.6 33 35.8 35 | 5.0 | 5.11 | 36.3 36.8 36.8 36.8 | 36.8 36.0 37.0 37.2 | 37.02 37.2 37.6 | 37.4 37.7 37.0 37.11 | 37.0 37.11 38.1 | 38.1 38.3 38.8 38.8 | 38.80 38.80 39.0 | 38.0 30.2 30.5 | 30.24 | 30.5 | 30.11 40.1 40.4 40.6 | 40.3 40.0 40.8 40.10 | 40.8 40.10 41.9 41.3 | 41.5 | 41.01 | 42.2 | 42.8 42.8 | 42.8 42.10 43.1 | 43.3 | 43.5 |
| .10 2 | 35.10 30 36.0 30 | 5.3 | 6.7 | 37.0 | 37.4 37.0 37.8 | 37.9 37.11 38.1 | 38.1 38.3 38.3 | 38.5 38.8 38.10 | 3840 30.0 30.2 | 30.2 30.5 30.7 | 30.7 30.0 30.11 | 30.11 40.4 | 40.4 40.6 40.8 | 40.8 40.10 41.1 | 41.1 | 41.5 | 41.0 42.0 42.2 | 42.2 42.4 42.7 | 42.0 42.0 42.1 | 4211 43.0 43.4 | 43.3 | 43.8 43.0 44.0 | 44.0 |
| .0 \$ | 30. 7 30 30. 0 37 30. 0 37 30. 0 37 | 5.11 | 7.4 | 37.6 37.8 37.10 | 37.10 38.1 38.3 | 38.3 38.5 38.7 | 38.70 39.0 | 39.0 39.2 39.4 | 39.4 39.7 39.6 | 39.9 | 40.4 | 40.6 40.8 40.50 41:3 | 41.1 | 41.5 | 41.10 42.0 | 42.2 42.5 | 42.7 42.9 | 42.11 43.2 | 43.4 | 43.8 | 44.3 | 44.5 | 44.10 |
| | 36.11 37 37.1 37 37.3 37 | 35 | 7.8 | 38.0 38.0 | 38.7 38.0 | 38.9 38.11 39.2 | 30.2 39.4 30.6 | 39.9 | 40.1 | 40.4 40.6 40.8 | 40.8 | 41:3 | 41.8 | 42.0 | 42.7 | 42.9 | 43.0 43.2 43.4 | 43.0 | 44.1 | 44.4 | 44.8 | 45.1 | 45.8 |
| 734 | 37. 3 37 37. 3 37 37. 3 37 37. 9 38 | 911 | 8.48 | 38.0 | 39.3 | 30.00 30.00 30.00 | 30.8 | 40.3 40.5 | 40.6 40.6 40.60 | 40.10 41.0 41.3 | 44.35 | 41.70 | 42.0 42.2 42.5 | 42.0 | 43.2 | 33.7 | 珍儿 | 44.4 | 44.0 | 45.1 | 45.0 | 45.8 | 10.3 |
| 45356 | 37.11 38 38.1 38 38.3 38 | 35.70 | 8.00 | 30.7 | 30.5 30.8 30.0 40.0 | 30.10 40.0 40.2 40.4 | 40.3 40.7 40.7 | 40.70 | 41.0 | 4.5 | 1200 122 123 124 | 42.4 42.4 42.0 | #2.7 #2.0 #3.2 | 43.02 | 43.4 43.9 43.9 | 43.7 | 440 | 44.91 | 25.8 | 45.00 45.11 | 40.4 | 400 400 40.8 | #0.8 #0.11 |
| .05 | 38.7 36 38.0 30 38.1 36 30.1 36 | 2.03 | 0.4 | 30.0 | 40.2 40.4 40.6 | 40.7 | 40.11 | 41.4 | 41.0 | 42.2 42.4 42.6 | 42.0 42.0 42.11 | 42.11 | 43.6 43.0 | 43.9 | 44.2 44.0 | 44.0 | 44.11 | 15.4 15.0 15.0 | 15.0 | 10,2 | 100 | 4011 | 47.0 |
| 8 2 | 30.3 30.3 30.5 | 2.7 | 0.10 | 40.3: 40.5 40.7 | 40.8 | 41.3 | 41.8 | 42.1 | 42.3 42.6 42.8 | 42.8 42.11 43.1 | 13.1 | 43.6 43.8 43.10 44.3 | 44.1 | 44.0 44.8 | 44.8 44.11 45.1 | 45.6 45.6 | 450 | 40.0 40.0 | 70.0 | 40.0 | 4 4 4 4 4 | | |
| 90 t | 30.3 36 30.5 36 30.0 36 30.0 46 | 2.4 | 0.5 | 40.10 | 41.2 | 41.9 | 42.2 | 42.7 | 43.0 43.2 | 43.3 | 43.0 | 44.3 | 44.8 | 45.3 | 15.8 | 40.4 | 10,0 | 4011 | 77.1 77.1 | 17.0 | 19.1 | 187 | 19.0 |
| 114 | 30.11 40 40.1 40 40.3 40 40.5 40 | 2.80 | 0.11 | 41.8 | 41.0 | 42.4 42.4 42.6 | 42.7 42.9 42.11 | #3.0 #3.4 | 35 | 44.2 | ##3 ##3 | 45.0 | 45.5 45.5 | 装 | 103 | 200 | 46.11 | 34.0 | 120 | | 100 | | 200 |

A TABLE OF FEET AND INCHES

to 6 Foot to Inches by 6 Foot 15 Foot and & an Inch FIFIFIFIFIFIFIFIFIFIFIFIFIFIFIFIFIFI FI 6.0 5.10 5.11 5.6 5.10 FIParts

42 7.10 % 8.09 8.45 8.05 8.85 9.02 9.05 9. 25 9.45 9.6% 9.85 9.10 % 57.8 57.3 57.10 58.3 58.5 57.3 57.11 58.4 58.9 58.4 10.05 2333 10.45 10.04 10.8½ 8½ 10 50.3 50.8 57.4 50.3 56.1 57.4 50.8 57.4 57.2 28 5 28 11 30 7 30 3 28 7 30 7 30 3 28 7 30 0 0 0 3 10.10% \$0.00 00.3 60.0 00.0 60.0 00.0 39.4 30.7 30.10 60.0 11.05 00.0 01.2 00.11 61.5 04.2 01.5 01.3 01.51 99. 4 59.00 59. 7 60.0 59. 8 60.3 60.8 60.3 11. 25 98.40 30.8 39.9 30.9 30.8 50.8 30.9 60.3 30.0 60.3 03.0 03.0 03.0 05.2 11. 45 11.05 03.0 11.85

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| A TABI From II Foot 10 Inches a | | EET AND | | 6 Foot |
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| PH EN EN EN EN EN EN | PERSONAL DEPOSITION OF THE PERSONAL PROPERTY O | FI FI FI FI | FIFIFIFI | EL EL EL EL EL |
| F.I. Parts 3.02 5.16 5.15 5.2 5.25 5.3 5.32 11.19 3 38.19 80.7 80.19 81.7 82.7 82.7 82.7 83.1 | 51 4 5.42 5.5 63.7 63.9 63.5 63.7 64.9 63.5 | 5.0 5.0 5.0 5.0 5.7 5.7 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 | 7 3 8 5 8 5 0 5 0 5 0 8 | 03 00 0 70 3 70 0 71 3 |
| 12.0 \$ 36.5 67.5 67.5 62.6 52.5 63.6 63.8 12.0 \$ 36.8 67.3 67.9 68.3 68.9 63.3 63.9 | 64.8 84.8 85.6 8 94.3 94.9 95.3 9 | 3. 8 68. 8 66. 8 67. 8 67 29 96. 3 86. 8 67. 8 67 | 8 8 3 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 | 6.6 70.6 77.6 77.6 72.0 70.3 70.6 77.6 72.0 72.3 |
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| 3 4 9 62.3 63.0 63.3 63.0 64.3 64.9 65.3 62.2 62.8 63.2 63.0 64.3 64.9 65.3 | 05.4 05.50 06.4 05.5 00.3 00.6 | 97.4 07.60 08.4 08.60 09 | 12 00 5 70 2 70 5 70 1 2 2 3 7 4 2 3 7 5 5 7 6 1 2 3 7 6 1 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 | 7 3 72 3 72 9 73 3 73 9 74 0 74 3 74 3 74 3 74 3 74 3 74 3 74 3 |
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| 37.3 37.6 38.0 37.3 37.6 38.0 6 26 37.0 37.0 38.0 38.3 38.7 | | | | |
| 38.3 38.3 38.0 38.0 38.0 38.0 30.4 30.7 30.70 | 40.1 | | | |
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| 7.0 42.3 42.7 42.10 43.2 43.5 43.9 44.0 44.4 42.10 43.1 43.5 43.8 44.0 44.3 44.7 | 44.7 44.7 45.2 44.70 45.2 44.70 45.2 45.5 | 15. 2 45. 0 45. 9 40. 1 40. 4 45. 0 45. 0 40. 4 40. 4 40. 8 40. | 0.4 40.8 40.11 47.3 47.0 0.8 40.7 47.3 47.0 47.10 0.11 47.3 47.0 47.10 48.1 | 98 / 48 2 48 8 49 9 49 3 28 3 48 8 48 3 46 3 46 7 |
| 7.34 43.7 43.9 44.2 44.8 44.8 45.1 | 43.5 45.8 46.6 4 | 40.3 40.7 40.11 47.2 47 40.7 40.0 47.2 47.5 47.5 47.5 | 1.0 48.7 9 48.7 48.4 48.8 2.0 48.4 48.4 48.8 48.7 3.0 48.4 48.8 48.7 48.3 | 40.3 49.3 49.7 49.10 50.2 40.3 40.7 40.10 50.2 50.5 40.0 49.10 50.1 50.5 50.9 |
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| 8.0 5 18.70 48.11 48.3 48.70 48.11 28.3 20.70 | 20.11 21 3 21.70 2 21.5 21.00 21.70 2 | 2. 11 52 3 52 7 52 11 53 22 0 53 0 53 2 53 0 53 | | |
| 8.24 40.7 40.1 50.3 50.7 51.0 51.4 51.8 | 52.0 52.7 52.9 5 52.0 52.7 52.9 5 52.7 52.9 5 | 3 0 83 4 53 8 54 0 54 3 3 63 7 53 8 54 7 54 | \$ 24 8 83 4 83 8 83 9 8 7 8 8 7 8 8 8 8 8 9 | 34 36 5 50 9 37 4 37 5 8 6 37 8 37 4 37 4 38 8 |
| 8.42 50.7 50.11 51.4 51.8 52.9 52.7 52.8 8.42 50.7 50.11 51.4 51.8 52.9 52.4 52.8 | 62.0 53.1 63.0 5 53.0 53.8 52.6 5 | 53.10 54.2 54.0 54.10 55 14.1 54.3 54.9 25.2 24 14.4 54.8 55.1 55.5 5 | 12 55.7 55.7 55.7 50.3 50.7 6 10 55.9 50.2 50.0 50.7 6 10 50.5 50.0 57.2 57.2 6 | 7.3 57.7 57.4 58.3 85.7 7.3 57.7 57.4 58.3 85.7 |
| 8.05 21.7 22.0 22.4 22.8 23.8 23.6 23.9 | 8376 83 4 84 8 8 844 848 849 8 | \$ 2 25 0 55 7 55 7 66 3 56 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 | 0.4 50.8 57.0 57.4 57.9 | 58.7 58.5 58.9 39.2 59.0 |
| 8.05 31.76 52.0 52.4 52.9 53.9 53.5 53.9 53.6 54.2 54.3 52.0 53.1 53.6 54.2 54.3 52.0 53.1 53.6 54.2 54.3 52.0 53.1 53.6 54.2 54.3 52.0 53.1 53.6 54.2 54.3 54.3 52.0 53.1 53.6 54.2 54.3 54.2 54.2 54.2 54.2 54.2 54.2 54.2 54.2 | 54.4 54.5 55.1 5 54.7 55.0 55.7 5 54.7 55.3 55.7 5 | 50.8 50.4 50.8 57.4 57 50.3 50.7 57.9 57.4 57 | | 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 |
| 8.85 - 22.70 23.9 23.4 23.8 24.70 25.7 | \$2. 2 \$3.0 \$3.4 \$3.8 \$3.8 \$3.8 \$3.8 \$3.8 \$3.8 \$3.8 \$3.8 | 50 3 50 70 57 0 57 7 58 58 58 58 58 58 58 58 58 58 58 58 58 | | 00.0 50.00 00.3 00.7 00.7 00.0 00.2 00.0 00.7 00.3 00.4 00.5 00.0 00.2 00.0 00.8 00.0 00.5 00.0 00.0 |
| 8.19 \$ 53.70 54.0 54.4 54.0 55.4 35.6 35.6 35.6 35.6 35.6 35.6 35.6 35.6 | | 7.7 3.3 3.7 3.3 3.3 3.3 3.3 3.3 3.3 3.3 | | 8.8 84.2 84.5 82.7 82.4 8.3 84.76 82.3 82.7 83.8 |
| 0 08 18 18 18 18 18 18 18 18 18 18 18 18 18 | | 1 3 5 3 5 3 5 3 5 5 5 5 5 5 5 5 5 5 5 5 | | |
| 0 - 2 - 33 - 8 - 54 - 0 - 54 - 57 - 2 - 57 - 7 - 57 - 7 - 58 - 7 - | 第 元 3 8 % 元 3 % 元 | | 0 20 6 20 0 20 0 70 0 7 | |
| 10 46 46 9 67 0 67 6 87 10 68 2 58 7 100 C | 60 4 60 0 60 2 6 | 676 80 11 81 4 81 8 88 88 88 88 88 88 88 88 88 88 88 8 | 4 989 984 983 988 9 | |
| 0.04 37.5 37.0 %5.2 38.7 38.0 30.4 37.0 0.04 37.8 38.4 38.4 38.6 38.4 39.5 39.5 39.5 39.5 39.5 39.5 39.5 39.5 | | 17 18 18 18 18 18 18 18 18 18 18 18 18 18 | ALCOHOL CONTRACTOR INCOMES AND RESIDENCE INCOMES INCOM | 2.3 (2.7) 64.3 66.3 66.9 2.3 (2.7) 64.3 66.3 66.9 2.4 (2.8) 66.3 67.3 67.3 66.3 66.6 67.3 67.8 |
| 8 3 3 3 6 3 4 3 7 36 6 36 3 66 6 | 61.3 61.7 62.0 6 | 25 0220 (33 03.8) 64 | 0 04.5 04.0 05.3 05.8 0 | 50.7 00.5 00.00 07.3 07.8 |

an abota | abota | abota | abota | abota | ab

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A TABLE OF FEET AND INCHES
From g Foot & Inches and a toy 6 Foot and t an Inch to 12 Foot 6 Inches by 7 Foot

| | | | | | | | | | | | | | | | | | Inch | | | | | | | |
|----------|---------------------------------|--------------------------------|--------------------------------------|--------------------------------|----------------------------------|-----------------------------------|--|-------------------------------|-------------------------------|---------------------------------------|-------------------------------|----------------------------------|--------------------------------|----------------------------------|--------------------------------|--------------------------------|-----------------------------------|-------------------------------|--------------------------------|--------------------------------|------------------------------|-------------------------------|----------------------------------|------------------------------------|
| EFParts | F.1 | | | | - | | | | | | | | | | | | F.I 6.85 | | | | | | | The second second |
| 0.85 | 28.72 | 29.1 | 39.0 | 50.10 | 00.3 | 90.8 | 61.1 | 01.6 | 91.11 | 92.4 | 42.8 | 43.1 | 93.6 | 93.11 | 94.4 | 949 | 0.55 05.5 08.8 | 05.6 | 95.11 | 00.4 | 00.9 | 97.2 | 97.70 | 97.11 98.7 98.7 |
| 9.10% | 50. 6 50. 2 60. 3 | 00.1 | 00.0 | 00.6 | 01.4 | 61.9 62.0 62.3 | 02.2 02.3 02.3 | 02.0 02.0 02.0 03.1 | 02.11 | 03.4 | 03.0 04.1 04.4 | 04.2 04.0 04.0 | 04.70 04.70 05.2 | 05.0 05.3 05.3 | 65.28 65.38 65.88 | 05.10 | 60.3 60.0 60.10 | 00.8 00.11 07.3 | 67. 1 67. 4 67. 8 | 67.0 67.0 68.1 | 67.12 68.60 | 09.4 | 08.5 08.9 08.4 | 08.10 08.15 08.50 |
| 10.04 | 60.8 60.11 61.2 | 01.1 | 01.6 01.0 02.0 | 01.8 02.2 02.5 | 02.4 | 02.0 03.0 03.3 | 03.2 | 03.70 | 04.0 64.3 04.7 | 04.5 04.5 05.8 | 04 10 | 05.0 | 03.80 800.3 | 0000 | 00.0 00.10 07.1 | 00.0 | 07. 4 07. 4 08.2 08.2 | 07.00 | 00000 | 08.7,7 | 69.0 69.7 69.7 | 09.5 09.0 70.0 | 00.10 | 70.4 |
| 10.24 | 01.8 61.11 02.2 | 02.0 02.4 02.7 | 02.0 02.0 03.0 03.0 | 02.11 | 03:25 03:35 03:57 | 03.10 | 04.3 04.0 04.0 | 04.8 | 95.14 | 55500 | 05.0 | 00000 | 66.9 | 97.90 97.00 97.00 | 07.8 07.12 08.2 | 68.7 68.7 | 68.0 68.0 69.0 69.4 | 68.12 69.6 69.6 | 09: 4 09: 7 09: 12 | 69.9 | 70.3 70.6 70.9 | 70.7 | 71.04 | 71.0 |
| | 02.8 02.7 03.2 03.2 | 03.4 | 03.7 | 0440 | 64.5 64.5 64.8 | 04.10 | 05.40 | 050000 | 60.2 60.5 60.8 | 66.70 66.70 67.1 | 67.03 67.70 | 677.00 677.00 688.00 | 07.10 08.5 08.5 | 08.4 08.7 08.10 | 68.9 69.8 69.3 | 60.2 60.5 60.9 | 08.7 86.11 70.2 70.5 | 70.0 70.4 70.7 | 70.0 | 70.11 | 71.4 | 71.0 | 72.20 | 72.8 72.8, 73.3 |
| 10.64 | 03.9 03.2 04.5 | 04.2 04.5 04.8 | 04.70 04.70 05.4 | 02500 | 02 28 000 3 | 05.11 00.2 00.5 | 66.4 66.7 66.10 | 00.0 07.3 07.3 | 97.3 97.9 97.9 | 67.8 67.2 68.5 | 68.7 68.7 | 68.6 68.10 60.1 | 60.0 80.0 80.0 | 60.5 60.8 10.3 | 00.10 70.1 70.5 | 70.3 70.7 70.10 | 70.0 71.0 71.3 71.7 | 71.2 | 71.7 71.11 72.2 72.5 | 72.0 72.4 72.7 72.7 | 72.0 72.0 73.4 | 72.11273.00 | 73.40 | 73.9 |
| 10.82 | 04.8 04.11 05.2 05.5 | 05.2 05.5 05.8 | 05.7 05.0 00.4 | 00.0 00.3 00.7 00.10 | 66.6 66.0 67.0 67.3 | 66.11 67.2 67.58 | 67.4 67.8 67.8 68.2 | 67.10 08.4 08.7 | 08.30 | 08.9 08.3 08.3 | 60.2 60.3 60.8 | 69.7 69.11 70.2 70.5 | 70.1 70.4 70.7 70.70 | 70.0 70.9 71.1 | 70.11 | 71.5 | 71.10 72.1 72.2 72.8 | 72.3 72.7 72.10 73.2 | 72.8 73.8 73.4 73.7 | 73.3 73.0 74.8 | 73.7, 73.3 74.0 | 74.4 74.8 74.8 | 74.0 74.10 75.1 | 74.11 75.3 73.70 |
| 10.10 % | 65.8 65.11 66.2 66.5 | 00.2 00.3 00.8 00.11 | 00.7 00.10 07.1 | 67.4 67.7 67.70 | 67.6 67.6 68.3 | 68.0 68.0 68.0 68.0 | 00000000000000000000000000000000000000 | 68.10 69.5 69.8 | 00.4 00.7 00.10 70.2 | 00.0 70.4 70.7 | 70.3 | 70.8 | 71.2 71.5 71.8 72.0 | 71.70 71.70 72.2 72.5 | 72.1 72.4 72.7 72.11 | 72.0 72.0 73.1 73.4 | 72.11 73.3 73.0 73.10 | 73.5 73.8 74.3 | 73.10 74.2 74.5 74.9 | 74 4 74 7, 74 7, 75 2 | 74.9 75.4 75.8 | 75.30.10 | 75.88 | 70.2 70.5 70.9 77.0 |
| 11.04 | 06.0 | 67. 2 | 97.8 | 68.4 | 68.7 | 60.0 | 60.0 | 20.11 | 70.2 | 70.10 | 71.4 | 71.9 | 72.3 | 72.8 | 73. 2 73. A | 73.7 | 74.1 74.4 74.8 74.11 | 74.0 | 75.0 | 75.5 | 75.11 | 70.4 70.8 70.7 77.3 | 76.10 77.5 77.8 | 77. 4 77. 7, 77. 1, 78. 2 |
| 11. 2334 | 67.9 68.0 68.6 | 08.2 08.5 08.11 | 08.8 08.1 00.2 09.5 | 69.4 69.8 69.8 | 69.70 69.70 70.4 | 70.4 70.4 70.7 70.6 | 70.6 | 71.0300 | 71.5 71.0 72.0 72.3 | 71.2.59 | 72.5 72.8 72.7 73.2 | 72.10 73.2 73.5 73.8 | 73.4 73.7 73.10 74.2 | 73.0 74.1 74.4 74.7 | 74.3 74.0 74.10 75.1 | 74.9 | 75:30 73:00 78:00 | 75.8 75.3 70.0 | 70.1 70.5 70.8 77.0 | 70.7 70.11 77.2 77.5 | 77.4 | 77.0 77.10 78.1 78.5 | 78.77.10 78.77.10 78.77.10 | 78.6 78.9 79.4 |
| 11.45 | 68.9 69.3 69.6 | 90.2 90.5 90.0 90.11 | 60.8 60.11 70.2 70.5 | 70.2 70.5 70.8 70.11 | 70.7 70.11 71.2 71.5 | 71.4 | 71.70 | 72.1 72.4 72.7 72.10 | 72.6 72.9 73.1 73.4 | 73.0 73.0 73.0 73.9 | 73.0 73.9 74.3 | 73.11 74.3 74.0 74.0 | 74.5 74.8 74.71 75.3 | 74.1/2 75.5 75.5 75.8 | 75.4 75.8 76.2 | 75.10 | 70. 4 70. 7 70. 10 77. 2 | 70.9 77.4 77.8 | 77.3 77.10 77.10 78.1 | 77. 9 78.0 78.4 78.7 | 78.3 78.9 78.9 | 78.8 78.8 79.3 79.7 | 2500 | 79.8 79.3 80.3 80.0 |
| 11.64 | 80.0 70.3 70.0 | 70:3 70:9 71:0 | 70. 8 70.11 71. 3 71. 6 | 71.2 | 71.8172.272.3 | 72.2 72.5 72.8 72.11 | 72.7 73.2 73.5 | 73.7 | 73.70 73.70 74.4 | 74.1 74.4 74.7 74.10 | 74.6 74.10 75.1 75.4 | 73.0 73.4 73.6 73.6 | 75.0 73.9 70.4 | 70.0 70.0 70.10 | 70.0 70.0 77.4 | 70.113 | 77.58 78.8 78.3 | 77.11 78.0 78.9 | 78.5 78.3 79.3 | 78.02.50 | 79.8 79.8 80.3 | 79.10 80.1 80.5 80.8 | 80.4 80.7 80.11 81.2 | 80.10 |
| 11.84 | 70.0 | 71.3 | 71.0 72.0 72.3 72.3 72.0 | 72.2 72.3 72.9 73.0 | 72.8 72.3 73.3 73.6 | 73. 2 73. 3 73. 8 73. 11 | 73.8 73.1 74.2 74.5 | 74.2 74.3 74.8 74.11 | 74.8 74.11 75.2 75.5 | 73 2 73 3 75 77 | 75.7,19.2 | 70.1 70.3 70.8 70.11 | 76.10 76.10 77.2 77.5 | 77. 1 77. 4 77. 8 77.11 | 77.70 77.10 78.1 78.5 | 78.4 | 78:76 | 79.0 79.4 79.7 79.11 | 79.6 70.10 80.1 80.4 | 80.0 80.4 80.7 80.10 | 80.6 80.0 81.1 81.4 | 81.0 81.7 81.10 | 81.0 81.0 82.1 82.4 | 82.0 82.3 82.70 |
| 11.10 % | 71.00 | 72:3 72:0 73:0 | 72.0 73.0 73.3 73.0 | 73.90 73.90 74.0 | 73.00 74.03 74.00 | 74.9 74.9 75.0 | 74.00 | 75.20 | 74.8 78.8 78.3 76.0 | 70.00 70.00 77.00 | 70.8 77.8 77.3 77.0 | 77. 2 77. 6 77. 9 78. 8 | 77.8,78.3 | 78.2 78.5 78.0 79.0 | 78.8 78.11 79.3 | 70.2 70.5 80.8 | 78.8, 80.3 | 80.2 80.5 80.0 81.0 | 80.8 | 81.50 | 81.8 82.3 82.0 | 82.2 82.5 83.0 | 82.8 82.3 83.0 | 83.2 83.5 83.0 84.0 |
| 12.04 | 73.8 73.8 73.8 | 23:3 73:90 74:00 | 73. 9 74. 8 74. 3 74. 0 | 74.3 74.6 74.9 75.0 | 74.9 | 73.3 73.8 76.8 | 75.80 | 70.3 | 70.9 77.0 77.4 77.7 | 77.3 77.10 77.10 78.1 | 77.8 78.6 78.7 | 78.3 78.70 78.10 | 78.9 78.4 78.4 | 79.3 | 70.0 80.4 80.4 80.7 | 80.3 80.7 80.10 81.1 | 80.9 81.4 81.7 | 81.3 | 81.9 82.4 82.4 82.8 | 82.7 82.70 83.2 | 82.0 83.4 83.8 | 83.3 83.70 84.2 | 83.9 84.4 84.4 | 84.4 84.7 84.7 85.2 |
| 12.3334 | 73.9 74.0 74.3 74.0 | 74.3 74.0 74.0 75.0 | 74.00 | 75.3 73.70 75.10 76.1 | 70.4 | 70.70 | 70.10 | 77.47 | 77.10 78.1 78.4 78.7 | 78.4 78.70 78.2 79.2 | 78.10 78.2 79.3 | 70. 8 70.00.2 80.2 | 70.10 80.2 80.5 80.8 | 80.4 80.9 80.2 | 80.11 | 81.38 | 8/./2 82.5 82.5 | 82.28 83.3 83.3 | 82.7 83.0 83.9 | 833.48 84.3 | 84.3 84.0 84.10 | 84 50 85 4 | 85.10 85.10 | 80.4 80.4 |
| 12.44 | 74.0 | 75.30 | 75.10 76.4 76.7 | 70.4 70.7 70.10 77.1 | 70.10 77.1 77.4 77.7 | 77. 70 77. 70 78. 2 | 77.10 78.3 78.8 | 78 8 78 9 78 2 79 2 | 78.2 79.3 79.8 | 70. 8 70. 8 70. 2 | 70.7 80.6 80.9 | 80.9 81.0 81.3 | 81.9 | 87.0 82.0 82.4 | 82.3 82.6 82.6 | 82.9 83.4 | 83.70 | 83.10 84.5 | 84.4 | 84.10 85.5 85.5 | 85.4 85.8, | 82.11 80.20 | 80.5 80.8 87.8 | 87.3 87.0 |
| | \ | | 3 | | | | | Z C | C | 3 | | | | 3 | 9 | | T. | | | | 7 | | | |
| | | | | | S | | | | | | | · A | | | | | | PO | | | | | | |
| | | F | om . |) 7 For | rt an | a ? | an i | hch | by 7 | Foot | ana | 10 | Tinc | h w | 8 10 | 000 | Inch | es by | 8 Fo | W vot | | | | |
| | F,I | F ,1 | F.I | F.I | F.I | F. 1 | F.I | F. I | F.I | F.1 | F.I | F.I | F.I | F.I | F.T | F.I | F. I | F.I | F.I | F. I | F. I | F. I | F. I | F.I |
| 7.0% | 49.7 40.11 50.3 | 50.3 | 50.0 | 1.2 | 1,22 | 1.3 | 1.32 | 1.4 | 1.42 | 1.0 | 1.32 | 7.0 | 7.02 | 1.1 | 1./2 | 1.0 | 1,02 | 1.9 | 7.92 | | | | | 0.0 |
| 7: 24 | 50.0 50.0 51.1 51.4 | 50.9 51.1 51.4 51.8 | 51.1 51.4 51.8 | 31.8 31.11 52.3 | 52.0 52.3 52.7 | 52.70 | 53. 3 | | | | 2 40 | | | | | | | | | | | | | 3 3 |
| 7. 45 | 51.8 51.11 52.13 52.10 | 51.11 52.3 52.0 52.10 | 52.70 52.70 53.2 | 52.7 52.10 53.1 53.5 | 23.70 23.30 23.00 23.00 | 53.0 53.0 53.9 | 53.0 53.0 54.5 54.5 | 54.1 54.5 54.8 | 54.5 54.8 55.0 | 35.0 55.4 | 55.8 | 66.2 | | | A.C | | | | | | | | A. 10. | 0.00 |
| 7.0% | 53.1 53.5 53.8 | 53.5 53.5 54.0 | 53.8 54.8 54.4 | 54.1 54.4 54.8 | 54.4 54.8 55.0 | 54.8 55.3 | 55.0 55.4 55.7 | - | 35.7 | 55.11 | 55.7 56.3 56.7 57.2 | 50.7 | 30.11 37.3 57.0 | 57.6 | 38.3 38.3 | 60.0 | | | | | | | | |
| 7-842 | 24.3 24.7 34.70 | 54.7 54.7 55. 3 | 54.11 55.3 55.0 | 55.3 55.70 55.70 | 55.70 | 35.77 35.77 30.60 30.60 | 50, 2 50, 6 50, 10 | 50.0 50.10 57.2 | 56.10 57.3 37.0 | 57.3 | 57.0 57.10 58.4 | 57.10 58.5 58.5 | 58.2 58.5 58.9 | 58.20 | 58.9 589.5 589.5 | A REST OF THE OWNER, THE PARTY | 59.50 | 60.1 80.5 80.5 | 60.0 | 61.4 | | | | ALAS |
| 7.10 % | 55.3 55.8 56.0 | 55.0 56.4 | 56.1 56.5 56.8 | 50.5 56.0 57.0 | 20.0 57.4 | 57. 1 57. 2 57. 8 | 57.5 57.0 58.0 | 57.9 58.4 58.4 | 28.4 | · · · · · · · · · · · · · · · · · · · | 58. 9 58. 4 59. 4 | 3999 | 59.58 | \$9.0 60.0 60.4 60.4 | 00.4 00.4 00.8 | 50000 | 00.00 | 01.04 | 01.4 01.8 02.0 02.4 | 01.80 02.40 02.40 | 62.0 62.4 62.8 63.8 | 62.8 | 63. 4 | 64.0 |
| 8.02 | 56.8 50.7 57.3 | 57.0 | 57. 4 | 57.8 57.8 58.3 | 58.0370 | 58.47 58.77 | 58.8 58.3 58.3 | 50.03 50.37 | 38.47 38.11 38.11 | 29. 87 39. 37 80. 37 | 60.37 | 00.4 00.8 00.11 | 60.8 61.3 61.3 | 61.0 | 61. 4 61. 8 61. 11 | 02.0 | 62.0 62.4 62.8 | 62.4 62.8 63.8 | 62.8 63.4 63.4 | 0334.00 | 63.4 63.8 64.8 | 63.8 64.0 64.4 64.4 | 04.0 04.8 05.8 | 64.4 64.8 65.0 65.4 |
| 8 - 24 | 57.10 | 58.2 | AL DISCHARGE | A ANDREW | 59.3 | 50.6 | 59.10 | 60.3 | Estimates. 48 | Company and | Service of Laboratory | Name of the last | Designation of the last | 62.3 | 92.7 | 62.11 | 63.3 | 93.7 | 03.11 | -BALL-III | 24.8 | 05.0 | 95.8 | 65.8 |

A TABLE OF FEET AND INCHES From 8 Foot 6 Inches and a 2 by 7 Foot and 2 an inch to 12 Foot 6 Inches by 8 Foot

| F1 | F.I | F. I | | | F.I | | | | | Marian Articles | THE RESIDENCE OF THE PARTY OF T | SCHOOL CHICAGO | and the same of | H STATE OF THE STATE OF | | | | | | | | F. I | F.I | F . I |
|-----------|-------------------------------|---------------------------------|-------------------------|------------------------------|------------------------------|------------------------------|--------------------------------|-------------------------------|-----------------------|------------------------------|--|------------------------|-------------------------------|-------------------------------|------------------------------|------------------------------|------------------------------|-------------------------------|--|-------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| FI Parts | 7.05 | 7.1. 60.6 | 7.18 | 7.2 | 7.25 | | | | | | | | | | | 7.8 | 7.8% | 7.9 | 7.95 | 7.10 | 7.102 | 7.11 | 7.112 | 8.0 |
| 34 | 9.3 9.3 01.0 | 00.10 | 61.5 | 01.0 | 62.0 62.0 | 02.3 02.6 02.10 | 62.7, 62.7, 63.2 | 02.8 03.3 03.7 | 03.4 | 03.8 64.8 64.3 | 04.0 04.4 04.8 | 64.4 64.8 65.8 | 04.9 05.4 | 05.9 05.9 | 05.5 66.4 | | | | | 07.3 67.4 67.4 | 07.7 07.11 08.3 | 07.11 08.3 08.7 | 68.8 69.0 | 88.8 69.4 |
| 8.84 | 01.7 01.7 02.2 | 02.8 02.3 02.7 | 02.1 02.4 02.11 | 02.5 03.8 03.4 | 82.0 83.0 83.8 83.8 | 03.2 03.0 03.0 04.0 | 03.0 03.10 04.5 | 03.10 04.0 04.0 | 04.3 04.10 05.2 | 04.7 04.7 05.2 05.0 | 04.11 | 05.4 | 05.8 00.4 00.7 | 00.0 00.4 00.8 07.0 | 00.5 00.9 07.0 07.4 | 00.9 07.5 07.5 | 07.2 07.5 07.0 08.1 | 07.0 67.0 68.2 68.5 | 07.00 08.00 08.00 | 03.70 | 08.7, 08.3 09.7 | 68.3 69.7 69.11 | 60.8 70.0 70.4 | 70.8 70.4 70.8 |
| 8.10 % | 02.0 62.0 63.4 | 02.10 03.2 03.5 | 03.3 033.0 033.0 | 03.7i | 64.0 64.3 64.70 | 04.4 04.8 04.11 | 94.9 85.8 95.4 | 05.1 | 05.5 05.9 | 05.10 00.2 00.5 | 00.2 00.0 00.10 | 60.70 67.3 | 60.11 | 67.4 | 67.8 68.3 | 08.0 08.4 08.6 00.0 | 08.5 | 68.9 68.9 69.5 | 69.6 69.6 69.0 | 60.0 60.10 70.3 | 00.11 70.3 70.10 | 70.3 | 70.8 71.0 71.4 71.7 | 71.4 |
| 9.0% | | THE CARLEST | SCHOOL STORY CO. | 64.10 65.1 63.5 | 85.20 85.00 85.00 | 95.70 85.70 | 05.11 00.3 00.6 | 00.4 | 06.8 07.8 07.4 | 07.1 07.4 07.8 | 07.15 07.5 08.0 | 67.10 68.1 68.5 | 68.2 | 68.7, 68.7, 60.2 | 68.13 69.7 | 00.4 00.5 00.5 | 69.8 76.8 70.4 | 78.1 78.5 70.9 | 70.5 | 70.10 | 71.30 | 71.7, | 71.11 | 72.4 72.8 73.0 |
| 0.25 | 04.10 | 65.3 | 85.71 | 66.0 | 66.3 | 66.9 | 00.10 | 07.3 67.6 67.10 | 07.7 07.11 08.3 | 08.0 08.4 08.7 | 08.7 08.8 08.0 | 08.9 | 09.2 09.3 | 60.10 | 70.3 | 70.7 | 70.8 | 71.4 | 71.9 | 72.2 | 72.0 72.0 72.0 73.2 | 72.11 | 73.3 | 73.8 74.0 74.4 |
| 9.45 | 63:3 66.0 66.4 | 66.1 66.3 | 00.0 | 88.7, 87.3 | 67. 3 67. 3 | 67. 4 67. 8 68. 0 | 08.4 08.4 | 68.5 68.9 | 68.0 68.2 88.3 | 69.3 69.0 | 69.7 00.11 70.3 | 70:8 70:4 | 70.5 | 70.0 | 71.2 | 71.7 | 72:3 | 72.4 | 72.9 | 73:9 73:8 | 43.0 73.10 74.3 | 73.11 | 74.7 | 74.8 |
| | | 07.0 07.3 | 87.8 08.0 | 07.9 08.5 | 97.74 68.6 68.6 | %.76 60.2 | 69.8 69.3 | 09.4 09.8 70.0 | 70.4 | 70.2 70.5 70.9 | 70.70 | 70.11 | 71.8 | 72.6 | 72.3 | 73.3 | 73.3 | 73.4 | 73.8 74.8 | 74.5 | 74.10 | 75.2 | 73:3 | 76.8 76.4 |
| 7 4 | 07.0 07.0 08.1 | BECOME STREET | SECTION AND DESCRIPTION | | | | | | | | | | | | | | | | | 75.5 | 75.10 | 76.2 | 76.7 | 77.8 77.4 77.8 |
| 9.8% | | 08.7 69.4 69.8 | 66.6 63.9 70.4 | 00.10 | 70.03 | 70.8 | 71.5 | 71.60 | 72.3 | 72.4 | 73:4 | 73.5 | 73.00 | 73.11 | 74.4 74.8 75.8 | 74.9 | 75.70 | 73.7, | 70.0 | 70. 8 77. 8 | 70.9 | 77.8 | 77.7, 78.3 | 78.4 78.8 78.8 |
| 9.10% | 69.6 60.10 70.1 70.5 | 60.11 70.3 70.10 70.10 | 70.4 | 70.9 | 71.00 | 71.71 | 72.0 72.4 72.7 72.11 | 72.50 | 72.50 | 73.702 | 73.80 74.3 74.7 | 74.4 74.8 75.8 | 74.0 74.9 75.5 | 75.00 | 73.7 75.7 70.3 | 76.6 76.4 76.8 | 70.9 | 70.10 | 77.3 | 77.88 78.84 78.4 | 78.3 78.3 78.9 | 78.70 78.20 79.2 | 78.11 78.3 79.7 | 70. 4 29. 8 80. 8 |
| 10.0% | 70.0 | 71.2 | 71.70 | 72.0 | 72.5 72.8 73.3 73.3 | 72.10 73.5 73.8 | 73.30 | 73.8 73.1 74.3 74.7 | 74.4 | 74.0 74.0 75.1 75.5 | 74.11 75.20 75.10 | 75.47 | 75.9 76.4 76.8 | 76.2 76.6 70.9 77.1 | 70.7, 70.7, 77.3 | 77.04 | 77:5 78:4 78:4 | 77.10 78.2 78.5 78.9 | 78.3 78.11 79.3 | 78.8 79.3 79.8 | 70.7 | 70.00 70.00 80.0 | 80.3 80.7 80.11 | 80.4 80.8 81.4 |
| 10.24 | 71.11 | 72.4 | 72.9 73.0 73.4 | 73.2 | 73.7 | 74.0 74.4 74.7 | 74.5 | 74.10 75.0 | 75.3 | 75.90 | 70, 2 70, 5 70, 9 | 76.70 76.10 77.3 | 77.0 | 77.5 | 77.10 | 78.37 78.77 78.77 | 78:8 78:8 70:4 | 70.1 | 79.60 70.00 80.00 | 80.0 80.7 80.11 | 80.5 | 80.10 | 81.3 | 81.8 82.4 82.4 82.8 |
| 10.44 | 73.1 73.4 | 73.0 73.0 73.9 | 73.7 | 74.4 | 74.9 | 75.3 | 75.8 | 70.1 | 70.0 | 70.11 | 77.5 77.8 78.8 | 77:10 78:1 78:5 | 78.3 78.7 78.7 | 78.8 78.8 79.4 | 79.1 | 79.00 79.10 80.3 | 80.0 80.4 80.7 | 80.5 | 80.10 | 81:3 | 81.8 82.8 82.4 | 82.2 82.6 82.6 | 82.7 82.11 83.3 | 83.0 83.4 83.8 |
| 10.6% | 73.11 24.3 74.0 | 74.4 74.8 75.8 | 74.10 75.1 75.2 | 75.7 | 75.8 76.0 76.3 | 76.5 | 76.10 76.10 77.3 | 77.0 77.4 77.7 | 77.9 78.1 | 77.10 78.3 78.6 | 78.7 78.7 78.7 | 78.9 79.1 79.4 | 79.2 79.0 79.10 | 79.7 | 80.5 80.5 80.8 | 80.0 | 81.3 | 81.8 82.8 82.4 | 82.2 82.0 82.0 | 82.7, 82.7, 83.3 | 83.0 83.4 83.8 | 83.5 83.5 84.0 | 83.11 84.3 84.7 | 84.4 84.8 85.0 |
| 10.84 | 74.70 75.5 | 75.10 | 78.8 | 70.9 70.9 | 78:71 77:3 | 77.4 | 77.9 | 78.3 78.6 78.10 | 78.8 79.0 | 78:1 73:3 | 70.3 79.7 70.10 80.3 | 80.4 80.7 | 80.9 | 80.11 | 81.4 | 82.1 82.5 | 82.70 | 82.8 83.0 83.4 | 83.5 | 83.7 | 84.4 84.8 | 84.0 | 84.11 85.3 85.7 | 85.4 85.8 86.8 |
| 10.10% | 70.3 | 70.5 | 76.11 | 77.4 | 78.9 | 78.3 78.0 | 78.8 79.4 | 70.2 | 80.3 | 80.0 80.4 80.8 | 80.6 80.10 81.1 | 80.11 | 81.8 | 82.0 82.0 | 82.7 | 83.4 83.4 | 83.6 83.0 | 83.8 83.11 | 84.9 | 84.10 | 85.4 85.8 | 83.3 | 88.3 88.7 | 87.0 |
| 11.0 | 70.10 77.2 77.5 | 77:4 | 77.9 78.4 78.4 | 78.3 78.6 78.10 | 78.8 79.3 | 70.2 70.5 79.9 | 79.7, 80.2 | 80.4 80.8 | 80.10 | 81.03 | 81.5 | 82.0 | 82.4 82.6 82.7 | 83.5 83.5 | 83.70 83.70 | 84.0 84.4 | 84.0 84.9 | 84.11 85.3 | 85.5 85.8 86.0 | 85.10 | 86.4 86.7 | 86.6 87.1 | 87.3 87.0 | 87. 8 88.8 88.4 |
| 1.0 % | 77. <i>9</i> 78.4 78.8 | 78.3 78.0 78.0 78.0 | 78.8 79.3 79.7 | 70.2 70.5 79.0 80.0 | 79.7 80.0 80.0 | 80.4 80.8 80.1 | 80.10 81.1 81.5 | 81.3 | 0002.4 002.4 | 82.2 82.6 82.6 | 82.6 83.0 83.3 | 83.5 | 83.7 83.11 84.3 | 84.4 84.4 84.8 | 84.6 84.50 85.2 | 85.8 85.3 85.7 | 85.5 | 80.0 | 86.4 86.8 87.8 | 86.10 87.2 87.6 | 87.3 87.7 87.11 | 87.7 88.5 | 88.6 88.6 88.0 | 88.8 80.4 |
| T. COOM | 787700 | 70.5 | 79.10 80.5 80.5 | 80.4 | 80.10 | 81.3 81.70 82.2 | 9048 90048 | 82.2 82.6 82.10 83.1 | 823.37 833.7 | 83334 | 83.7136 | 84.4 | 84.0 84.10 85.2 85.0 | 85.0 85.4 85.8 85.11 | 85.0 85.9 86.5 | 86.7 86.7 86.7 | 80.9 87.0 87.4 | 87.0 87.0 87.10 | 87.88 88.4 | 88.39 88.39 | 88:9 89:3 | 88:4 89:5 89:5 | 89.6 89.10 90.2 | 90.8 90.8 |
| 11. 4 5 | 80.1 80.5 80.8 | 80.7 80.50 1.2 | 81.4 | 81.10 | 82.0 82.4 82.7 | 82.6 82.9 83.1 | 83.7 83.7 | 83.5 83.6 84.0 | 83.11 84.2 84.0 | 84.4 84.00 85.03 | 84.10 85.60 | 85.4 85.7 85.7 | 85.9 | 80.7 80.7 80.7 | 86.0 87.1 87.4 | 87.0 87.0 87.10 | 97.0000 90000 90000 | 00000 00000 1000 | 88.8 88.3 89.7 | 89.5 | 80.7, 90.3 90.7 | 90.1 90.5 90.9 91.0 | 90.0 90.10 91.6 | 91.0 91.4 92.0 |
| 11.62 | 81.3 | 81.9 82.1 82.4 | 82.3 82.0 82.0 | 82.9 83.0 83.4 | 83.3 83.6 83.6 | 83.8 84.0 84.3 | 84.2 84.6 84.0 | 84.8 84.11 85.3 | 85.1 85.5 85.9 | 85.7 85.71 86.3 | 80.1 80.3 80.8 | 86.70 86.70 87.3 | 87. 4 87. 4 87. 8 | 87.0 87.10 88.3 | 88.4 88.8 | 88.0 88.10 89.1 | 89.0 89.7 | 89.3 89.9 90.1 | 80.11 90.3 90.7 | 90.5 | 90.11 | 01.4 01.8 02.0 | 01.10 02.2 02.6 | 92.4 92.8 93.0 |
| 8 ".84 | 82.2 82.5 82.0 | 92.8 92.11 83.3 | 83.5 | 83.7 83.11 84.3 | 84.5 | 84.11 85.3 | 85.4 85.4 85.8 | 85.7 85.10 86.3 | 80.0 80.4 80.8 | 80.0 86.10 87.2 | 87.0 87.4 87.8 | 87.10 88.1 | 88.4 88.7 | 88.9 | 89.3 | 89.9 | 90.3 90.7 | 90.9 91.1 91.5 | 91:3 | 91.9 92.0 92.4 | 92.2 92.0 92.10 | 02.8 03.8 03.4 | 93.2 | 93.8 93.8 94.4 |
| 11.10 % | 83.4 83.7 | 83.10 84.0 | 84.4 | 85.0 | 85.7 | 85.9 86.0 86.5 | 86.7 86.11 | 80.9 87.1 87.5 | 87.7 87.7, | 87.9 | 88.7 88.7 | 88.9. 89.4 | 89.3 82.70 | 89.9 90.1 90.4 | 90.3 90.70 | 90.9 | 91.6 | 91.8 92.0 92.4 | 92.2 92.6 92.10 | 93.0 93.4 | 93.2 93.6 93.6 | 93.8 94.4 94.4 | 94.2 94.6 94.50 | 94.8 95.0 95.4 95.4 |
| 12.0 % | 84.2 84.0 | 84.8 85.8 85.4 | 85.3 85.6 85.10 | 80.8 | 86.10 86.10 | 80.8 87.8 | 87.3 87.0 87.10 | 87.8 88.8 | 88.0 | 88.8 88.4 | 89.0 | 36:8 88:4 | 90.0 | 91.8 | 91.0 | 92.8 92.4 92.4 | 92.10 93.2 | 93.8 93.4 93.9 | 93.6 | 94.8 94.4 84.8 | 94.6 94.10 95.2 | 95.8 | 95.0 95.10 96.3 | 96.8 96.8 |
| 12 2 4 | 83.5 | 82.7, 80.2 | 80.5 80.8 | 80.7, 87.2 | 87. 5 87. 5 87. 8 | 87. 7 88.2 88.2 | 88.9 | 89.0 | 89.9 | 90.7 | 90.5 | 90.11 | 91.5 | 92.3 | 92.9 | 93.3 93.7 | 93.0 | 94.3 | 94.6 | 95.8 95.8 | 95.10 95.10 | 90.4 90.4 | 90.0 | 97. 4 97. 4 |
| 1337 | 86.3 86.7 86.60 | 86.9 87.4 87.4 | 87.3 87.7 87.70 | 87.9 88.5 | 88.7 | 88.10 89.5 | 80.4 | 90.10 90.2 90.3 | 90.4 | 90.10 | 91.4 | 92.2 | 92.3 | 93.8 | 93.3 94.6 | 94.3 | 94.5 | 95.3 | 96.5 | 96.3 96.7 | 96.10 97.1 | 97. 8 | 98.6 | 98.8 |
| 12.4% | 87.2 87.5 88.7 88.0 | 87.8 87.11 88.3 88.0 | 88.69 88.9, | 889.8 890.3 89.3 | 89.10 89.10 90.1 | 90.4 90.7 | 90.8 90.10 90.10 91.2 | 91.4 | 91.7 | 92.5 92.5 | 92.7 | 93.59 | 93.8 93.7 94.3 | 04.3 94.6 94.9 | 94.8 95.8 95.4 | 95.3 95.6 95.10 | 95.9 96.0 96.4 | 96.10 96.10 | 97.5 | 97. 3 97. 7 97.11 | 97.9 98.1 98.5 | 98.4 98.8 98.11 | 98.10 99.1 99.6 | 99.4 99.8 100.0 |
| | P | | Ration | 0 | | 9 | | | | | | | | | | array de la | | A salt | | | T. | S) | \ | |
| R | | 10.00 | | | | | . 9 | | | | | | | | | | 200 | | 7 | A CO | - | | | - |
| | | | | -6 | | | | 2000年 | | 5 | | Inch | | 96 | of A | ncho | I las | a for | The state of the s | Inch | es es | | | |
| | F.I | F.I | F.I | F.I | F.I | F.I | F.I | F. I | F.I | F.I | F.I | F.I | F.I | F. I | F.I | F.I | F. I | F.I | F.I | F. I | F. I | F. I | F. I | F.I |
| FI Parts | 8.05 | 8.1 | 8.15 | 8.2 | 8.25 | 8.3 | 8.35 | 8.4 | 8.44 | 8.5 | 8.5% | 8.6 | 8.64 | 8.7 | 8.74 | 8.8 | 8.8% | 8.9 | 8.94 | 8.10 | 8.10 | 8.11 | 8.11/2 | 9.0 |
| 14 | 05.0 | 05.4 | 66.0 | 66.0 | 0 | | | | | | | | | | | | | | | * . | | | | |

A TABLE OF FEET AND INCHES From 8 Foot 4 Inches and at by 8 Foot and 2 an Inch to 12 Foot 6 Inches by 8 Foot

| Property of the Property of th | P.I P.I F.I V.I P.I P.I P.I P.I P.I P.I P.I P.I P.I P |
|---|--|
| Column C | 8.3 8.3 8.4 8.4 8.5 8.4 8.6 8.6 8.7 8.7 8.8 8.8 6.9 8.9 8.10 8.11 8.14 9.0 |
| S | 2 80 1 80 5 70 3 70 0 70.00 71.6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 |
| 8 | 70.0 70.0 71.3 71.0 71.11 72.3 72.7 72.11 73.4 73.8 |
| A | 7 57. 60 57. 70 72.3 72.7 72.7 73.4 73.8 74.9 74.9 74.9 74.9 74.9 74.9 74.9 74.9 |
| 9 | 72.0 73.3 73.7 74.8 74.8 74.9 75.1 75.0 76.2 76.7 76.7 77.3 77.8 78.0 |
| 9 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | 73.7 73.7 74.8 74.8 75.8 75.4 75.8 75.4 75.8 76.0 76.0 77.3 77.3 77.8 78.0 78.0 78.0 78.0 80.3 80.3 80.0 |
| 1 | 74.11 73.4 75.8 76.1 70.5 76.10 77.2 77.7 78.4 78.8 78.1 78.5 70.10 80.3 80.7 81.0 81.4 81.5 75.7 76.0 76.5 76.0 77.2 77.7 78.4 78.8 78.1 78.5 76.0 80.3 80.7 81.0 81.4 81.0 82.1 75.7 76.0 76.5 76.0 76.5 76.0 77.2 77.6 77.11 78.4 78.8 78.1 79.5 79.10 80.2 80.7 81.0 81.4 81.0 82.1 82.6 |
| 1 | 76. 0 76. 4 76. 6 77. 6 77. 6 77. 78. 3 78. 8 79. 9 79. 9 80. 7 80. 7 80. 7 81. 4 81. 6 82. 7 82. 6 82. 8 83. 3 78. 8 77. 6 77 |
| 0 | 77. 4 77. 9 78. 1 78. 0 78. 1 79. 4 79. 8 80. 1 80. 0 80. 1 81. 3 81. 8 82. 0 82. 5 83. 2 83. 7 84. 0 84. 4 84. 9 78. 1 78. 0 78. 0 79. 3 70. 8 80. 0 80. 3 80. 0 81. 3 81. 8 82. 0 82. 5 83. 2 83. 7 84. 0 84. 4 84. 9 81. 3 81. 7 82. 0 82. 4 82. 9 83. 7 83. 1 84. 4 84. 9 81. 9 81. 7 82. 0 82. 4 82. 9 83. 7 83. 7 84. 4 84. 9 81. 9 81. 7 82. 0 82. 4 82. 9 83. 7 83. 7 84. 4 84. 9 81. 9 81. 7 82. 0 82. 4 82. 9 83. 7 83. 7 84. 9 84. 9 81. 9 |
| 9 6 6 78 7 76 9 78 9 78 9 78 9 78 9 80 2 80 7 80 7 80 7 80 7 80 7 80 7 80 7 | 78.4 78.9 79.2 79.7 79.1 80.4 80.9 81.2 81.0 81.1 82.4 82.9 83.7 83.0 83.1 84.8 85.7 85.0 78.7 79.0 70.0 80.4 80.8 81.7 81.0 82.4 82.8 83.1 83.0 83.1 84.8 85.7 85.0 83.0 83.0 84.3 84.8 85.7 85.0 85.3 85.0 85.3 |
| 9 10 7 7 7 10 10 10 10 10 10 10 10 10 10 10 10 10 | 1 80.0 80.0 80.0 80.0 80.4 80.9 82.0 82.0 83.4 83.9 84.7 84.7 85.0 83.5 86.7 87.0 87.6 80.0 80.0 80.0 80.0 80.0 80.0 80.0 80 |
| ## 170 0 80.0 80.7 80.0 82.3 82.6 82.7 82.0 82.3 82.8 83.6 83.7 83.0 83.4 84.7 84.8 85.7 83.0 85.7 85.0 85 | 80.0 87.7 82.8 82.5 82.6 83.7 84.0 84.5 84.0 85.3 85.7 86.0 87.3 87.8 86.7 88.0 87.3 87.8 86.7 88.0 87.3 87.8 86.7 88.0 87.3 87.8 86.7 88.0 87.3 87.8 86.7 88.0 87.3 87.8 86.7 88.0 87.3 87.8 86.7 88.0 87.3 87.8 86.7 88.0 88.0 87.3 87.8 86.7 88.0 88.0 87.3 87.8 88.7 88.0 88.0 87.3 87.8 88.7 88.0 88.0 87.3 87.8 88.7 88.0 88.0 87.3 87.8 88.7 88.0 88.0 87.3 87.8 88.7 88.0 88.0 87.3 87.8 88.7 88.0 88.0 87.3 87.8 88.7 88.0 88.0 87.3 87.8 88.7 88.0 88.0 87.3 87.8 88.7 88.0 88.0 87.3 87.8 88.7 88.0 88.0 87.3 87.8 88.7 88.0 88.0 87.3 87.8 88.7 88.0 88.0 87.3 87.8 88.7 88.0 88.0 87.3 87.8 88.7 88.0 88.0 87.3 87.8 88.7 88.0 88.0 87.3 87.8 88.7 88.0 88.0 87.3 87.8 88.7 88.0 88.0 87.3 87.8 88.7 88.0 87.0 87.3 87.8 88.7 88.0 87.0 87.3 87.8 88.7 88.0 87.0 87.3 87.8 88.7 88.0 87.0 87.3 87.8 88.7 88.0 87.0 87.3 87.8 88.7 88.0 87.0 87.3 87.8 88.7 88.0 87.0 87.3 87.8 88.7 88.0 87.0 87.3 87.8 88.7 88.0 87.0 87.0 87.0 87.0 87.0 |
| 1 | 82.2 82.7 83.0 83.7 83.0 83.7 84.3 84.8 85.7 83.0 85.7 85.0 85.0 85.7 85.0 85.7 85.0 85.7 85.0 85.0 85.7 85.0 85.7 85.0 85.7 85.0 85.7 85.0 85.7 85.0 85.7 85.0 85.7 85.0 85.7 85.0 85.7 85.0 85.0 85.0 85.0 85.0 85.0 85.0 85.0 |
| 10.4 2 83 1 83.0 84.4 84.9 85.2 85.7 80.0 86.5 80.0 87.4 87.9 88.2 88.7 80.1 80.0 80.3 90.0 91.3 91.7 92.5 92.5 92.1 93.4 93.4 93.5 84.5 84.5 85.0 85.7 85.0 85.7 85.0 85.7 85.0 85.7 85.0 85.7 85.0 90.3 90.0 91.3 91.7 92.5 92.5 92.1 93.4 93.4 93.5 85.0 85.7 85.0 85.7 85.0 90.3 90.0 91.3 91.7 92.5 92.5 92.1 93.4 93.5 92.5 92.5 92.1 93.4 93.5 92.5 92.5 92.5 92.5 92.5 92.5 92.5 92 | 83.7 83.8 84.7 84.0 85.3 85.8 86.7 86.0 86.7 87.7 87.6 87.3 88.3 88.8 80.0 88.7 80.4 80.4 80.4 80.5 80.0 88.3 88.3 88.8 80.0 80.7 87.3 87.0 87.3 87.0 88.3 88.3 80.5 80.0 80.7 87.3 87.0 88.3 88.3 80.5 80.0 80.7 87.3 87.0 88.3 88.3 80.5 80.0 90.3 90.8 97.7 97.6 83.0 84.4 84.9 85.2 85.7 86.0 86.5 86.0 87.3 87.8 88.3 88.3 88.7 80.0 90.3 90.8 97.7 97.6 |
| 10. 4 2 83 1 83.0 84.4 84.9 85.2 85.7 86.0 86.5 86.0 87.4 87.9 88.2 88.7 80.1 80.0 80.0 0.3 00.0 0.3 00.0 0.3 00.0 02.1 03.4 03.4 03.5 02.1 03.5 03.6 03.1 03.5 03.6 03.1 03.5 03.6 03.1 03.5 03.6 03.5 03.6 03.7 04.5 04.5 04.5 04.5 04.5 04.5 04.5 04.5 | 84.3 84.8 85.7 85.6 84.7 86.4 86.9 87.7 88.7 88.7 88.0 88.3 80.4 80.4 80.7 90.0 91.0 91.5 92.3 84.7 85.4 85.4 85.4 85.4 85.4 85.4 85.4 85.4 |
| 10.0 12 84.9 85.3 85.8 80.1 80.4 80.0 87.0 87.5 87.0 88.3 88.8 80.1 80.0 80.1 90.5 90.0 91.2 91.0 92.3 92.8 93.1 93.0 93.1 93.0 94.4 94.0 92.2 97.2 91.8 92.0 93.3 92.8 93.1 93.0 93.1 93.1 93.1 93.1 93.1 93.1 93.1 93.1 | 85.7 86.9 86.5 86.4 87.9 88.2 88.7 80.1 89.6 89.4 90.9 91.3 97.8 92.1 02.6 92.1 03.4 85.3 86.4 87.3 87.3 87.8 88.6 88.7 80.4 80.5 80.5 80.0 80.3 90.9 91.3 91.3 92.4 92.4 92.4 93.4 93.4 80.3 87.3 87.3 87.3 87.8 88.6 88.7 80.4 80.5 80.5 80.0 80.3 90.9 91.3 91.3 92.4 92.4 92.4 93.4 93.4 93.6 93.3 93.4 93.4 93.6 93.3 93.4 93.4 93.6 93.3 93.4 93.4 93.6 93.3 93.4 93.4 93.6 93.3 93.4 93.6 93.3 93.4 93.4 93.6 93.4 93.6 93.4 93.6 93.4 93.6 93.4 93.6 93.4 93.6 93.4 93.6 93.4 93.6 93.4 93.6 93.4 93.6 93.4 93.6 93.4 93.6 93.6 93.4 93.6 93.6 93.6 93.6 93.6 93.6 93.6 93.6 |
| 10.8 2 8 6 7 8 7 0 8 7 5 8 7 7 8 8 8 8 8 8 8 8 7 8 8 7 8 8 8 7 8 8 8 8 8 8 8 8 7 8 8 7 8 | 87.0 87.5 87.0 88.4 88.0 89.3 89.8 90.7 90.7 91.0 91.5 91.10 92.4 92.9 93.2 93.7 94.7 94.0 87.4 87.9 88.3 88.8 89.3 89.0 89.7 90.5 90.0 91.3 91.0 92.3 92.8 93.7 93.7 94.0 94.5 94.0 87.4 87.9 88.3 88.8 89.3 80.0 80.7 90.5 90.0 91.3 91.9 92.3 92.7 93.7 93.7 94.4 94.0 94.5 97.3 |
| 10.10 12 87.5 87.1 88.4 88.0 89.3 89.9 90.2 90.7 01.1 01.6 92.0 92.5 02.1 03.4 03.10 04.3 04.8 02.3 03.7 06.1 06.6 07.0 07.5 07.10 07.4 07.10 | 88.5 88.7 86.4 86.9 86.3 60.6 67.7 67.7 62.8 52.3 62.7 63.4 63.7 62.8 62.7 63.4 63.7 62.8 62.7 63.4 63.7 63.7 63.7 63.7 63.7 63.7 63.7 63.7 |
| 11.0 88.5 88.4 89.4 89.0 80.3 90.9 91.2 91.8 92.7 93.8 93.6 93.1 94.5 94.10 53.4 95.9 90.3 90.8 97.2 97.7 98.7 98.6 99 | 80.0 80.0 80.3 80.0 91.2 91.8 92.1 92.8 93.1 94.4 94.5 93.3 93.8 90.2 90.7 97.1 97.6 89.9 90.2 90.7 91.1 91.0 92.0 93.4 93.4 93.4 94.5 95.3 93.8 90.2 90.7 97.1 97.6 |
| 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 90.7 90.10 97.4 97.5 92.4 92.5 93.3 93.8 94.7 95.7 95.5 95.0 96.3 96.7 97.7 98.7 98.7 90.5 97.2 97.8 98.7 98.7 90.9 97.2 97.8 98.7 98.7 97.2 97.7 98.7 98.7 98.7 98.7 98.7 98.7 98.7 |
| 2 85.10 86.3 90.9 91.2 91.8 92.7 93.7 93.6 94.8 94.1 95.3 95.10 30.4 50.9 97.3 57.8 98.2 98.8 98.7 100.8 10 | 01.5 81.1 82.4 82.6 83.3 83.6 84.7 85.8 85.3 85.7 86.7 86.6 87.6 87.6 88.4 88.6 88.3 88.6 88.7 88.6 88.7 88.6 88.7 88.6 88.7 88.7 |
| 11 2 2 90.2 90.7 91.1 91.6 92.0 92.5 92.1 93.5 93.10 94.4 94.0 95.3 95.5 96.1 90.7 97.7 08.1 08.6 90.0 90.6 90.1 100.5 1 | 02.5 02.7 03.5 03.0 04.4 94.0 95.3 05.9 96.2 06.8 07.2 07.7 08.7 08.6 09.0 09.6 00.7 100.5 100.0 07.3 07.0 08.5 08.6 08.6 08.6 08.6 08.6 08.6 08.6 08.6 |
| 11.4 12 01.6 01.11 02.5 02.11 03.4 03.10 04.4 04.0 05.3 05.0 00.3 00.8 07.2 07.8 08.1 08.7 00.1 00.6 100.0 100.6 100.11 101.5 101.11 10 3.1 02.3 02.3 02.5 03.3 03.0 04.2 04.8 05.2 05.7 06.1 00.7 07.0 08.0 08.6 08.1 00.5 100.1 100.4 100.10 101.4 101.10 102.3 10 3.4 02.3 02.7 03.1 02.3 02.7 03.1 02.3 02.5 05.0 00.5 00.1 07.5 07.0 08.4 08.0 08.6 08.1 00.5 100.3 100.6 100.1 101.8 102.3 102.8 | 03.00 04.4 04.0 05.3 05.0 06.3 06.8 07.2 07.8 08.1 08.7 00.1 00.6 100.0 100.6 100.1 101.5 101.1 102.4 04.2 04.8 05.3 05.7 06.1 06.7 07.0 08.0 08.0 08.1 00.5 00.1 100.4 100.0 101.4 101.10 102.3 102.0 04.6 05.5 05.0 05.0 06.5 06.1 07.5 07.0 08.4 08.0 08.1 00.5 100.3 100.6 101.3 101.8 102.3 102.8 103.1 |
| 11 6 1/2 92.10 93.4 93.9 94.5 94.10 95.4 95.10 96.4 96.9 97.3 97.9 98.3 98.8 99.2 99.8 100.7 100.7 101.7 102.7 102.8 103. | 95.3 95.8 96.2 96.8 97.3 97.7 98.1 98.7 99.7 100.0 100.6 101.0 101.6 101.11 102.5 102.11 103.5 103.10 103.1 |
| 3. 03.0 04.4 04.9 05.3 05.0 00.3 00.0 07.3 07.8 08.2 08.8 00.2 00.7 00.7 101.7 102.7 102.7 103.1 103.0 104.0 | 90.3 90.9 97.3 97.8 98.2 98.8 99.2 99.8 100.2 100.7 101.7 101.7 102.1 102.7 103.1 103.0 104.0 104.0 105.0 106.7 107.7 107.7 108.1 108.5 108.1 108.5 108.1 105.4 106.0 107.5 107.1 108.5 108.1 108.5 108.1 108.5 108.1 105.4 106.0 107.5 107.1 108.5 108.5 108.5 10 |
| 9 2 9 4 9 9 5 9 9 6 9 7 9 9 7 9 9 8 9 9 8 9 9 8 9 9 8 9 9 8 9 9 9 9 | 97.7 98.7 98.7 99.7 99.7 100.7 100.7 101.7 102.7 102.7 103.0 104.0 104.0 105.0 105.0 105.0 106.0 |
| 12.0 2 90.0 97.0 98.0 98.0 99.0 90.0 100.0 101.0 101.0 102.0 103.0 103.0 104.0 104.0 105.0 | 98.8 00.2 09.8 100.2 100.8 101.6 102.0 102.0 103.0 103.0 104.0 104.0 105.0 105.0 106.0 106.0 107.0 108.0 108.0 108.0 109.0 100.0 100.0 101.0 102.0 102.0 103.0 103.0 104.0 104.0 105.0 105.0 106.0 106.0 107.0 108.0 108.0 109 |
| 77. 2 97. 8 98. 2 98. 8 99. 2 99. 8 100. 2 100. 8 107. 2 107. 8 102. 2 102. 8 103. 3 103. 5 104. 5 104. 5 105. 5 1 | 90.8 100.2 100.8 101.2 101.8 102.2 102.8 103.3 103.0 104.3 104.0 105.3 105.0 106.3 106.0 107.3 107.0 108.3 108.0 100.4 100.4 101.5 101.5 101.5 102.7 102.7 102.7 103.7 103.7 104.7 105.5 105.7 106.7 106.7 107.0 107.0 108.0 108.0 100.0 100.0 |
| 12. 2 2 08. 2 08. 8 99. 2 99. 8 100.3 100.9 101.3 101.9 102.3 102.9 103.3 103.9 104.3 104.9 105.4 105.0 106.4 106.0 107.4 107.10 108.4 108.0 109.4 109.3 109.9 108.4 108.0 109.3 109.9 108.3 109.9 108.3 109.9 108.3 109.9 108.3 109.9 108.3 109.9 108.3 109.9 108.3 109.9 108.3 109.9 108.4 108.0 109.9 108.3 109.9 108.3 109.9 108.3 109.9 108.3 109.9 108.3 109.9 108.3 109.9 108.3 109.9 108.3 108 | 101.7 101.7 102.7 102.7 103.7 103.7 104.8 103.2 103.8 100.8 107.2 107.8 108.2 108.9 100.3 100.0 110.3 101.5 101.1 102.5 102.1 103.5 104.0 105.0 105.0 105.0 100.7 100.7 100.7 108. |
| 12 4 2 00 6 100 0 100 7 101 1 101.7 102.7 102.7 103.6 104.0 105.8 105.8 106.7 107.7 108.3 108.0 108.0 109.4 100.0 110.4 110.0 111.3 1 | 102.1 102.7 103.6 103.6 104.8 104.8 105.8 105.2 103.8 106.3 106.9 107.3 107.9 108.3 108.0 109.4 109.0 110.4 110.0 111.4 102.5 102.5 102.5 103.6 104.8 104.8 104.8 105.8 105.8 105.8 105.8 108.3 108.8 |
| 3 2 100.8 101.8 101.7 102.7 103.4 103.8 104.2 104.8 105.2 105.9 105.3 105.9 107.3 107.5 108.0 10 | 105.7 105.8 104.2 104.8 105.9 100.5 100.9 107.3 107.10 108.4 108.0 109.11 110.5 110.11 111.5 112.0 112 |
| Commence of the second | A PROPERTY OF THE PARTY OF THE |
| THE RESERVE THE PARTY OF THE PA | THE PARTY OF THE P |
| . From 9 Foot and 2 an Inch by 9 Foot and 2 an inch to 9 Foot 2 Inches by 9 Foot 2 Inches | d'an Inch by o Foot and an inch to g root 2 Inches by g Foot 2 Inches |
| The state of the s | F. I |
| 9.0 % 81.9 82.6 82.1 83.3 83.8 84.0 | |

A TABLE OF FEET AND INCHES

| ## 1 | | | Froi | ngs | Foot | 2 Jr. | iche. | sar | rda | 1 20 | 149 | Foot | and | t an | Inc | h to | 12 F | oote | f Inc | hes 0 | 4 10 | Food | t | M | | |
|--|----------|--------------------------|--------------------------|-------------------------|-------------------------|--|------------------------|--------------------------|----------------------------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|-------------------------|--------------------------|--------------------------|-----------------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|-------------------------|-------------------------|
| | 1 1 | F. | F | F | I F | IF | IP | SAPERATED IN | COMPANIES OF THE PERSON NAMED IN | 15/15/Argulate | S SERVICE OF STREET | - | - | | | | | | F, I | F. I | F, I | F, I | F. I | F.I | F, I | F. I. |
| | 9.24 | 83. | 83.4 | 8 84. | 0 84 | 2 9. | 10 0 | 2.3 | 9.35 | 9.4 | 9.4 | 9.5 | 9.5% | 9.0 | 9.0 | 9.7 | 9.75 | 9.8 | 9.8 | 9.9 | 9.9 | 9.10 | 9.10 | 9.11 | 9.11 | 10.0 |
| | 3.16 | 84. | 84. | 84. | 8 8 5 | 7 83 | 7 8 | 6.4 | 86.4 | 87.1 | | , y. | | 1 | | | | | 8 | | | | | | . 10 | |
| | 9.412 | 84. 85. 85. | | 1 80 | 7 85 4 80 | # 80 8 87 | 40,00 | 7.6 | 87.6 87.6 | 87.0 87.11 88.3 | 87.11 88.3 88.8 | 88.8 | 80.0 | 1. | | | | | | 1. 4 | | | | | alian d | |
| | 9.6% | 80.8 | 86.8 | 87. 87. | 97. 5 87. | 0 87 | 10 8 | 8.3 | 38.8 30.1 | 80.1 | 80.5 80.70 | 80.10 | 90.3 | 90.8 | 91.1 | 01.10 | | 100 | 14, | | | | 1. | 4 | | |
| | 0.82 | 87.5 | 87.7 | 88. | 0 88 3 88 7 80 | 3 88 7 89 0 80 | 8 8 | 0.0 | 20.2 | 90.3 00.7 | 90.3 | 90.8 | 91.5 | 91.70 | 92.3 | 92.8 | 93.0 | 93.5 | 043 | | | | | | | |
| | 9 12 | 88.4 | | 80. | 9 89. | 4 80 0 00 2 90 | 9 90 | 0.2 0.8 0.11 | 20.7 | 0000 | 91.5 | 91.10 92.2 92.7 | 92.3 92.7 93.0 | 92.7 93.0 93.5 | 03.0 | 03.5 | 03.10 04.3 04.8 | 04.3 04.8 05.1 | 94.8 95.1 95.6 | 95.1 95.0 95.0 | 05.11 | 06.8 | | | | |
| | 11/2 | 89.8 | 89.6 90.5 | 90.1 90.1 | 00. | 3 90 | 11 900 | 1.4 9 | 21.0 | 92.2 92.7 92.11 | 92.7 93.0 93.4 | 93.5 93.5 | 93.5 93.70 94.2 | 93.10 94.2 94.7 | 04.3 04.7 95.0 | 04.8 05.8 05.5 | 95.1 95.5 95.70 | 05.5 05.10 06.3 | 05.10 00.3 00.8 | 00.3 00.8 | 90.8 | 97.6 | 07.0 07.11 08.4 | 08.4 08.0 | 00.2 | |
| | | 90.9 | 90.0 | 91. | 3 97. 3 92. 3 92. | 92 1 92 5 92 | 0 0 | 2.0 g 2.11 g 3.3 g | 93.4 93.8 | 93.4 93.9 94.1 | 93.9 94.2 94.6 | 94.7 | 94.7 95.0 95.4 | 95.0 95.5 93.0 | 95.5 | 95.10 96.3 96.8 | 90.3 | 90.8 | 97.1 | 97.0 | 97.11 | 98.4 | 98.9 | 99.7 | 100.0 | 100.0 |
| | 10.2 1/2 | 91.7 | 92.4 | 92.3 | 93. 3 03. | 7 94 | .0 0 | 3.8 S | 24.6 | 94.11 | 95.4 | 95.4 93.9 | 96.2 | 90.7 | 97.0 | 97.0 | 97.70 | 98.3 | 08.4 | 08.0 | 99.7 | 100.0 | 100.0 | 100.5 | 100.10 | 101.3 |
| ## 15 15 15 15 15 15 15 15 | 334 | 93.5 | 93.10 93.10 | 93. | 93. | 9 95 | 3000 | 4.70 2.2 5.7 | 25.3 | 05.8 96.5 | 96.0 | 90.0 90.11 97.4 | 97.9 | 97.4 97.9 98.2 | 97.70 98.2 98.7 | 98.8 98.8 | 98.8 98.5 | 90.0 99.0 99.11 | 99.6 99.11 100.4 | 00.11 100.4 100.9 | 100.4 | 100.9 | 101.3 | 101.8 | 102.1 | 102.0 |
| ## 15 15 15 15 15 15 15 15 | 10.45 | 94.2 | 94.7 94.7 95.0 | 94.1 | 9 05 | 10 95 10 95 | .0 00 | 5.0 5 | 20.5 | 90.10 97.3 97.7 | 97.3 97.8 98.1 | 97.8 98.1 98.6 | 98.3 98.0 98.11 | 98.7 98.11 98.4 | 99.5 99.5 | 90.70 | 99.10 100.3 100.8 | 100.3 | 100.0 | 101.2 | 101.7 | 102.0 | 102.5 | 103.4 | 103.4 | 103.0 |
| 3 | 10.0 1/2 | 95.4 | 95.4 | 95. | 2 96. 7 97. | 8 97 | 97 | 1.0 9 | 77.7 | 98.0 98.5 08.0 | 98.5 98.10 00.3 | 98.10 99.3 90.8 | 99.4 | 100.2 | 100.7 | 100.7 | 101 10 | 101.11 | 101.11 | 102.4 | 10230 | 103.8 | 103.8 | 104.0 | 104.7 | 105.5 |
| 8 | 8 | 96.5 | 96.1 | 96.4 | 97. | 5 97 9 98 | 7 00 | 9.3 6 | 8.9 | 00.2 | 100.0 | 100.1 | | | 101.9 | 102.3 | 102.3 | 102.8 | 103.7 | 104.0 | 104.0 | 104.6 | 104.11 | 105.4 | 106.3 | 100.3 |
| | 8 4 | 97.7 | 97.8 98.0 98.5 | 98.4 98.4 | 98 | 0 90 90 4 99 | 0 99 | 0.2 1 | 00.3 00.8 | 100.4 | 100.0 | 101.3 | | 102.6 | 102.7 | 103.0 | 103.6 103.10 104.3 | 104.4 | 104.4 | 10410 105.3 105.7 | 105.3 | 105.8 106.1 106.6 | 106.7 106.7 107.0 | 100.7 107.0 107.5 | 107.1 | 107.6 |
| 2 | 10.10 12 | 98.8 98.8 | 98.9 98.3 99.6 | 90.7 | 99. 100. 100. | 8 100 100 5 100 | 0 10 | 0.7 K | 01.1 | 101.0 | 101.11 102.4 102.0 | 102.5 102.10 103.2 | 10210 103.3 103.8 | 103.4 103.8 104.1 | 103.9 104.2 104.7 | 104.3 104.7 105.0 | 104.8 105.1 105.6 | 105.1 | 105.7 | 100.0 100.5 100.10 | 106.6 100.11 107.4 | 106.11 107.4 107.0 | 107.5 107.10 108.3 | 107.10 108.3 108.8 | 108.4 108.0 100.2 | 108.0 100.2 100.7 |
| 2 | 11.0 % | 99.5 | 100-4 | 100.4 | 2 101. | 3 101 | 8 10 | 2.2 10 | 02,2 | 102.8 103.1 | 103.7 | 104.0 | 104.0 | 104.0 | 104.11 | 105.5 | 105.10 | 100.4 | 100.9 | 107.8 | 107.8 | 108.7 | 100.0 | 109.0 | 100.0 | 110.0 |
| ### ### ### ### #### ################# | 2 2 2 | 100.7 | | 101.0 | 102. | 0 102 | 5 10 | 3.3 | 03.4 | 103.10 | 104.4 | 104.0 | 105.3 | 105.8 | 100.7 | 106.7 | 107.6 | 107.0 | 108.0 | 108.6 | 108.11 | 109.50 | 100.10 | 110.4 | 110.0 | 111.3 |
| ### ### ### ### #### ################# | 3342 | 101.9 | 102.2 102.7 102.11 | 102.8 103.0 103.5 | 103 103 103 | 0 104 | 7 104 | 4.5 NO NO | 74.6 74.11 75.4 | 105.0 105.0 105.0 | 105.6 105.10 106.3 | 105.11 106.4 106.9 | 100.5 100.10 107.2 | 100.10 107.3 107.8 | 107.4 107.0 108.2 | 107.10 108.3 108.7 | 108.8 109.1 | 108.0 | 100.3 | 100.8 | 110.2 | 110.7 | 111.16 | 112.0 112.5 | 112.0 | 112.6 |
| 11 | 11.4% | 102/0 | 103.4 | 103.10 | 104. | 3 104 8 105 0 105 | 9 105 | 5.3 10 | 25.8 | 106.2 106.7 106.11 | 106.8 107.0 107.5 | 107.1 | 107.7 | 108.1 | 108.0 | 100.0 | 100.0 | 100.11 | 110.5 | 110.11 | 111.5 | 111.10 | 112.4 | 113.3 | 113.3 | 113.0 |
| 18 \$ 2 | 11.02 | 104.0 | 104.5 | 104.11 | 105. | 5 106. 10 106 2 106 | | 7 | 77.3 | 107.9 | 107.10 | 108.8 | | 109.3 | 110.2 | 110.7 | 111.1 | 111.7 | 112.1 | 112.6 | 113.0 | 113.0 | 113.7 | 114.5 | 114.0 | 115.0 |
| 11 10 10 10 10 10 10 10 10 10 10 10 10 1 | 8 4 | 105.6 | 100.0 | 100.5 | 100 | 107. | 5 107 | 1.6 10 | 8.5 | 108.6 | 109.0 | 109.6 | 100.4 | 110.00 | 110.11 | 111.50 | 111.11 | 112.4 | 112.30 | 113.4 | 113.70 | 114.4 | 11410 | 115.8 | 13.0 | 116.3 110.8 |
| 11 10 10 10 10 10 10 10 10 10 10 10 10 1 | 0 12 | 100.3 | 100.9 | 107.3 | 107. | 108 | 2 108 | 8 10 | 0.7 | 100.8 | 110.7 | 110.8 | 111.6 | 111.7 | 112.6 | 112.7 | 113.6 | 113.7 | 114.1 114.0 114.11 | 114.7 | 115.1 | 115.6 | 116.0 | 116.6 | 117.0 | 117.6 |
| Trum to Fort and 's an Inch by to foot and 's an Inch to II Foot by II Foot F. I. F | 11 | 107.4 | 107.10 108.3 108.7 | 108.4 | 108.1 | 0 100. 3 100. 7 110 | 9 110 | 3 11 | 0.4 | 110.10 | 111.4 | 111.10 | 112.4 | 112.10 | 113.4 | 113.10 | 114.4 | 114.0 | 115.3 | 115.0 | 116.3 | 110.9 | 117.3 | 117.0 | 118.3 | 118.0 |
| Trum to Fort and 's an Inch by to foot and 's an Inch to II Foot by II Foot F. I. F | 12.02 | 108.0 | 109.5 | 109.0 | 110. | 5 110. | 0 111 | .5 11 | 11.6 | 112.0 | 112.6 | 113.5 | 113.6 | 114.5 | 114.0 | 115.5 | 115.11 | 116.5 | 116.11 | 117.0 | 117.6 | 118.0 | 118.11 | 119.0 | 119.11 | 120.0 |
| Trum to Fort and 's an Inch by to foot and 's an Inch to II Foot by II Foot F. I. F | 1 42 | 100.8 | 110.3 | 110.8 | 111. | 1112. | 8 112 | 3 " | 3.8 | 13.7 | 113.8 | 114.2 | 114.8 | 115.7 | 115.8 | 110.2 | 110.8 | 117.2 | 117.0 | 118.7 | 118.0 | 119.3 | 10.0 | 120.3 | 120.9 | 121.3 |
| Trum to Fort and 's an Inch by to foot and 's an Inch to II Foot by II Foot F. I. F | 334 | 110.0 | 111.3 | 111.9 | 112. | 3 113 | 7 114 | 8 11 | 3.70 | 14.4 | 114.10 | 115.4 | 115.10 | 110.0 | 110.11 | 17.50 | 117.11 | 118.50 | 119.4 | 110.5 | 119.11 120.4 120.0 | 120.5 | 121.0 | 121.6 121.11 122.4 | 122.0 | 122.6 |
| From 10 Foot and \$ an Inch by 10 foot and \$ an inch to 11 Foot by 11 Foot FI F | 12.4% | 111.11 | 112.5 | 112.11 | 1137 | 0 114. | 11 114 | .6 11 | 5.4 | 15.0 | 110.0 | 116.6 | 117.1 | 117.7 | 118.1 | 118.7 | 119.6 | 110.7 | 120.2 | 120.8 | 121.2 | 121.8 | /22.2 /22.7 | /22.0 /23.2 | 123.3 | 123.0 |
| From 10 Foot and 2 an Inch by 10 foot and 2 an Inch to 11 Foot by 11 Foot F. I. F. | 6 | 113.8 | 113.0 | 114.1 | 114. | 115. | 1 115 | 7 11 | 6.3 | 16.8 | 17.2 | 117.8 | 118.3 | 118.9 | 118.3 | 16.6 | 120.4 | 120.10 | 121.4 | 121.10 | 122.5 | 122.11 | 123.5 | 123/1 | 124.6 | 125.0 |
| From 10 Foot and 2 an Inch by 10 foot and 2 an Inch to 11 Foot by 11 Foot F. I. F. | \$ | | 10/ | وعوراء | | 1000 | 68.6 | 3200 | | **** | 1 | **** | 111 | | | MIDDAME. | | | | 10 mm | | | 911 | 3 | | |
| From 10 Foot and 2 an Inch by 10 foot and 2 an Inch to 11 Foot by 11 Foot F. I. F. | | 2 | | | | The state of the s | | | | 1 | | | | | | | 2 W. T. | | | | 机 | | | 3 | | |
| F. I. | 2 | 10 | | 7.5.19 | | 1 | | Do | | | | | | | | | | | ~ | | | | | | 3 | , 100 (14, 100) |
| ElParts 10.0% 10.1 10.1% 10.2 10.2% 10.3 10.3% 10.4 10.4% 10.5 10.5% 10.6 10.0% 10.7 10.7% 10.8 10.9% 10.10 10.10% 10.11 10.11% 11.0 10.0% 10.13 101.8 102.1 102.0 102.0 102.1 103.4 103.0 103.4 103.0 104.3 104.8 10.5 10.5 10.4 10.0 10.0 10.1 10.1 10.1 10.1 10.1 | | F.I | FI | | | | | | | | | | | | | | | | | | | F.I | F.I | F. I | F.I | F.I |
| 0. 2 1/2 102.6 102.1 103.4 103.9 104.2 104.8 105.1 105.0 105.1 105.0 105.1 106.4 106.9 107.2 107.8 108.1 106.4 106.9 107.2 107.8 108.1 106.4 106.9 107.2 107.8 108.1 106.4 106.9 107.2 107.8 108.1 106.4 106.9 107.2 107.8 108.1 106.4 106.9 107.2 107.8 108.1 106.4 106.9 107.2 107.8 108.1 108.4 106.9 107.2 107.8 108.1 108.4 106.9 107.2 107.8 108.1 108.4 108.0 107.1 106.4 106.9 107.2 107.7 108.1 108.4 108.1 109.4 109.10 110.3 110.8 111.7 112.1 112.1 112.1 112.1 112.1 112.1 112.1 113.4 113.9 114.8 115.1 116.4 106.9 107.2 107.7 108.6 108.1 109.4 109.10 110.3 110.8 111.7 112.0 112.5 112.1 113.4 113.9 114.8 115.1 116.4 106.9 110.3 110.8 111.7 112.0 112.5 112.1 113.4 113.9 114.8 115.1 116.7 116.0 116.8 111.7 111.7 112.0 112.5 112.1 113.4 113.9 114.8 115.1 116.7 116.6 116.8 1 | FIParts | 10.05 | 10.1 | 10.12 | 10.2 | 10.2 | | | | | | | | | | | | | | | | | | | | |
| 0. 2 1/2 102.6 102.1 103.4 103.9 104.2 104.8 105.1 105.0 105.1 105.0 105.1 106.4 106.9 107.2 107.8 108.1 106.4 106.9 107.2 107.8 108.1 106.4 106.9 107.2 107.8 108.1 106.4 106.9 107.2 107.8 108.1 106.4 106.9 107.2 107.8 108.1 106.4 106.9 107.2 107.8 108.1 106.4 106.9 107.2 107.8 108.1 108.4 106.9 107.2 107.8 108.1 108.4 106.9 107.2 107.8 108.1 108.4 108.0 107.1 106.4 106.9 107.2 107.7 108.1 108.4 108.0 107.1 107.5 106.1 106.4 106.9 107.2 107.8 108.1 108.4 108.0 107.1 107.3 107.8 108.1 108.4 108.0 107.2 107.2 107.7 108.1 108.4 108.0 107.4 108.0 107.2 107.2 107.7 108.1 108.4 108.0 109.4 109.0 100.3 100.8 107.2 107.2 107.7 108.5 108.6 108.0 109.4 109.0 110.3 110.8 111.1 111.7 112.1 112.1 112.1 113.4 113.9 114.3 114.8 115.1 115.7 116.6 108.4 109.9 110.3 110.8 111.1 111.7 112.0 112.5 112.1 113.4 113.9 114.3 114.8 115.1 115.7 116.6 117.4 108.4 108.9 110.3 110.8 111.1 111.7 112.0 112.5 112.1 113.4 113.9 114.3 114.8 115.1 115.7 116.6 117.4 108.0 108.4 108.9 110.3 110.8 111.1 111.7 112.0 112.5 112.1 113.4 113.9 114.3 114.8 115.1 115.7 116.6 117.4 116.0 112.5 112.10 113.4 113.9 114.3 114.8 115.1 115.7 116.0 117.4 116.0 112.5 112.10 113.4 113.9 114.3 114.8 115.1 115.7 116.0 117.4 116.0 112.5 112.10 113.4 113.5 114.8 115.1 115.7 116.0 117.4 116.0 112.5 112.10 113.4 113.5 114.8 115.1 115.7 116.0 117.4 | 1 42 | 101.3 | 101.8 | 102.6 | 102 A | A S | | | | | | 7.7 | | | | | | | | | 1 a) ve | | | | * | 1 |
| 0. 4 \(\frac{1}{2} \) 104.7 \(\frac{1}{2} \) 105.0 \(\frac{1}{2} \) 107.7 \(\frac{1}{2} \) 108.0 \ | 10.212 | 102.6 | 103.4 | 103.4 | 103.0 | 104. | 105 | 8 10 | 5.11 | | | | | 24. | | | | | | | | | | | - 12 m | |
| 0.0 \(\frac{4}{2} \) 100,10 \(\frac{10}{6} \) 100,2 \(\frac{107.7}{100.7} \) 108.0 \(\frac{108.0}{100.4} \) 100,4 \(\frac{100.0}{100.4} \) 100.0 \(\frac{100.0}{100.3} \) 110.8 \(\frac{111.7}{111.7} \) 112.0 \(\frac{12.5}{112.11} \) 113.4 \(\frac{13.0}{13.4} \) 113.9 \(\frac{1}{13.4} \) 100.8 \(\frac{10.7}{100.7} \) 100.8 \(\frac{10.7}{100.7} \) 100.8 \(\frac{10.7}{100.7} \) 100.8 \(\frac{10.7}{100.7} \) 100.8 \(\frac{10.7}{100.4} \) 100.9 \(\frac{100.2}{100.3} \) 110.8 \(\frac{111.7}{111.7} \) 112.0 \(\frac{12.5}{112.11} \) 113.4 \(\frac{13.0}{13.4} \) 113.9 \(\frac{13.0}{14.3} \) 114.8 \(\frac{13.0}{15.7} \) 116.6 \(\frac{10.7}{100.7} \) 116.6 \(\fra | 10.4% | 103.9 | 104.2 | 104.7 | 105.0 | 105. | 1 106 | 4 100 | 6.9 10 | 08.9 07.2 N | 07.8 | 100 6 | | , | |),), | | | | | | e4. | | | | |
| 0.0 \(\frac{4}{2} \) 100,10 \(\frac{10}{6} \) 100,2 \(\frac{107.7}{100.7} \) 108.0 \(\frac{108.0}{100.4} \) 100,4 \(\frac{100.0}{100.4} \) 100.0 \(\frac{100.0}{100.3} \) 110.8 \(\frac{111.7}{111.7} \) 112.0 \(\frac{12.5}{112.11} \) 113.4 \(\frac{13.0}{13.4} \) 113.9 \(\frac{1}{13.4} \) 100.8 \(\frac{10.7}{100.7} \) 100.8 \(\frac{10.7}{100.7} \) 100.8 \(\frac{10.7}{100.7} \) 100.8 \(\frac{10.7}{100.7} \) 100.8 \(\frac{10.7}{100.4} \) 100.9 \(\frac{100.2}{100.3} \) 110.8 \(\frac{111.7}{111.7} \) 112.0 \(\frac{12.5}{112.11} \) 113.4 \(\frac{13.0}{13.4} \) 113.9 \(\frac{13.0}{14.3} \) 114.8 \(\frac{13.0}{15.7} \) 116.6 \(\frac{10.7}{100.7} \) 116.6 \(\fra | 34 | 104.7 105.0 105.5 | 105.0 | 105.0 | 105.1 106.4 106.9 | 100.5 | 107. | 7 10 | 7. 8 10 | 8.0 | 08.6 | 108.11 | 100.3 | 110.3 | | | | | | | , i | | | | | |
| 0 8 4 107. 6 108.0 108.3 108.0 100.4 100.0 110.2 110.8 111.1 111.7 112.0 112.5 112.11 113.4 113.0 114.3 114.8 115.1 115.7 116.6 110.8 110.7 111.0 112.5 112.0 113.4 113.0 114.3 114.8 115.1 115.7 116.6 110.8 110.7 111.0 111.0 112.5 112.0 113.4 113.0 114.3 114.8 115.1 115.7 116.0 116.6 110.8 110.7 111.0 111.0 111.0 112.5 112.0 113.4 113.0 114.3 114.8 115.1 115.7 116.0 116.6 110.11 117.4 | 7 4 | 105.10 100.3 100.8 | 100.0 | 100.0 | 107.2 107.7 108.0 | 107.7 | 7 108. 108. 108. | 16 100 | 3.11 10 | 0.4 | 00.4 10.3 10.3 | 100.10 | 110.3 | 110.8 | 112.0 | 112.5 | 112.11 | 112.0 | |) (1) (2) (3) | | * | | | | ` |
| 10 2 108.4 108.5 100.3 100.9 110.7 111.0 111.0 112.5 112.5 113.5 114.8 115.1 115.7 116.5 116.5 116.5 117.4 117.10 118.3 119.5 | 10.8% | 107.6 | 107.7 108.0 108.5 | 108.5 | 10810 | 100.1 | 100. | 2 110 | 2.2 11 | 0.8 | 11.6 | 12.7 | 112.0 | 112.5 | 112.11 | 113.4 | 113.0 | | 114.8 | 115.7 | 116.6 | 1 | | | | i k |
| 11 4 100.0 110.0 111.5 111.10 112.4 112.0 113.3 113.8 114.2 114.7 113.1 115.0 116.0 116.5 110.11 117.4 117.10 118.3 118.0 116.2 110.8 120.1 110.0 110.11 111.4 111.50 112.3 112.5 113.8 114.7 113.1 113.0 116.0 116.0 117.4 117.0 118.3 118.0 116.2 110.8 120.1 120.0 121.0 | 10.10% | 108.0 | 108.70 100.3 | 100.3 100.8 | 110.7 | 110.7 | 110. | 0 111 | 6 11 | 2.4 | 12.5 | 13.3 | 113.4 | 13.5 | 14.2 | 114.8 | 15.7 | 115.7 | 110.5 | 116.5 | 110.11 | 117.4 | 118.3 | | | , |
| | 11.0 | 100.7 | 110.1 | 110.0 | 111.0 | 111.1 | 0 112. | 9 113 | 2 0 11 | 3.3 | 3.3 | 13.9 | 114.7 | 13.0 | 15.0 | 116.0 | 10.5 | 110.5 | 117.4 | 17.10 | 118.3 | 18.9 | 10.2 | 10.8 | 20.0 | 121.0 |

The state of the s

A TABLE OF FEET AND INCHES From 11 Foot and & an inch by 10 Foot and & an inch to 12 Foot 6 Inches by 11 Foot

| | 1 | Fro | m 11 | Foot | ana | lia | n inci | h by | 10 F | rot a | nd i | an | inch | · w | /2 F | oot o | Inci | res v | y 11 1 | root | | | | |
|--|------------------------------------|--|-----------------------------------|------------------------------------|------------------------------------|-----------------------------------|-----------------------------------|----------------------------------|----------------------------------|--|---------------------------|--|------------------------------------|------------------------------------|------------------------------------|---|------------------------------------|------------------------------------|------------------------------------|-----------------------------------|----------------------------------|---------------------------------------|-----------------------------------|---------------------------|
| | F. I | Service Constitution of the Constitution of th | F.I | Rec Shidered | | to Const | Resident | F.I | F.I | F.I | F.I | F.I | F. I | F.I | F.I | F.I | E.I | F,I | F.I | F. I | F. I | F. I | F. I | FI |
| FIParts | 110.11 | 111.4 | 111.10 | 112.3 | 112.0 | 113:2 | 113.8 | | 10.42 | | | | | 110.10 | 117 4 | 117.0 | | | | 110.7 | BOOK SE | 120.0 | 121.0 | 121.5 |
| 2 2 | 111.0 | 112.7 | 113.4 | 113.6 | 13.7 | 114.0 | 114.0 | 114.11 | 115.30 | 113.11 | 116.4 | 116.10 | 117.3 | 117.0 | 117.0 | 118.8 | 119.7 | 120.0 | 120.0 | 121.0 | 121.0 | 121.10 | 122,4 | 122.4 |
| 11.25 | 113.5 | 113.0 | 113.11 | 114.4 | 114.5 | 113.4 | 115.0 | 115.0 116.3 116.8 | 110.3 | 117.7 | 117.8 | 118.7 | 18.7 | 10.0 | 120.0 | 1200 | 120.0 | 120.11 | 121.5 | 121.10 122.4 122.0 | 122.10 | 123.3 | 123.3 123.0 124.2 | 123.0 124.2 124.8 |
| 11.45 | 114.3 | 115.1 | 115.7 | 115.8 | 110.7 | 110.7 | 117.6 | 117.0 | 118.0 | 118.0 | 110.0 | 110.5 | 120.4 | 120.5 120.10 121.3 | 120.10 | 121. 4 | 121.10 | 122.3 | /22.0 /23.2 | /23.3 /23.8 | 123.8 124.2 124.7 | 124.2 124.8 | 124.8 | 125.1 |
| 11.02 | 115.6 | 115.0 | 116.5 | | 117.0 | 117.50 | 118.4 | 118:10 | 118.51 | 120.3 | 120.3 | 120.9 | | | | | | 123.7 | 124.7 | 124.7 124.7 125.0 125.0 | 125.0 | 125.0 120.0 126.5 | 123.7 120.0 120.0 120.11 | 120.6 |
| 7 % | 116.9 | 117.3 | 117.8 | 17.9 | 18.3 | 18.9.7 | 118.0 | 120.1 | 120.2 | 120.8 | 121.2 | 122.1 | | 123.0 | 123.6 | 124.0 124.5 | | 124.6 125.0 125.5 | 125.0 | 123.11 | 120,0 | 126.11 | 127.50 | 127.10 128.4 |
| 11.82 | 117.7 | 118.16 | 118.7 | 110 4 | 110.6 110.11 120.4 120.10 | 120 5 | 12011 | 121.5 | 121.6 | 12270 | 122.5 | 122.11 123.4 123.10 | 124.4 | 123.11 124.4 124.10 | 124 5 124 10 125 3 125 0 | 124.11 125.4 125.9 126.3 | 125:5 125:10 126:3 126:9 | 125,10 120,4 120,0 127,2 | 120.4 120.10 127.3 127.8 | 126.10 127.3 127.0 128.2 | 127.4 | 127.10 128.3 128.9 | 128.4 128.93 129.33 | 128.10 129.3 129.0 |
| 11.10 % | 118.70 | 119.9 | 120.3 | 120.4 | 121.3 | 121.9 | 121.9 | 122.8 | 122.9 123.2 123.8 | 123.8 | 123.9 124.3 124.8 | 124.3 124.8 125.1 | 124.9 | 125.8 | 125.9 126.2 126.7 | 120.3 126.8 127.1 127.7 128.0 | | | | - | 120.2 120.7 130.1 130.6 | 120.8 | 130.2 | 130.8 |
| 12.0 | 120.6 | 120.7 | 121.6 | 121.7 | 122.6 | 122.7 | 122.3 122.8 123.1 123.6 | 123.7 | 124.6 | 124.7 | 125.6 | 126.0 | 126.6 | 127.0 | 127.6 | 128.0 | | | | 130.0 | | | 131.1 | 132.0 |
| 12.04 | 120.11 121.4 121.0 122.2 | 122.3 | 122.0 | 122.10 123.3 123.8 | 123.4 | 123.10 124.3 124.8 | 123.11 124.4 124.9 125.3 | 124)0 125.3 125.9 | 125.4 | 125,10 126,4 120,9 | 120.10 120.10 127.3 | 126.10 127.4 127.9 | 120.11 127.5 127.10 128.3 | 127.11 128.4 128.9 | 127.11 128.5 128.10 129.3 | 128.5 128.11 120.4 129.9 | 128.11 120.5 120.10 130.3 | 120.5 120.11 130.4 130.10 | 120.11 130.5 130.10 131.4 | 131.11 | 130.11 | 131.41 132.4 132.10 | 132.5 132.10 133.4 | 132.Y1 133.4 133.10 |
| 12.25 | 122.7 | 123-1 | 123.7 | 124.1 | 124.7 | 125.2 | 125.8 126.1 126.6 126.11 | 126.7 | 126.8 | 127.2 | 127.8 | 128.2 128.7 | 128.8 | 120.2 | 120.9 | 130.3 130.8 | 130.0 | 131.3 | 131.0 132.2 132.8 | 132.3 132.8 133.2 | 132.0 133.3 133.8 | 133.3 133.9 134.2 | 133.9 134.3 134.8 | 134.3 134.0 135.2 |
| 12.45 | 123.10 | | 125.4 | | 125.11 | 120.5 | 127.4 | 127.5 | 127.11 | 128.0 | | 129.6 129.11 130.4 | 130.5 | 130.6 | 131.0 | 131.7 | 132.0 | 132.7 | 133.7 | 133.7 | 134.7 | 134.8 | 135.2 | 135.8 |
| 3,5 | 124.8 125.1 125.6 | 1757 | 125.2 | 120.3 120.8 127.1 | 126.4 126.0 127.2 127.7 | 127.3 127.8 128.1 | 128.3 128.8 | 128.4 128.9 129.2 | 128.50 128.30 129.8 | 120.4 | 130.4 | 130.10 131.3 | 131.4 | 131.10 | 132.10 | 133.4 | 133.30 | 133.11 | 134.5 | 135.0 | 135.0 | 136.6 136.5 | 36.6 137.0 | 37.0 |
| (2 | 9 | | | | -Ald | 15 T | | | | | CO | | | 1 | | | | | To the second | | === | R | 1 | |
| | | - AA | 4 | | | | NO. | Ċ. | | n L | | 52 | | | 4 | * | | ranto | | William . | | | | |
| | | T. B. | | | | 24 | | Va* | | | | | | | | * September | | | | | | ь чи | 1 |) |
| - | 7 | For | m // | Font | E | - | n Inc. | h /n | 117 | cat | O) - | Lan | inch | 5 | to 12 | foot | 61 | che | lu | 12 F | rot | | | |
| | F. I | F. I | | F.I | F.I | F. I | F. I | F.I | F. I | F.I | F. I | F.I | F.I | F. I | F. I | F.I | F, I | F. I | F.I | F. I | F. I | FI | F. I | F. I |
| F.I.Parts | | 11.1 | 11.15 | 11.2 | 11.25 | 11.3 | 11.35 | 11.4 | 11.45 | 11.5 | 11.5% | 11.6 | 11.6% | 11.7 | 11.75 | 11.8 | 11.8 | 11.9 | 11.95 | 11.10 | 11.10 | 11.11 | 11.112 | 12.0 |
| 11.0% | 121.11 122.5 122.10 123.4 | 122.10 | 123.0 | 124.8 | | | | 3 | | | | A - | •. | | | | | | | | | | | |
| 11.25 | 123.0 | 124.3 | 124.8 | 125.2 125.7 120.1 120.7 | 125.8 | 126.7 | 127.6 | | | | | | | | | | 1.0 | | | | | 7 | | 1 |
| 11.45 | 125.2 | 125.2 | 125.7 | 120.7 | 127.0 | 127.0 | 129 5 | 128.11 | 120.5 | .00 1 | | | | | | | | | | | | | | 4 |
| 3,2 | 120.1 126.6 127.0 | 127.0 | 127.0 | 127.0 127.11 128.5 | 128.0 128.5 128.11 | 128.5 | 120.5 | 120.50 120.10 130.4 | 130.10 130.4 130.10 | 130.4 130.10 131.3 | 131.4 | 132.3 | | | | | | (v.) (i) | | | | 32.4 | | 3.11 |
| 7 7 12 | 127.5 127.11 128.4 128.0 | 127.11 128.5 128.10 120.4 | 128.5 128.10 129.4 120.0 | 128.11 120.4 120.10 130.3 | 120.4 120.10 130.4 130.9 | 120.10 130.4 130.0 131.3 | 130.4 130.10 131.3 | 130.10 131.3 131.9 | 131.3 | 132.00 132.00 10.0 | 13330 | 132.0 133.8 133.8 | 33.3 | 134.2 | 135.2 | 136.1 | | | | | | | | |
| 11.8 % | 120.3 | 120.0 | 130.3 | 130.0 | 131.3 | 131.0 | 132.2 | /32.8 /33.2 | /33.2 /33.8 | 133.8 | 134.2 134.8 | 134.8 | 135.2 | 135.7 | 130.1 | 136.7 | 137.1 | 138.1 | 120 1 | | | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | | |
| 11.10 % | 130.2 | 131.7 | 131.8 | 132.7 | 132.8 | 133.7 | 133.7 | 134.7 | 134.7 | 135.1 | 135.7 | 136.7 | 136.7 | 137.7 | 137.7 | 138.1 | 138.7 139.4 | 138:0 | 140.0 | 140.0 | 141.0 | 440.0 | | |
| 12.0 | 131.7 132.0 132.0 | 132.0 | 132.7 133.0 133.0 | 133.1 133.0 134.0 | 133.7 134.0 134.0 | 134.6 135.0 | 134.7 135.0 135.0 | 135.1 135.0 130.0 | 135.7 136.0 136.6 | 136.6 137.0 | 130.7 137.0 137.0 | 137.0 137.6 138.0 | 37.0 38.0 138.6 | 138.0 138.0 139.0 | 138.0 139.0 139.0 | 130.0 130.0 140.0 | 130.0 140.0 140.0 | 140.0 140.6 141.0 | 140.0 141.0 141.0 | 141.0 141.0 142.0 | 141.0 142.0 142.0 | 42.6 43.0 | 143.0 143.6 | 144.0 |
| 12.0 % | 133.0 | 133.6 133.11 134.5 | 134.0 134.5 134.1 | 134.6 134.11 135.5 | 135.0 135.5 135.11 | 135.6 | 136.0 136.5 130.11 | 136.6 136.11 137.5 | 137.0 137.5 137.11 | 137.6 137.11 138.5 | 138.5 138.5 138.11 | 138.6 138.11 139.5 | 130.0 130.6 130.11 | 130.6 140.0 140.5 | 140.11 | | 141.0 141.0 142.0 | 41.6 42.0 142.6 | 142.0 142.0 143.0 | 142.6 143.0 143.0 | 143.0 143.0 144.0 | 143.6 144.0 144.0 | 144.0 144.0 145.0 | 144.0 145.0 145.0 |
| 12.25 | 134.4 | 13410 | 135.4 | 13510 136.4 136.0 | 130.4 | 137.4 | 137.5 137.10 138.4 | 137.71 138.4 138.10 | 138.5 138.10 130.4 | 138.11 130.5 130.10 | 130.5 130.11 140.4 | 139.11 140.5 140.10 | 140.5 140.11 141.5 141.10 | 140.11 141.5 141.11 142.5 | 141.5 | 142.5 | 142.11 143.5 143.11 | 143.5 | 143.11 144.5 | 144.0 144.0 144.11 | 145.0 | 145.6 140,0 | 40.0 46.0 | 140.6 147.0 |
| 3 4 | 135.2 | 136.8 | 130.5 | 137.3 | 37.0 | 138.9 | 138.10 | 138.10 139.4 130.9 | 130.10 | 140.10 | 140.10 | 141.10 | 144,4 | 14 230 | 143.4 | 143.11 | 144.5 | 144.5 | 145.5 | 145.5 | 140.0 | 147.0 | 47.0 47.0 | 148.0 |
| 3,4 | 30.8 | 737.7 738.7 | 138.7 138.7 130.1 | /38.8 /38.8 /30.7 | 30.8 30.8 | 130.3 130.2 140.7 | 140.2 140.8 141.2 | 140.3 140.0 141.2 141.8 | 140.0 141.3 141.0 142.2 | 141.9 141.9 142.8 142.8 | 142.3 142.9 143.3 | 142.0 | 142.10 143.4 143.0 144.3 | 143.10 144.4 144.9 | 144.4 144.10 145.4 | 144.4 144.10 145.4 145.10 | 145.5 145.10 146.4 | 145.71 146.5 146.50 | 146.5 146.11 147.5 | 140.11 147.5 147.11 | 147.5 147.11 148.5 | 48.0 48.0 149.0 | 4449 | 140.0 140.0 130.0 |
| و | 2 | A 1 | | of the control | C | 73 | | 1 | No. | 23 | | A CONTRACTOR OF THE PARTY OF TH | 65 | 35 | M | 30 | | 9_ | | | MAN ST | ites " | 3 | |
| | A AND A | | 2799 | | | | | | • | 2/ | 771 | | | | Man Angeleta | | | | | | 798 | 3 | 7 | , |
| | | THE HEALTH | | W. A. M | | | | | | | | danovil (1) | | THE CAN STORE | initias lebinum | Charles . | PARTY STATE | | | W. 100 | | | \$ - 1.00 miles | |
| \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\ | 9: | | | | 201 | -490 | inch | | O Far | | 1 + - | n [n | hm | 12 F | ot 6 | inch | 660 | 12 1 | ant f | Inc | her | <u> </u> | | |
| | F.I | - | 1 /2 F. I | | F.I | F.I | - | | - | - | F.I | - | - | I FO | | | 09 | | | I a | | | 1,0 | |
| FLParts | March Co. | | | | | | | The second second | | | | | | | | | | | | | • | | J | |
| 12.0% | 145.0 145.6 146.0 | 146.0 146.6 147.0 | 147.0 | 440.0 | | | | | | | | | | | | | | | | | | 3 | | |
| 12.25 3 5 | 147.0 147.0 | 147.0 147.0 148.0 | 48.0 | 148.0 148.0 140.0 140.7 | 140.1 | 150.1 | | *, ** | | | | £ . | | | | | | 4 | | * | | | | |
| 3 2 | 148.0 | 149.0 | 149.7 | 150.1 | 140.7 150.1 150.7 | 150.1 | OF ST. PR. ASSESSED. ASSES | 152.1 | 152.2 | | | | - | 1 | | | | | | | | 14. T | | |
| 55.5 | 140.0 140.0 150.0 | 150.0 150.0 151.0 | 150.1 150.7 151.1 151.7 | 150.7 151.1 151.7 152.1 | 151.7 152.1 152.7 | /52.7 /52.7 /53.1 | 152.1 152.7 153.2 153.8 | 153 2 153 8 154 2 | 153.8 154.8 | 154.2 154.8 155.3 | 155.3 | 1563 | | * | | | | | | . , . | | | | 4 |
| | | , | | | | i i | | | | | | | | 1. 7 | | | | | | | | | | |
| 100 | | | 70 | | | | | | | | 75000 | | | 3.55 | | 1 | - | 30000 | - | | | | | 1 |

49

A TABLE of FEET and INCHES.

From Half an Inch, by Half an Inch; to 228 Foot, by 11 Inches

| Color Colo | 82.6 91.8 16 83.3 92.6 16 83.4 93.4 16 83.4 93.4 16 83.6 95.0 16 83.6 95.0 16 83.7 95.0 16 83.6 98.4 16 83.7 99.2 16 83.6 98.4 16 99.2 16 99.2 16 99.3 160.6 | 0.11 99.11 100.10 101.9 102.8 103.7 104.6 105.5 106.4 107.3 108.2 109.1 110.0 110.11 111.10 112.9 113.8 114.7 115.6 116.5 117.4 118.3 119.2 120.1 121.0 121.11 122.10 123.8 124.8 125.7 126.6 127.5 128.4 |
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| Section Sect | 33.3 92.6 16 34.0 93.4 16 34.9 94.2 16 35.6 95.0 16 37.0 96.8 16 37.0 96.8 16 37.0 96.8 16 37.0 96.8 16 37.0 96.8 16 37.0 96.8 16 37.0 96.8 16 37.0 96.8 16 37.0 96.8 16 37.0 100.0 17 39.0 100.0 17 39.0 100.1 17 39.0 100.1 17 39.0 100.1 17 39.0 100.1 17 39.0 100.1 17 39.0 100.1 17 39.0 100.1 17 39.0 100.1 17 39.0 100.1 17 39.0 100.1 17 39.0 100.1 17 39.0 110.1 17 39.0 100.1 17 3 | 101.9 102.8 103.7 104.6 105.5 106.4 107.3 108.2 109.1 110.0 110.11 111.10 112.9 113.8 114.7 115.6 116.5 117.4 118.3 119.2 120.1 121.0 121.11 122.10 123.9 124.8 125.7 126.6 127.5 128.4 |
| According Column | 34.9 94.2 16.3 16.3 16.3 16.3 16.3 16.3 16.3 16.3 | 104.6 105.5 106.4 107.3 108.2 109.1 110.0 110.11 111.10 112.9 113.8 114.7 115.6 116.5 117.4 118.3 119.2 120.1 121.0 121.11 122.10 123.8 124.8 125.7 126.6 127.5 128.4 |
| Color | 37.0 96.8 10 37.9 97.6 16 38.6 98.4 16 39.9 97.6 16 39.0 100.0 17 99.0 100.10 17 99.1 101.8 17 99.2 102.6 17 99.3 102.6 17 99.4 105.0 17 99.5 105.10 17 99.6 108.4 17 99.0 100.0 17 99.0 110.0 17 99.0 17 99.0 17 99.0 100.0 17 99 | 106.4 107.3 108.2 109.1 110.0 110.11 111.10 112.9 113.8 114.7 115.6 116.5 117.4 118.3 119.2 120.1 121.0 121.11 122.10 123.9 124.8 125.7 126.6 127.5 128.4 |
| Company Comp | 88.6 98.4 16 89.3 99.2 16 99.0 100.0 1 99.6 101.8 1 99.3 102.6 1 99.3 102.6 1 99.4 105.0 1 99.5 105.10 1 99.6 105.0 1 99.6 105.0 1 99.6 106.8 1 109.1 105.0 1 99.9 110.10 1 99.9 110.10 1 99.9 110.10 1 113.4 1 102.0 113.4 1 105.0 113.4 1 105.0 115.10 1 105.0 115.8 1 105.0 115.10 1 105.0 116.8 1 105.0 118.4 1 107.3 119.2 1 08.9 120.10 1 08.9 120.10 1 09.9 120.10 1 09.9 110.3 1 110.3 1 110.3 1 120.0 1 10.3 1 110.3 1 110.3 1 110.3 1 110.3 1 | 109.1 110.0 110.11 111.10 112.9 113.8 114.7 115.6 116.5 117.4 118.3 119.2 120.1 121.0 121.11 122.10 123.9 124.8 125.7 126.6 127.5 128.4 |
| The property of the property | 90.9 100.10 11.8 12.6 11.0 12.6 11.0 12.6 11.0 12.6 11.0 12.6 11.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 | 110.11 111.10 112.9 113.8 114.7 115.6 116.5 117.4 118.3 119.2 120.1 121.0 121.11 122.10 123.9 124.8 125.7 126.6 127.5 128.4 |
| 1.0 1.5 | 93.0 103.4 1: 93.9 104.2 1. 93.9 104.2 1. 93.9 105.0 1: 95.3 105.10 1: 95.3 105.10 1: 96.9 107.6 1. 98.3 109.2 1: 99.9 110.10 1: 99.9 110.10 1: 99.9 110.10 1: 112.6 1: 02.0 113.4 1: 02.9 114.2 1: 03.6 115.0 1: 04.3 115.0 1: 05.0 116.8 1: 05.0 116.8 1: 05.0 117.6 1: 06.6 118.4 1: 07.3 119.2 1: 08.0 120.0 1: 08.9 120.0 1: 08.9 120.0 1: 09.6 1: 110.8 1: 1 | 113.8 134.7 115.6 116.5 117.4 118.3 119.2 120.1 121.0 121.11 122.10 123.9 124.8 125.7 126.6 127.5 128.4 |
| Color Colo | 994.6 105.0 15.0 15.0 15.0 15.10 15.0 15.0 15 | 115.6 116.5 117.4 118.3 119.2 120.1 121.0 121.11 122.10 123.9 124.8 125.7 126.6 127.5 128.4 |
| See A. | 96.9 107.6 197.6 108.4 198.3 109.2 199.0 110.0 1299.0 110.0 1299.0 110.1 120.0 113.4 120.2 115.0 120.0 116.8 120.0 116.8 120.0 116.8 120.0 | 118.3 119.2 120.1 121.0 121.11 122.10 123.9 124.8 125.7 126.6 127.5 128.4 |
| Time | 98.3 109.2 1299.0 110.0 1299.9 110.10 12.6 12.6 12.6 12.6 12.0 12.6 12.6 12.6 12.6 12.6 12.6 12.6 12.6 | 120.1 121.0 121.11 122.10 123.9 124.8 125.7 126.6 127.5 128.4 |
| 1-90 6.666 1.0 2.6 3.6 4.5 3.6 6.7 8.8 9.9 0.00 11.1 11.5 15.5 0.00 11.1 11.5 11.5 0.00 11.1 11.5 11.5 0.00 11.1 11.5 11.5 0.00 11.1 11.5 11.5 0.00 11.1 11.5 11.5 0.00 11.1 11.5 | 99.99 111.8 12.6 12.0 113.4 12.0 12.9 114.2 12.0 12.0 115.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0 12 | 122.10 123.9 124.8 125.7 126.6 127.5 128.4 |
| | 02.0 113.4 12 02.9 114.2 12 03.6 115.0 12 05.0 116.8 12 06.6 118.4 12 07.3 119.2 12 08.0 120.0 12 08.9 120.10 12 08.9 122.6 12 11.0 123.4 12 | 124.8 125.7 126.6 127.5 128.4 |
| 1. 1. 1. 1. 1. 1. 1. 1. | 04.3 115.10 12.05.0 116.8 12.05.0 117.6 12.05.0 120.10 120 | 127.5 |
| Section Sect | 05.9 117.6 120.0 120.10 | 700 0 |
| 1. 1. 1. 1. 1. 1. 1. 1. | 08.0 120.0 1 08.9 120.10 1 09.6 121.8 1 10.3 122.6 1 11.0 123.4 1 | 129.3 130.2 131.1 |
| 1. 1. 1. 1. 1. 1. 1. 1. | 09.6 121.8 1 10.3 122.6 1 11.0 123.4 1 | 132.0 |
| 350 1. & Color, 0 4-0 7.0 9-1 1-1 | | 133.10 134.9 135.8 |
| 320 1 4-60-23 0 5.4 | 12.6 125.0 1 | 136.7 |
| 1 | 14.0 126.8 1 | 138.5 139.4 140.3 |
| \$\frac{1}{3}\$\text{c}\$ \$\frac{1}{6}\$\tau\$ \$\f | 15.6 128.4 II. 16.3 129.2 II | 141.2 |
| 19.06 -7.66 5.0 6.6 6.99 10.0 13.4 15.8 20.0 23.9 35.0 23.9 35.0 23.9 37.4 15.8 20.0 37.4 20.0 | 17.9 130.10 1 | 143.0 143.11 144.10 |
| ### Also 1, 96.66 7, 0 6, 10 10.3 13.8 17, 1 10.6 43.0 11.6 10.6 44.0 17.1 11.0 43.8 13.6 31.0 | 19.3 132.6 1. 20.0 133.4 1. | 145.9 |
| 450 1.00.co. 3.0 7.4 11.0 13. 18.4 2.0 2.5 2.5 | 21.6 135.0 12 | 147.7 148.6 149.5 |
| 45.0 1.11.0.0-3;10.0 7.8 11.0 15.4 19.2 23.0 24.0 36.8 34.0 34.4 34.2 166.0 6.11.0 37.8 37.0 37.5 37.1 37.5 37. | 23.0 136.8 1 23.9 137.6 1 | 150.4 |
| 49.0 2. 0.66.4 1.6 8.2 12.3 16.4 20.5 26.0 30.5 36.0 39.2 33.4 33.4 37.5 41.8 33.1 37.5 41.8 33.1 37.5 41.8 33.1 37.5 41.8 33.1 37.5 41.8 33.1 37.5 41.8 33.1 37.5 41.8 33.1 37.5 41.8 33.1 37.5 41.8 33.1 37.5 41.8 33.1 37.5 41.8 33.1 37.5 41.8 33.1 37.5 41.8 33.1 37.5 41.8 37.5 | 25.3 139.2 1 | 152.2 153.1 154.0 |
| \$\frac{3}{5}\tau = \frac{2}{5}\tau = \frac{1}{5}\tau = \frac{1}\tau = \frac{1}{5}\tau = \frac{1}{5}\tau = \frac{1}{5}\tau = \frac{1}{5}\tau = \frac{1}{5}\tau = \frac{1}{5}\tau = \frac{1}{5}\ | 26.9 140.10 1 27.6 141.8 1 | 154.11 155.10 156.9 |
| \$\frac{1}{5}\frac{1}{6}\frac{2}{1}\$, \$\frac{1}{6} | 29.0 143.4 | 157.8 |
| \$7.0 2. 4.6.04 9.0 9.6 14.3 19.0 23.9 28.6 33.3 38.8 43.0 42.9 47.6 52.3 177.0 7. 4 14.9 29.6 44.5 19.4 24.2 29.0 33.10 38.8 43.0 48.4 33.2 177.0 7. 5 14.10 29.8 44.6 19.4 24.2 89.0 10.4 19.8 24.2 29.0 33.10 38.8 43.0 48.4 33.2 177.0 7. 5 14.10 29.8 44.6 19.4 44.6 19.8 47.0 10.0 | 30.6 145.0 16 | 159.6 160.5 161.4 |
| 90.0 2, 5.6.0, 17.0 0.70 14.9 16.9 20.0 35.0 30.0 35.0 40.0 44.3 40.2 54.1 179.0 7.5, 64.11.1 29.10 44.9 19.8 74.7 89.6 10.4 11.0 10.5 12.0 15.0 10.0 15.0 15 | 32.9 147.6 16 33.6 148.4 16 | 162.3 |
| 62.0 2. 7.00.65; 2.0 10.4 15.9 20.3 25.5 31.0 26.3 31.0 30.2 41.4 46.6 51.3 50.9 42.0 47.3 52.6 57.9 183.0 7. 7.6 15.3 30.4 45.6 60.8 75.10 20.6 20.9 122.0 10.6 4.0 2.8 8.0.65; 4.0 10.8 16.9 21.8 27.1 32.6 33.0 33.0 33.0 33.0 33.0 33.0 33.0 33 | 34.3 35.0 150.0 1 | 165.0 |
| 64.0 2. 8.6.0 5. 40 10.8 16.0 31.4 26.8 32.0 37.4 42.8 48.0 53.4 58.8 184.0 7. 8. 15.5 30.10 46.3 61.8 77.1 92.4 16.6 62.0 -9.0.6 56.0 11.0 16.6 22.0 -9.0.6 56.0 11.0 16.6 22.0 -9.0.6 56.0 11.0 16.6 22.0 -9.0.6 56.0 11.0 16.6 22.0 11.8 27.1 33.6 39.1 44.8 50.3 55.10 61.5 185.0 7. 9.0 15.6 51.0 46.6 62.0 77.6 93.0 10.8 18.0 11.4 17.0 22.8 28.4 34.0 39.8 45.4 51.0 56.8 62.4 188.0 7.10.0 15.8 31.4 47.0 62.8 78.4 49.0 19.8 125.4 17.0 22.8 28.9 34.6 40.3 46.5 52.6 58.4 64.2 190.0 7.10.0 15.8 31.4 47.0 62.8 78.4 49.0 199.8 125.4 17.0 2.11.60.5 11.0 11.0 12.5 41.5 41.5 47.4 53.3 59.2 60.0 66.1 199.0 7.11.0 15.0 31.8 47.0 63.4 79.9 95.0 111.0 127.4 17.0 2.18 6.0 51.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 1 | 36.6 151.8 16 37.3 152.6 16 | 166.10 |
| 67.0 2. 96.065. 7:011.2 16.9 22.4 27.11 33.6 39.1 44.8 50.3 55.10 61.5 187.0 7.9.6 15.7 31.2 46.9 62.4 77.11 93.6 10.9 10.9 10.9 10.9 10.9 10.9 10.9 10.9 | 38.9 154.2 16 | 168.8 |
| 75.0 3. 0.6.06. 1.0 12.2 18.3 24.4 30.5 36.6 42.7 17.0 3. 1.6.06. | 155.10 15 | 171.5 |
| 73.0 3. 0.0.66. 1.0 12.2 18.3 24.4 30.5 36.6 42.7 48.8 54.9 60.10 66.0 193.0 8. 0.0 16.0 32.0 48.0 64.8 80.5 96.6 112.7 128.8 174.0 3. 1.0.66. 2.0 12.4 18.6 24.8 30.10 37.0 43.2 49.4 55.0 61.8 67.10 194.0 8. 1.0 16.2 32.4 48.6 64.8 80.10 97.0 112.2 129.4 175.0 3. 1.6.66. 3.0 12.6 18.9 25.0 31.3 37.6 43.9 30.0 56.3 62.6 68.9 195.0 8. 1.6 16.3 32.6 48.9 65.0 81.3 97.6 113.9 130.0 57.0 63.4 192.0 193.0 8. 0.0 16.1 194.0 8. 1.0 16.2 32.4 48.6 64.8 80.10 97.0 112.2 129.4 175.0 194.0 8. 1.0 16.2 32.4 48.6 64.8 80.10 97.0 112.2 129.4 175.0 194.0 8. 1.0 16.2 32.4 48.6 64.8 80.10 97.0 112.2 129.4 175.0 194.0 8. 1.0 16.2 32.4 48.6 64.8 80.10 97.0 112.2 129.4 175.0 194.0 8. 1.0 16.2 32.4 48.6 64.8 80.10 97.0 112.2 129.4 175.0 194.0 8. 1.0 16.2 32.4 48.6 64.8 80.10 97.0 112.2 129.4 175.0 194.0 8. 1.0 16.2 32.4 48.6 64.8 80.10 97.0 112.2 129.4 175.0 194.0 8. 1.0 16.2 32.4 48.6 64.8 80.10 97.0 112.2 129.4 175.0 194.0 8. 1.0 16.2 32.4 48.6 64.8 80.10 97.0 112.2 129.4 175.0 194.0 8. 1.0 16.2 32.4 48.6 64.8 80.10 97.0 112.2 129.4 175.0 194.0 8. 1.0 16.2 32.4 48.6 64.8 80.10 97.0 112.2 129.4 175.0 194.0 8. 1.0 16.2 32.4 48.6 64.8 80.10 97.0 112.2 129.4 175.0 194.0 8. 1.0 16.2 32.4 48.6 64.8 80.10 97.0 112.2 129.4 175.0 194.0 8. 1.0 16.2 32.4 48.6 64.8 80.10 97.0 112.2 129.4 175.0 130.0 112.0 112.0 112.0 128.0 112.0 1 | 2.6 158.4 17 3.3 159.2 17 | 173·3 174.2 175·1 |
| 74.0 3. 1.0.06. 2.0 12.4 18.6 18.9 25.0 31.3 37.0 43.2 49.4 55.6 61.8 68.9 195.0 8. 1.616.3 32.6 48.9 65.0 65.4 13.9 130.0 130.8 113.9 130.0 130.8 113.9 130.0 130.8 113.9 130.0 130.8 113.9 130.0 130.8 113.9 130.0 130.8 113.9 130.0 130.8 113.9 130.0 130.8 113.9 130.0 130.8 113.9 130.0 130.8 113.9 130.0 130.8 113.9 130.0 130.8 113.9 130.0 130.8 113.9 130.0 130.8 113.9 130.0 130.8 113.9 130.0 130 | 4.9 160.10 17 | 176.0 |
| 77.0 3. 2.6.06. 5.0 12.10 19.3 25.8 32.1 38.6 44.11 51.4 57.9 64.2 70.7 71.6 19.0 3. 3.0.6 6.6 13.0 19.6 26.0 32.6 39.0 45.6 52.0 58.6 65.0 71.6 198.0 8. 3.6 16.7 33.2 49.9 66.8 82.1 19.9 26.4 32.11 39.6 46.1 53.8 59.3 65.10 72.5 19.0 8. 3.6 16.7 33.2 49.9 66.8 82.1 19.9 26.4 32.11 39.6 46.1 53.8 59.3 65.10 72.5 19.0 8. 3.6 16.7 33.2 49.9 66.8 82.1 19.9 26.4 32.11 39.6 46.8 53.4 60.0 66.8 73.4 20.0 46.8 53.4 60.0 66.8 73.4 20.0 19.0 8. 4.6 16.8 33.4 50.0 66.8 33.4 100.0 116.3 133.4 134.0 132.8 133.4 100.0 116.3 133.4 134.0 | 6.3 162.6 17 17.0 163.4 17 | 178.9 |
| 79.0 3. 3.0.00. 7.013.2 3.00. 7.013.2 3.00 | 8.6 165.0 18 | 180.7 181.6 182.5 |
| 82.0 3. 5.0.06.10.013.8 20.6 27.4 34.2 41.0 47.10 54.8 61.6 68.4 75.2 20.2 8. 5.016.10 33.8 50.6 67.4 84.2 101.0 117.10 134.8 1135.4 135.4 <td>50.0 166.8 18 50.9 167.6 18</td> <td>184.3</td> | 50.0 166.8 18 50.9 167.6 18 | 184.3 |
| 85.0 3. 6.6.07. 1.6 14.2 21.3 28.4 35.5 42.6 49.7 156.8 63.9 70.10 77.11 205.0 8. 6.617.1 34.2 51.3 68.4 85.5 102.6 119.7 136.8 18.4 18.5 10 103.0 120.2 137.4 151.6 68.8 85.10 103.0 120.2 137.4 151.6 68.8 18.5 10 103.0 120.2 137.4 151.6 68.8 18.5 10 103.0 120.2 137.4 151.6 137.4 151.6 137.4 15 | 52.3 169.2 18 | 185.2 186.1 187.0 |
| | 53.9 170.10 18 54.6 171.8 18 | 187.11 188.10 189.9 |
| 87.0 3: 7.6.07. 3.c 14.6 21.9 29.0 36.3 43.6 50.9 58.0 65.3 72.6 79.9 207.0 8. 7.617.3 34.6 51.9 69.4 36.8 103.0 120.4 138.8 18.0 3. 8.0 07. 4.0 14.8 22.0 29.4 36.8 44.0 51.4 58.8 66.0 73.4 80.8 208.6 8. 8.017.4 34.8 52.0 69.4 86.8 104.0 121.11 130.4 | 55.3 172.0 118 | 190.8 |
| 90.0 3. 9.0.07. 6.015.0 22.6 30.0 37.6 45.0 52.6 60.0 67.6 75.0 82.6 210.0 8. 9.017.6 35.0 52.6 70.0 87.0 105.0 122.0 140.8 91.0 3. 9.6.07. 7.015.2 22.9 30.4 37.11 45.6 53.1 60.8 68.3 75.10 83.5 211.0 8. 9.617.7 35.2 52.9 70.4 87.11 105.6 123.8 141.4 | 56.0 173.4 19 56.9 174.2 19 | 192.6 193.5 194.4 |
| 92.0 3.10.0.07. 8.015.4 23.0 30.8 38.4 46.0 53.8 61.4 69.0 76.8 84.4 212.0 8.10.017.8 35.4 53.0 70.8 88.9 106.6 124.3 142.0 93.0 3.10.6.07. 9.015.6 23.3 31.0 38.9 46.6 54.3 62.0 69.9 77.6 85.3 213.0 8.10.617.9 35.6 53.3 71.0 88.9 106.6 124.3 142.0 142.8 107.0 124.10 142.8 | 56.0 173.4 19 56.0 174.2 19 57.6 175.0 19 58.3 175.10 19 | 195.3 |
| 95.0 3.11.6.07.11.015.10 23.9 31.8 39.7 47.6 55.5 63.4 71.3 79.2 87.1 215.0 8.11.617.11 35.10 53.9 71.8 89.7 107.6 125.5 143.4 96.0 4.0.008. 0.016.0 24.0 32.0 40.0 48.0 56.0 64.0 72.0 80.0 88.0 216.0 9. 0.018.0 36.0 54.0 72.0 90.0 108.0 109.0 108.0 109.0 108.0 109.0 108.0 109.0 108.0 109 | 173.4 1956.0 174.2 1957.6 175.0 1958.3 175.10 1959.0 176.8 1959.0 177.6 160.6 178.4 1959.0 | 198.0 |
| 97.0 4. 0.6.0 8. 1.0 16.2 24.3 32.4 40.5 48.6 56.7 64.8 72.9 80.10 88.11 217.0 9. 0.6 18.1 30.2 54.3 72.4 90.5 108.6 120.7 144.5 98.0 4. 1.0.0 8. 2.0 16.4 24.6 32.8 40.10 49.0 57.2 65.4 73.6 81.8 89.10 218.0 9. 1.0 18.2 36.4 54.6 72.8 90.10 109.0 127.2 145.4 145.4 120.0 9. 1.6 18.3 36.6 54.9 73.0 91.3 109.6 127.9 146.0 | 56.0 173.4 19 56.9 174.2 19 57.6 175.0 19 58.3 175.10 19 59.0 176.8 19 60.6 178.4 16 61.3 179.2 16 62.0 180.0 19 | 199.10 |
| 100.0 4. 2.6.08. 4.016.8 25.0 33.8 42.1 50.6 58.1 67.4 75.9 84.2 92.7 221.0 9. 2.618.5 36.10 55.3 73.8 92.1 110.6 128.11 147.4 148.0 | 56.0 173.4 19 56.0 174.2 19 57.6 175.0 19 58.3 175.10 19 176.8 19 177.6 16 60.6 178.4 19 61.3 179.2 19 180.0 10 63.6 181.8 18 64.3 182.6 2 | 201.8 |
| 102.0 4. 3.0.08. 6.017.0 25.6 34.0 42.6 51.0 59.6 68.0 76.6 85.0 93.6 222.0 9. 3.018.6 37.0 55.6 74.0 92.0 111.6 129.0 148.8 103.0 4. 3.6.08. 7.017.2 25.9 34.4 42.11 51.6 60.1 68.8 77.3 85.10 94.5 223.0 9. 3.018.7 37.2 55.9 74.4 92.11 111.6 130.1 148.8 103.0 4. 4.0.08. 8.017.4 26.0 14.8 43.4 52.0 60.8 59.4 78.0 86.8 95.4 | 56.0 173.4 19 56.9 174.2 19 57.6 175.0 19 58.3 175.10 19 59.0 176.8 19 177.6 19 | 203.6 |
| 105.0 4. 4-6.0 8. 9.0 17.6 26.3 35.0 43.9 52.6 61.3 70.0 78.9 87.6 96.3 225.0 9. 4.6 18.9 37.6 56.3 75.0 93.9 112.6 131.3 150.8 106.0 4. 5.0.0 8.10.0 17.8 26.6 35.4 44.2 53.0 61.10 70.8 79.6 88.4 97.2 226.0 9. 5.0 18.10 37.8 56.6 75.4 94.2 113.0 131.10 150.8 | 56.0 173.4 195.0 174.2 195.0 175.0 195.0 176.8 176.3 176.3 176.3 176.2 166.6 178.4 166.3 179.2 166.0 180.0 166.6 181.8 166.3 182.6 183.4 182.6 184.2 185.0 186.8 185.0 186.8 186.8 20.6 186.8 20.6 186.8 20.6 186.8 20.6 186.8 20.6 186.8 20.6 186.8 20.6 186.8 20.6 2 | 204.5 |
| 107.0 4. 5.6.c \$.11.017.10 26.9 35.8 44.7 53.6 62.5 71.4 80.3 88.2 98.1 227.0 9. 5.618.11 37.10 56.9 75.8 94.7 113.0 133.0 152.0 108.0 4. 6.0.09. 0.018.0 27.0 36.0 45.0 54.0 63.0 72.0 81.0 90.0 99.0 228.0 9. 6.019.0 38.0 57.0 76.0 95.0 114.0 133.0 152.0 | 56.0 173.4 195.6 174.2 195.7 175.0 195.8 175.0 195.8 195.9 177.6 195.9 177.6 195.9 177.6 195.9 177.6 195.9 180.0 | 204.5 |

A TABLE of FEET and INCHES.

From 229 Foot, by Half an Inch; to 468 Foot, by 11 Inches.

| A F. I. P. F. I. F. I. F. I | L) F. L F. L F. L | (F. I. F. I. F | i. (F. L. F. L. | F. I. P. F. I. | F. I. F. I. | F. L. F. L. | F. I. F. I. | F. L F. L | F. L F. L |
|--|---|---|---|--|---|--|---|--|---|
| F. I. O. O.I O.1 O.2 O.3 229.0 9. 6.619.1 38.2 57.3 | 76.4 95.5 114.6 | 0.7 0.8 | 0.9 0.10 0.11 1.9 190.10 209.11 | F. 1. 0. 0.1 0.1 349.014. 6.629.1 | 0.2 0.3 58.2 87.3 | 0.4 0.5 | 0.6 0.7 | 0.8 0.9 232.8 261.9 233.4 262.6 | 0.f0 0.11 290.10 319.11 |
| 230.0 9. 7.019.2 38.4 57.6 231.0 9. 7.619.3 38.6 57.9 232.0 9. 8.019.4 38.8 58.0 | 77 7 9010 11010 | 134.9 154.0 17 | 2.6 191.8 210.10 3.3 192.6 211.9 4.0 193.4 212.8 | 350.014. 7.029.2 351.014. 7.629.3 352.014. 8.089.4 | 58.4 87.6 58.6 87.9 58.8 88.0 | 117.0 146.3 | 175.6 204.2 175.6 204.9 176.0 205.4 | 234.0 263.3 234.8 264.0 | 291.8 320.10 292.6 321.9 293.4 322.8 |
| 233.0 9. 8.619.5 38.10 58.3 234.0 9. 9.019.6 39.0 58.6 235.0 9. 9.619.7 39.2 58.9 | 78.4 97.11 117.6 | 136.6 156.0 17 | 4.9 194.2 213.7 5.6 195.0 214.6 6.3 195.10 215.5 | 353.0 14. 8.629.5 354.0 14. 9.029.6 355.0 14. 9.629.7 | 58.10 88.4 59.0 88.6 59.2 88.6 59.4 89.0 | 118.4 147.11 | 176.6 205.11 177.0 206.6 177.6 207.1 178.0 207.8 | 235.4 264.9 236.0 265.6 236.8 266.3 237.4 267.0 | 294.2 323.7 295.0 324.6 295.10 325.5 296.8 326.4 |
| 236.0 9.10.019.8 39.4 59.0 237.0 9.10.019.9 39.6 59.3 238.0 9.11.019.10 39.8 59.6 | 79.0 98.9 118.6 | 138.3 158.0 17 138.10 158.8 17 | 7.0 196.8 216.4 7.9 197.6 217.3 8.6 198.4 218.2 | 356.014.10.029.8 357.014.10.629.9 358.014.11.029.10 | 59.6 89.5 59.8 89.6 | 119.0 148.9 | 178.6 208.3 179.0 208.10 179.6 209.5 | 238.0 267.9 238.8 268.6 239.4 269.3 | 297.6 327.3 298.4 328.2 299.2 329.1 |
| 239.0 9.11.619.11 39.10 59.9 240.0 10. 0.0 20.0 40.0 60.0 241.0 10. 0.6 20.1 40.2 60.3 | 80.4 100.5 120.6 | 140.7 160.8 18 | 9.3 199.2 219.1 0.0 200.0 220.0 0.9 200.10 220.11 | 359.0 14.11.629.11 360.0 15. 0.0 30.0 361.0 15. 0.630.1 | 60.0 90.0 60.2 90.0 60.4 90.0 | 120.0 150.0 | 180.6 210.7 181.0 211.2 | 240.0 270.0 240.8 270.9 241.4 271.6 | 300.10 330.11 |
| 242.0 10. 1.0 20.2 40.4 60.6 243.0 10. 1.6 20.3 40.6 60.9 244.0 10. 2.0 20.4 40.8 61.0 | 81.0 101.3 121.6 81.4 101.8 122.0 | 141.9 162.0 18 142.4 162.8 18 | 1.6 201.8 221.10 2.3 202.6 222.9 3.0 203.4 223.8 | 362.015. 1.030.2 363.015. 1.630.3 364.015. 2.030.4 | 60.8 91.0 | 121.0 151.3 | 181.6 211.9 182.0 212.4 | 242.0 272.3 242.8 273.0 | 302.6 332.9 303.4 333.8 |
| 245.0 10. 2.620.5 40.10 61.3 245.0 10. 3.020.6 41.0 61.6 247.0 10. 3.620.7 41.2 61.9 248.0 10. 4.020.8 41.4 62.0 | 82.0 102.6 123.0 82.4 102.11 123.6 | 143.6 164.0 18 144.1 164.8 18 | 3.9 204.2 224.7 4.6 205.0 225.6 5.3 205.10 226.5 | 365.015. 2.630.5 366.015. 3.030.6 367.015. 3.630.7 368.015. 4.030.8 | 61.0 91.6 61.2 91.6 61.4 92.6 | 122.0 152.6 | 183.0 213.6 183.6 214.1 184.0 214.8 | 243.4 273.9 244.0 274.6 244.8 275.3 245.4 276.0 | 304.2 305.0 335.6 205.10 306.8 337.4 |
| 249.0 10. 4.6 20.9 41.6 62.3 250.0 10. 5.6 20.10 41.8 62.6 251.0 10. 5.6 20.11 41.10 62.9 | 83.0 103.9 124.6 83.4 104.2 125.0 | 145.3 166.0 18 145.10 166.8 18 | 6.0 206.8 227.4 6.9 207.6 228.3 7.6 208.4 229.2 | 369.015. 4.6 30.9 370.015. 5.0 30.10 371.015. 5.6 30.11 | 61.6 92.6 61.8 92.6 61.10 92.6 | 123.0 153.9 123.4 154.2 | 184.6 215.3 185.0 215.10 185.6 216.5 | 246.9 276.9 246.8 277.6 247.4 278.3 | 307.6 338.3 308.4 339.2 309.2 340.1 |
| 252.0 10. 6.0 21.0 42.0 63.0 253.0 10. 6.6 21.1 42.2 63.3 254.0 10. 7.0 21.2 42.4 63.6 | 84.0 105.0 126.0 84.4 105.5 126.6 | 147.0 168.0 18 | 8.3 209.2 230.1 9.0 210.0 231.0 9.9 210.10 231.11 | 372.015. 6.031.0 373.015. 6.631.1 374.015. 7.031.2 | 62.0 93.0 62.2 93.0 62.4 93.0 | 124.0 155.0 | 186.0 217.0 186.6 217.7 187.0 , 218.2 | 248.8 279.9 | 310.0 341.0 310.10 341.11 311.8 342.10 |
| 255.c 10. 7.621.3 42.6 63.9 256.c 10. 8.021.4 42.8 64.0 257.0 10. 8.021.5 42.10 64.3 | 85.0 106.3 127.6 85.4 106.8 128.0 | 148.9 170.0 19 149.4 170.8 19 | 0.6 211.8 232.10 1.3 212.6 233.9 2.0 213.4 234.8 | 375.015. 7.631.3 376.015. 8.031.4 377.015. 8.631.5 | 62.6 93.9 62.8 94.0 | 125.0 156.3 | 187.6 218.9 | 250.0 281.3 | 312.6 343.9 313.4 344.8 |
| 258.0 10. 9.0 21.6 43.0 54.6 259.0 10. 9.6 21.7 43.2 64.9 260.0 10.10.0 21.8 43.4 65.0 | 86.0 107.6 129.0 86.4 107.11 129.6 | 150.6 172.0 19 151.1 172.8 19 | 2.9 214.2 235.7 3.6 215.0 236.6 4.3 215.10 237.5 5.0 216.8 238.4 | 378.015. 9.031.6 379.015. 9.631.7 380.015.10.031.8 | 63.0 94.6 63.2 94.9 63.4 95.0 | 126.0 157.6 | 189.6 221.1 | 252.0 283.6 252.8 284.3 | 315.0 346.6 315.10 347.5 316.8 348.4 |
| 261.0 10.10.621.9 43.6 65.3 262.0 10.11.0 21.10 43.8 65.6 263.0 10.11.621.11 43.10 65.9 | 87.0 108.9 130.6 87.4 109.2 131.0 | 152.3 174.0 19 152.10 174.8 19 | 5.9 217.6 239.3 6.6 218.4 240.2 7.3 219.2 241.1 | 381.015.10.6 31.9 382.015.11.0 31.10 383.015.11.631.11 | 63.6 95.3 | | 190.6 222.3 191.0 222.10 191.6 223.5 | 254.0 285.9 254.8 286.6 255.4 287.3 | 317.6 349.3 318.4 350.2 319.2 351.1 |
| 265.0 11. 0.022.0 44.0 66.0 265.0 11. 0.622.1 44.2 66.3 266.0 11. 1.022.2 44.4 66.6 | 88.0 110.0 132.0 | 154.0 176.0 19 154.7 176.8 19 | 8.0 220.0 242.0 8.9 220.10 242.11 9.6 221.8 243.10 | 384.0 16. 0.0 32.0 385.0 16. 0.6 32.1 386.0 16. 1.0 32.2 | 64.0 96.0 64.2 96.3 64.4 96.6 | 128.4 160.5 | 192.0 224.0 192.6 224.7 193.0 225.2 | 256.8 288.9 | 320.10 352.0 320.10 352.11 321.8 353.10 |
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| 291.012. 1.624.3 48.6 72.9 292.012. 2.024.4 48.8 73.0 293.012. 2.624.5 48.10 73.3 | 97.0 121.3 145.6 97.4 121.8 145.0 97.8 122.1 146.6 | 169.9 194.0 213 170.4 194.8 219 170.11 195.4 219 | 243.4 267.8 | 412.0 17. 2.0 34.4 | 68.6 102.9 68.8 103.0 | 137.4 171.8 | 206.6 240.11 | 274.0 274.8 309.0 275.4 309.9 | 342.6 376.9 343.4 377.8 344.2 378.7 |
| 294.012. 3.024.6 49.0 73.6 295.012. 3.624.7 49.2 73.9 296.012. 4.024.8 49.4 74.0 | 98.0 122.6 147.0 98.4 122.11 147.6 98.8 123.4 148.0 | 171.6 196.0 220 172.1 196.8 22 172.8 197.4 223 | 0.6 245.0 259.6 1.3 245.10 270.5 | 415.0 17. 3.6 34.7 416.0 17. 4.0 34.8 | 69.0 103.6 69.2 103.9 69.4 104.0 | 138.4 172.11 | 207.6 208.0 242.8 | 277.4 312.0 | 345.0 379.6 345.10 380.5 346.8 381.4 |
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| 313.013. 0.6 26.1 52.2 78.3 314.013. 1.026.2 52.4 78.6 315.013. 1.626.3 52.6 78.9 | 104.4 130.5 156.6 | 182.7 208.8 234 183.2 209.4 235 | .6 261.8 287.10 | 433.0 18. 0.636.1 434.0 18. 1.036.2 | 72.2 108.3 72.4 108.6 72.6 108.9 | 144.4 180.5 144.8 180.10 | 216.6 252.7 | 288.8 324.9 289.4 325.6 | 360.10 396.11 361.8 397.10 362.6 398.9 |
| 316.013. 2.026.4 52.8 79.0 317.013. 2.626.5 52.10 79.3 318.013. 3.026.6 53.0 79.6 | 105.0 131.3 157.6 105.4 131.8 158.0 105.8 132.1 158.6 | 183.9 210.0 236 184.4 210.8 237 184.11 211.4 237 185.6 212.0 238 | 9 264.2 290.7 | 436.0 18. 2.6 36.5 | 72.8 109.0 | 145.4 181.8 | 218.6 254.4 | 290.8 327.0 | 363.4 399.8 364.2 409.7 365.0 401.6 |
| 319.0 13. 3.626.7 53.2 79.9 320.0 13. 4.0 26.8 53.4 80.0 321.0 13. 4.6 26.9 53.6 80.3 | 106.0 132.6 159.0 106.4 132.11 159.6 106.8 133.4 160.0 | 186.1 212.8 230 186.8 213.4 240 | 265.10 292.5 266.8 293.4 | 439.018. 3.030.7 | 73.0 · 109.6 73.2 109.9 73.4 110.0 | 146.4 182.11 146.8 183.4 | 219.6 256.1 220.0 256.8 | 292.8 329.3 293.4 330.0 | 365.10 402.5 366.8 403.4 367.6 404.3 |
| 322.013. 5.026.10 53.8 30.6 323.013. 5.626.11 53.10 80.9 324.013. 6.027.0 54.0 81.0 | 107.0 133.9 160.6 107.4 134.2 161.0 107.8 134.7 161.6 108.0 135.0 162.0 | 187.3 214.0 240 187.10 214.8 241 188.5 215.4 242 189.0 216.0 243 | .6 268.4 295.2 .3 269.2 296.1 | 441.0 442.0 18. 5.036.10 443.0 18. 5.636.11 18. 6.037.0 | 73.8 110.6 73.10 110.9 74.0 111.0 | 147.4 184.2 | 221.0 257.10 221.6 258.5 | 294.8 331.6 295.4 332.3 | 368.4 405.2 369.2 406.1 370.0 407.0 |
| 325.013. 6.627.1 54.2 31.3 326.013. 7.027.2 54.4 81.6 327.013. 7.627.3 54.6 81.9 | 108.4 135.5 162.6 108.8 135.10 163.0 109.0 136.2 163.6 | 189.7 216.8 243 190.2 217.4 244 190.9 218.0 245 | .6 271.8 298.10 | 445.0 18. 6.6 37.1 446.0 18. 7.0 37.2 | 74.2 111.3 74.4 111.6 74.6 111.9 | 148.4 185.5 | 222.6 259.7 223.0 260.2 | 296.8 333.9 297.4 334.6 | 370.10 407.11 371.8 408.10 372.6 409.9 |
| 328.0 13. 8.0 27.4 54.8 82.0 329.0 13. 8.6 27.5 54.10 82.3 330.0 13. 9.0 27.6 55.0 \$1.6 | 109.4 136.8 164.0 109.8 137.1 164.6 110.0 137.6 165.0 | 191.4 218.8 246 191.11 219.4 246 192.6 220.0 247 | 9 274.2 301.7 | 448.0 18. 8.0 37.4 | 74.8 112.0 | 149.4 186.8 | 224.0 261.4 224.6 261.11 225.0 262.6 | 198.8 336.0 199.4 336.9 | 373.4 410.8 374.2 411.7 375.0 412.6 |
| 331.013. 9.627.7 55.2 82.9 332.013.10.027.8 55.4 83.0 333.013.10.627.9 55.6 83.3 | 110.4 137.11 165.6 110.8 138.4 166.0 | 193.1 220.8 248 193.8 221.4 249 194.3 222.0 249 | .3 275.10 303.5 .0 276.8 304.4 | 451.018. 9.637.7 452.018.10.037.8 452.018.10.637.9 | 75.2 112.9 75.4 113.0 | 150.4 187.11 150.8 188.4 151.0 188.9 | 225.6 263.1 226.0 263.8 | 338.3 | 375.10 413.5 376.8 414.4 |
| 334.013.11.027.10 55.8 83.5 335.013.11.627.11 55.10 83.9 336.014. 0.028.0 56.0 84.0 | 111.4 139.2 167.0 111.8 139.7 167.6 112.0 140.0 168.0 | 194.10 222.8 250 195.5 223.4 251 196.0 224.0 252 | .6 278.4 306.2 .3 279.2 307.1 | 454 0 18.11.0 37.10 | 75.8 113.6 | 151.4 189.2 | 27.0 264.10 127.6 265.5 | 03.4 341.3 | 377.6 415.3 378.4 416.2 379.2 417.1 380.0 418.0 |
| 337.014. 0.628.1 56.2 34.3 338.014. 1.028.2 26.4 34.6 339.014. 1.628.3 56.6 84.9 | 112.4 140.5 168.6 112.8 140.10 169.0 113.0 141.3 169.6 | 196.7 224.8 252 197.2 225.4 253 197.9 226.0 254 | 9 280.10 308.11 .6 281.8 309.10 282.6 210.9 | 457.019. 0.638.1 458.019. 1.038.2 459.019. 1.638.3 | 76.2 114.3 76.4 114.6 76.6 114.9 | 152.4 190.5 152.8 190.10 153.0 191.3 | 228.6 266.7 229.0 267.2 129.6 267.9 | 304.8 342.9 305.4 343.6 306.0 344.3 | 380.10 418.11 381.8 419.10 382.6 420.9 |
| 340.c 14. 2.028.4 56.8 85.0 341.c 14. 2.628.5 56.10 85.3 342.c 14. 3.028.6 57.0 85.6 | 113.4 141.8 170.0 113.8 142.1 170.6 114.0 142.6 171.0 | 198.4 226.8 255 198.11 227.4 255 199.6 228.0 256 | 283.4 311.8 9 284.2 312.7 6 285.0 313.6 | 460.0 19. 2.0 38.4 461.0 19. 2.6 38.5 462.0 19. 3.0 38.6 | 6.10 115.3 | 153.4 191.8 153.8 192.1 154.0 192.6 | 230.0 268.4 2 230.6 268.11 2 231.0 269.6 | 345.0 307.4 345.9 308.0 346.6 | 383.4 421.8 384.2 422.7 385.0 423.6 |
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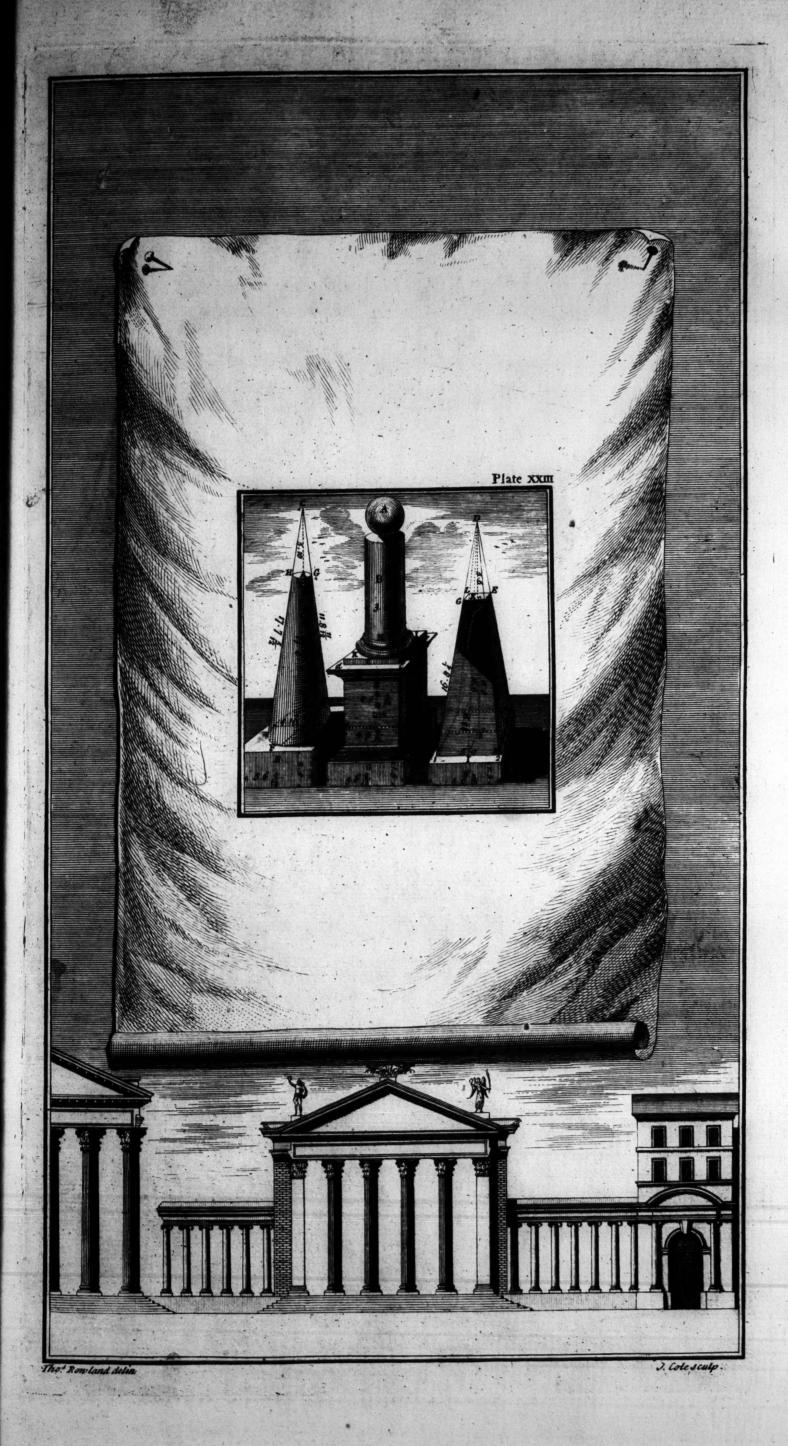
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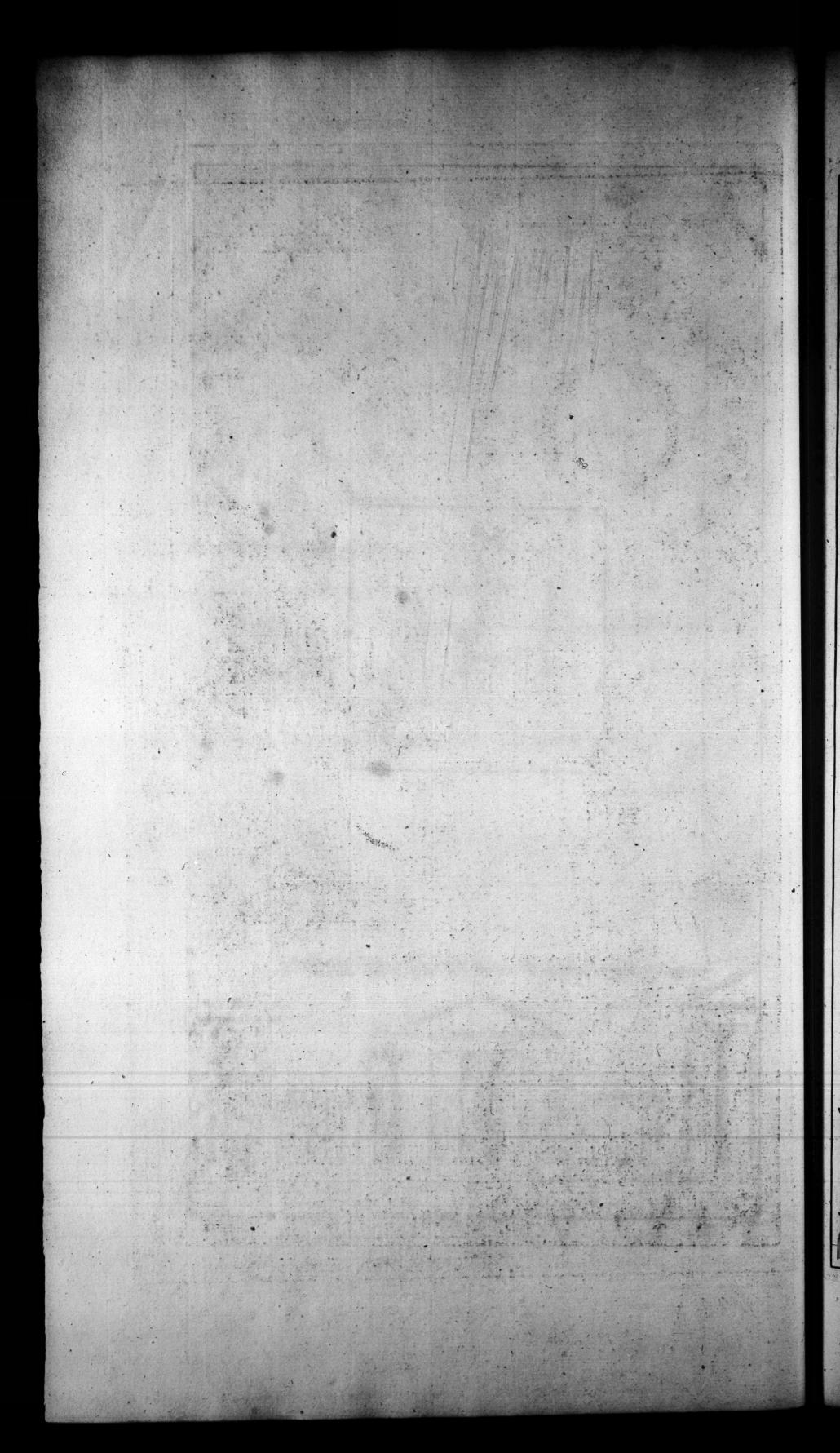
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| 17.0 | 221.0 | 238.0 | 255.0 | 272.0 | - | 324.0 | *8054 | 4000000 | A | 3804 .C | 0 / | 100 | 29.0 | 725.0 | 754.0 | 783.0 | 812.0 | 841.0 | 900.0 | 1 | | C 25 3 C 3 | | 1371 | |
| 19.0 | 247.0 | 266.0 | 285.0 | 304.0 | | 342.0 | 361.0 | 400.0 | .87.25 . | 1000 | | 10 4274 10 1011 | 31.0 | 775.0 | 806.0 | 837.0 | 868.0 | 899.0 | 930.0 | 961.0 | 1024.0 | in ngawarar in | | | |
| 21.0 | 273.0 | 294.0 | 315.0 | 336.0 | 357.0 | 378.0 | 399.0 | 420.0 | 441.0 | 66 | 2081 .68 | Ed April | 33.0 | 825.0 | 858.0 | 891.0 | 924.0 | 957.0 | 990.0 | 1023.0 | 1056.0 | 1089.0 | | | |
| 23.0 | 286.a | 308.0 | 345.0 | 308.0 | | 414.0 | 437.0 | 460.0 | 483.0 | 484.0 | 529.0 | 60 | 34.0 | 875.0 | 910.0 | 945.0 | 980.0 | 1015.0 | 1050.0 | 1085.0 | 1120.0 | 1155.0 | 1190.0 | 1225.0 | vao6 o |
| 25.0 | 325.0 | 350.0 | 375.0 | 400.0 | 425.0 | 450.0 | 456.0 | 500.0 | 525.0 | 550.0 | 575.0 | 576.0 | 37.0 | 925.0 | 962.0 | 999.0 | 1036.0 | 1073.0 | | 1147.0 | 1184.0 | 1188.0 | 1258.0 | 1295.0 | 1332.0 |
| 26.0 | 338.0 | 364.0 | 405.0 | 432.0 | 459.0 | 486.0 | | 540.0 | 567.0 | 572.0 | 598.0 | 648.0 | 38.0 | 975.0 | 1014.0 | 1053.0 | 1092.0 | 1131.0 | | 1209.0 | 1248.0 | 1254.0 | 1326.0 | Control of the Contro | 1404.0 |
| 28.0 | 377.0 | 406.0 | Contract Con | THE REAL PROPERTY. | - | The second division in | 532.0 | 580.0 | 609.0 | 616.0 | 667.0 | 696.0 | 41.0 | 1025.0 | 1066.0 | 107.0 | 1148.0 | 1189.0 | 1230.0 | 1271.0 | 1312.0 | | 1394.0 | 1435.0 | 1476.0 |
| 30.0 | 390.0 | 420.0 | 465.0 | 496.0 | 527.0 | 558.0 | 570.0 | 620.0 | 630.0 | 682.0 | 713.0 | 744.0 | 43.0 | 1075.0 | 1118.0 | 1161.0 | 1204.0 | 1247.0 | 1260.0 | 1333.0 | 1376.0 | 1419.0 | 1462.0 | 1505.7 | 1512.0 |
| 32.0 | 416.0 | 462.0 | | Military Cont. Market | 561.0 | - | 627:0 | 660.0 | 693.0 | 704.0 | 736.0 | 768.0 | 45.0 | 1125.0 | 1170.0 | 1215.0 | 1260.0 | 1305.0 | | 1395.0 | 1408.0 | | 1530.0 | 1575.0 | 1620.0 |
| 34.0 35.0 | 443.0 | 476.0 | 510.0 | 544.0 | | 100000000000000000000000000000000000000 | ELECTRONIC TOP AND ALKER | 700.0 | 714.0 | 748.0 | 782.0 | 816.0 | 47.0 | 1175.0 | 1222.0 | 1269.0 | 1316.0 | 1363.0 | 1410.0 | 1457.0 | 1472.6 | THE RESIDENCE OF THE PARTY OF | 1564.0 | | 1666.0 |
| 35,0 | 468.0 | 504.0 | - | 100000000000000000000000000000000000000 | - | MARKET WITH STREET | 703.0 | 720.0 | 756.0 | 792.0 | 828.0 | 864.0 | | | 1248.0 | | | | CONTRACTOR OF STREET | 1519.0 | 1536.0 | 1617.0 | 1666.0 | | 1764.0 |
| 38.0 | 494.0 | 532.0 | 570.0 | 608.0 | 646.0 | BCC030200.00000 | 722.0 | 760.0 | 798.0 | 836.0 858.0 | 874.0 | 912.0 | 51.0 | 1275.0 | 1326.0 | 377.0 | 1428.0 | 1479.0 | | 1581.0 | 1600.0 | 1650.0 | 1700.0 | 1785.0 | 1800.0 |
| 40.0 | 533.0 | 574.0 | 600.0 | Section 201 | AND DESCRIPTION OF THE PARTY OF | B. STORES | | 820.0 | 861.0 | 902.0 | 920.0 | 960.0 | | | - | | | The same of the same of | 1500.0 | | 1664.0 | | 1768.0 | 1820.0 | 1908.0 |
| 41.0 | 546.0 | 588.0 | 630.0 | 672.0 | 714.0 | 756.0 | 798.0 | 840.0 | 882.0 | 924.0 | 966.0 | 1008.0 | 54.0 | 1350.0 | 1404.0 | 1458.0 | 1512.0 | 1566.c | 1620.0 | 1674.0 | 1728.0 | 1782.0 | 1836.0 | 1890.0 | 1944.0 |
| 43.0 | 572.0 | 616.0 | 660.0 | 704.0 | 748.0 | 792.0 | 836.0 | 880.0 | 924.0 | 968.0 | 1012.0 | 1056.0 | 56.0 | 1400.0 | 1456.0 | 1512.0 | 1568.0 | 1624.0 | 1680.0 | 1736.0 | 1792.0 | 1848.0 | | | 2016.0 |
| 45.0 | 585.0 598.0 611.0 | | 675.0 690.0 705.0 | 736.0 | 782.0 | 828.0 | 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 920.0 | | 1012.0 | Section 1. The section of the sectio | 1104.0 | 58.0 | 1450.0 | 1508.0 | 1566.0 | 1624.0 | 1682.c | 1740.0 | 1798.0 | | 1914.0 | 1972.0 | 2030.0 | 2088.0 |
| 47.0 48.0 | 624.0 | 672.0 | 720.0 | 768.0 | 816.0 | 864.0 | 912.0 | 960.0 | 1008.0 | 1056.0 | 1104.0 | 1152.0 | 60.0 | 1500.0 | 1560.0 | 1620.0 | 1680.0 | 1740.0 | 1830.0 | 1860.0 | 1920.0 | 1980.0 | 2040.0 | 2100.0 | 2160.0 |
| 50.0 | 650.0 | 700.0 | 735.0 750.0 765.0 | 800.0 | 850.0 | 900.0 | 950.0 | 1000.0 | 1050.0 | 1100.0 | 1150.0 | 1200.0 | 62.0 | 1550.0 | 1612.0 | 1674.0 | 1736.0 | 1798.c | 1860.0 | 1922.0 | 1984.0 | | 2108.0 | 2170.0 | 2232.0 2268.0 |
| 51.0 | 676.0 | 728.0 | 780.0 | 832.0 | 884.0 | 936.0 | 988.0 | 1040.0 | 1092.0 | 1144.0 | 13. | 1248.0 | 64.0 | 1600.0 | 1664.0 | 1728.0 | 1792.0 | 1856.c | 1920.0 | 1984.0 | | 2112.0 | F254112 (15 5 12 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | | 2304.0 |
| 53.0 54.0 | 689.0 702.0 | | 810.0 | 864.0 | 918.0 | 972.0 | 1026.0 | 1080.0 | 1134.0 | NAME OF TAXABLE PARTY. | 1242.0 | 1296.0 | 66.0 | 1650.0 | 1716.0 | 1782.0 | 1848.0 | 1914.0 | 1980.0 | 2046.0 | 2112.0 | 2178.0 | | 2310,0 | 2376.0 |
| 55.0 | 715.0 | 784.0 | 840.0 | 896.0 | 952.0 | 1008.0 | 1064.0 | 1100.0 | 1176.0 | 1232.0 | 1288.0 | 1344.0 | 68.0 | 1700.0 | 1768.0 | 1836.c | 1904.0 | 1972.0 | 2040.0 | 2108.0 | The state of the s | 2244.0 | E INTERNATION DESIGNATION OF THE PERSON OF T | 2380.0 | 2448.0 |
| 57.0 | 741.0 | 812.0 | 855.0 | 928.0 | 986.0 | 1044-0 | 1083.0 | 1160.0 | 1218.0 | 1254.0 | CONSTRUCTOR AND | 1392.0 | 70.0 | 1750.0 | 1820.0 | 1890.0 | 1960.0 | 2030.0 | 2100.0 | 2170.0 | 2240.0 | 2310.0 | | 2450.0 | 2520.0 |
| 59.0 | 767.0 780.0 | 840.0 | 900.0 | 944.0 | 1003.0 | 1080.0 | 1140.0 | 1180.0 | 1200.0 | 1320.0 | 1380.0 | 1440.0 | 72.0 | 1800.0 | 1872.0 | 1944.0 | 2016.0 | 2088.c | 2160.0 | 2232.0 | 2304.0 | 2376.0 | 2448.0 | 2520.0 | 2592.0 |
| 61.0 | 793.c 806.c | 854.0 | 930.0 | 992.0 | 1037.0 | 1116.0 | 1178.0 | 1240.0 | 1302.0 | | 1403.0 | 1488.0 | 74.0 | 1850.0 | 1924.0 | 1998.0 | 2072.0 | 2146.c | 2190.0 | 2294.0 | 2368.0 | 2409.0 2442.0 | 2516.0 | 2590.0 | 2628.0 2664.0 |
| 63.0 64.0 | 819.c 832.c | | | | | | | 1280.0 | | | | 1512.0 | 76.0 | 1900.0 | 1976.0 | 2052.0 | 2128.6 | 2204.0 | 2280.0 | 2356.0 | 2432.0 | 2508.0 | 2550.0 2584.0 | 2660.0 | 2700.0 2736.0 |
| 65.0 | 845.c 858.c | | | | 1105.0 | | | AND THE RESERVE OF THE PERSON NAMED IN | | 1430.0 | | 1584.0 | 78.0 | 1950.0 | | 0.0015 | 2184.0 | 2262.0 | 2340.0 | 2418.0 | 2496.0 | 254110 257410 | 2652.0 | 2730.0 | 2772.0 |
| 67.0 68.0 | 871.c 884.c | 938.0 | 1005.0 | 1072.0 | 1139.0 | 1206.0 | 1273.0 | | | 1474.0 | The state of the s | 1632.0 | | | | | | | 2370.0 2400.0 | . 0 | 2523.0 | | 2720.0 | -0 | 2844.0 2880.0 |
| 69.0 | 897.0 | 100000000000000000000000000000000000000 | P.O. B. | CHARLEST THE COLUMN | 1173.0 | TOTAL SECTIONS | MENT LYCHTONICA | 1380.0 | | 1518.0 | | 1680.0 | | | | | | | 2430.0 2460.0 | | CO 200 200 CO CO | 7.3 | 7 00 | 2870.0 | 2952.0 |
| 71.0 | 923.0 | 994.0 | 1065.0 | 1136.0 | 1207.0 | 1278.0 | 1349.0 | 1420.0 | | 1562.0 | | 1704.0 | 84.0 | 2100.0 | 2184.0 | 2268.0 | 2352.0 | 2436.0 | 2520.0 | 2604.0 | | | 2822.0 2856.0 | 2905.0 | 3024.0 |
| 73.0 | 949.0 | 1022.0 | 1095.0 | 1168.c | 1241.c 1258.c | 1314.c | 1387.0 | 1460.0 | | 1606.0 | and the second | 1752.0 | 86.0 | 2150.0 | 2236.0 | 2322.0 | 2408.c | 2494.0 | 2550.0 2580.0 | 2000.0 | 2720.0 2752.0 | 2838.0 | 2924.0 | 212 | 3060.0 3096.0 |
| 74.0 75.0 76.0 | 975.0 | 1050.0 | 1125.0 | 1200.0 | 1275.c 1292.c | 1350.0 | 1425.0 | | 1575.0 | 1650.0 | BALL BALL TO THE | 1800.0 | 87.0 | 2175.0 | 2262.0 | 2349.c | 2436.0 | 2523.0 | 2610.0 2640.0 | 2097.0 | 2784.0 | 2871.0 | | | 3132.0 |
| 77.0 | 1001.0 | 1078.0 | 1155.0 | 1232.0 | 1309.0 | 1386.0 | 1463.0 | 1540.0 | 1617.0 | 1694.0 | 1771.0 | 1848.0 | 89.0 | 2225.0 | 2314.0 | 3403.0 | 2492.0 | 2581.0 | 2670.0 | 2759.0 | 2848.0 | 2937.0 | 3026.0 | 3115.0 | 3204.0 |
| 78.0 79.0 80.0 | 1027.0 | 1106.0 | 1185.0 | 1264.0 | 1326.c | 1422.0 | 1501.0 | 1580.0 | 1659.0 | 1738.0 | 1817.0 | 1896.0 | 91.0 | 2275.0 | 2366.0 | 2457.0 | 2548.C | 2639.0 | 2730.0 2760.0 | 2821.0 | 2912.0 2944.0 | 3003.0 | 3094.0 | - | 3276.0 |
| 81.0 | 1053.0 | 1134.0 | 1215.0 | 1296.0 | 1360.c | 1458.0 | 1539.0 | - | 1701.0 | 1782.0 | 1863.0 | 1944.0 | 93.0 | 2325.0 | 2418.0 | 2511.0 | 2604.0 | 2697.0 | | 2883.0 | 2976.0 | 3069.0 | | 3255.0 3290.0 | 3348.0 3384.0 |
| 83.0 | 1079.0 | 1162.0 | 1245.0 | 1328.0 | 1411.0 | 1494.0 | 1577.0 | 1650.0 | 1743.0 | 1826.0 | 1909.0 | 1992.0 | 95.0 | 2375.0 | 2470.0 2496.0 | 2565.0 | 2560.c | 275500 | 2850.0 | 2945.0 | 3040.0 | 3135.0 | 3230.0 | MESSAGES ILD TO LATER I | 3420.0 |
| 85.0 | 1105.0 | 1190.0 | 1275.0 | 1360.0 | 1445.c | 1530.0 | 1615.0 | 1700.0 | 1785.0 | 1870.0 | 1955.0 | 2040.0 | 97.0 | 2425.0 | 2522.0 2548.0 | 2619.0 | 2716.0 | 2813.0 | 2910.0 | 3007.0 | 3104.0 | | 3298.0 | 3395.0 | 3492.0 |
| 86.0 | 1131.0 | 1218.0 | 1305.0 | 1392.0 | 1479.0 | 1566.0 | 1653.0 | 1720.0 | 1827.0 | 1914.0 | 2001.0 | 2088.0 | 99.0 | 2475.0 | 2574.0 2600.0 | 2673.0 | 2772.0 | 2871.0 | 2970.0 | | 3168.0 | 3267.0 | 3366.0 | 3465.0 | 3564.0 |
| 88.0 | 1157.0 | 1246.0 | 1335.0 | 1424.0 | 1513.0 | 1602.0 | | | 1869.0 | 1958.0 | 2047.0 | 2136.0 | 101.0 | 2525.0 | 262 6. 0 | 2727.0 | 2828.c | 2929.0 | 3030.0 | 3131.0 | 3232.0 3264.0 | 3333.0 | 3434.0 | 3535.0 | 3636.0 3672.0 |
| 90.0 | 1183.0 | 1274.0 | 1365.0 | 1456.0 | 1547.0 | 1638.0 | 1729.0 | 1820.0 | | 2002.0 | 2093.0 | 2184.0 | 103.0 | 2575.0 | 2678.0 | 2781.0 | 2884.0 | 2987.0 | 3090.0 | 3193.0 | 3296.0 | 3399.0 | 3502.0 | 3605.0 | 3708.0 3744.0 |
| 93.0 | 1209.0 | 1302.0 | 1395.0 | 1488.0 | 1581.0 | 1674.0 | 1767.0 | 1860.0 | 1953.0 | 2046.0 | 2139.0 | 2232.0 | 105.0 | 2625.0 | 2730.0 2756.0 | 2835.0 | 2940.0 | 3045.0 | 3150.0 | 3255.0 | 3360.0 3392.0 | 3465.0 | 3570.0 | 3675.0 | 3780.0 3816.0 |
| 94.0 | 1235.0 | 1330.0 | 1425.0 | 1520.0 | 1615.0 | 1710.0 | 1805.0 | 1900.0 | 1995.0 | 2090.0 | 2185.0 | 2280.0 | 107.0 | 2675.0 | 2782.0 2808.0 | 2889.0 | 2996.0 | 3103.0 | 3210.0 | 3317.0 3348.0 | 3424.0 3456.0 | 2.0 | 3638.0 3672.0 | 3745.0 3780.0 | 3852.0 3888.0 |
| 97.0 | 1261.0 | P2 58.0 | 1455.0 | 155240 | 1649.0 | 1746.0 | 1343.0 | 1940.0 | 2037-0 | 2134.0 | 2231.0 | 2328.0 | 109.0 | 2725.0 | 2834.0 | 2943.0 | 3052.0 | 3161.0 | 3270.0 | 3379.0 | 3488.0 | 3597.0 | 3706.0 | 3815.0 | 3924.0 3960.0 |
| 98.0 99.0 | 1274.0 | 1372.0 1336.0 | 1470.0 | 1568.0 | 1666.c | 1764.0 | 1862.0 | 1980.0 | 2079.0 | 2178.0 | 2277.0 | 2352.0 | 111.0 | 2775.0 | 2860.0 2886.0 2912.0 | 2997.0 | 3108.0 | 3219.0 | 3330.0 | 3441.0 | 3552.0 3584.0 | 3663.0 | 3774.0 | 3885.0 | 3996.0 |
| 100.0 | 1313.0 | 1414.0 | 1515.0 | 1616.0 | 1717.0 | 1818.0 | 1919.0 | | 2121.0 | 2222.0 | 2323.0 | 2424.0 | 113.0 | 2825.0 | 2938.0 | 3051.0 | 3164.0 | 3277.0 | 3390.0 | | 3616.0 | 3729.0 | 3842.0 3876.0 | 3955.0 | 4068.0 |
| 102.0 | 1326.0 | 1428.0 | 1545.0 | 1632.0 | 1734.0 | 1836.0 | 1938.0 | 2040.0 | 2103.0 | 2200.0 | 2369.0 | 2472.0 | 115.0 | 2875.c | 2990.0 | 3105.0 | 3220.0 | 3335.0 | 3450.0 | 3534.0 3565.0 3596.0 | 3680.0 | 3795.0 | 3910.0 | 4025.0 | 1140.0 1176.0 |
| 105.0 | 1352.0 | 1456.0 | 1560.0 | 1664.0 | 1768.0 | 1872.0 | 1976.0 | | 2205.0 | 231010 | 2415.0 | 2520.0 | 117.0 | 2925.0 | 3042.0 | 3159.0 | 3276.0 | 3393.0 | 3510.0 | 3627.0 | 3744.0 | 3861.0 | 3978.0 | 4095.0 | 4212.0 4248.0 |
| 105.0 | 1378.0 | 1484.0 | 1500.0 | 1696.0 | 1802.0 | 1908.0 | 2014.0 | 2120.0 | 2226.0 | 2332.0 | 2438.0 2461.0 | 2544.0 2568.0 | 119.0 | 2975.0 | 3094.0 | 3213.0 | 3332.0 | 3451.0 | 3570.0 | 3689.0 | 3776.0 3808.0 3840.0 | 3927.0 | 4046.0 | 4165.0 | 1284.0 1320.0 |
| 109.0 | 1404.0 | 1512.0 | 1620.0 | 1728.0 | 1836.0 | 1944.0 | 2052.0 | 2160.0 | 2289.0 | 2376.0 | 2507.0 | 2592.0 | 121.0 | 3025.0 | 3146.0 | 3267.0 | 3388.0 | 3509.0 | 3630.0 | 3751.0 | 3872.0 | 3993.0 | 4114.0 | 4235.0 | 4356.0 |
| 111.0 | 1430.0 | 1540.0 | 1665.0 | 1760.0 | 1870.0 | 1980.0 | 2100:0 | 2200.0 | 2310.0 | 2420.0 | 2530.0 | 2004.0 | 123.6 | 2075.0 | 3198.0 | 3321.0 | 3444.0 | 3567.0 | 3660.0 | 3782.0 | 3936.0 | 4059.0 | 4148.0 | 4305.0 | 4392.0 |
| 112.0 | 1456.0 | 1568.c | 1605.0 | 1792.0 | 1904.0 | 2016.0 | 2128.0 | 2240.0 | 2352.0 | 2464.0 2486.0 | 2570.0 | 2712.0 | 1250 | 2125.0 | 2250.0 | 2275.0 | 2500.0 | 2625.0 | 3720.0 | 2875.0 | 4000.0 | 1125.0 | 4250.0 | 4375.0 | 4500.0 |
| 114.0 | TA82-C | T c06.0 | 1710.0 | 1824.0 | 1028.0 | 2052.0 | 2166.0 | 2280.0 | 2415.0 | 2508.0 | 2645.0 | 2730.0 | 125.0 | 3150.0 | 3276.0 | 3402.0 | 3528.0 | 3654.0 | 3780.0 | 3900.0 | 1064.0 | 4191.0 | 4284.0 | 4445.0 | 4530.0 |
| 116.0 | 1508.0 | 1624.0 | 1740.0 | 1856.0 | 1972.0 | 2106.0 | 2204.0 | 2320.0 | 2436.0 2457.0 | 2552.0 | 2008.0 | 2784.0 | 128.0 | 3200.0 | 3328.0 | 3450.0 | 3584.0 | 3712.0 | 3840.0 | 3999.0 | 4128.0 | 1257.0 | 4352.0 | 4515.0 | 4644.0 |
| 117.0 | 1534.0 | 1652.0 | 1770.0 | 1888.0 | 2006.0 | 2124.0 | 2242.0 | 2360.0 | 2478.0 | 2596.0 | 2714.0 | 2832.0 | 130.0 | 3250.0 | 3380.0 | 3510.0 | 3640.0 | 3770.0 | 3930.0 | 4030.0 | 4160.0 | 4290.0 | 4420.0 | 4550.0 | 4680.0 |
| 119.0 | 1560.0 | 1680.0 | 1800.0 | 1920.0 | 2040.0 | 2160.0 | 2280.0 | 2400.0 | 2520.0 | 2640.0 | 2700.0 | 2880.0 | 132.0 | 3300,0 | 3432.0 | 3564.0 | 3696.0 | 3828. | 3960.0 | 4092.0 | 4256.0 | 1350.0 | 4522.0 | 4655.0 | 4;83.0 |
| | 1586.0 | 1708.C | 1840.0 | 1052.0 | 2057.0 | 210b.c | 2318.0 | 2440.0 | 2541.0 2562.0 2583.0 | 2684.0 | 2806.0 | 2928.0 | 134.0 | 3350.0 | 3484.0 | 3618.0 | 3752.0 | 3880. | 1020.0 | 4154.0 | 4288.0 | 4422.0 | 4556.0 | 4.690.0 | 1860.0 |
| 123.0 | 1612.0 | 1736.0 | 1860.0 | 1984.0 | 2108.0 | 2232.0 | 2337.0 | 2480.0 | 2604.0 | 2728.0 | 2852.0 | 2976.0 | 136.0 | 3400.0 | 3530.0 | 3672.0 | 3808.0 | 3944- | 4080.0 | 4210.0 | 4352.0 | 4488 0 | 4658.0 | 4705.0 | 4932.0 |
| | 1638.0 | 1764.0 | 1800.0 | 2016.0 | 2125.0 | 2268.0 | 2394-0 | 2520.0 | 2625.0 2646.0 | 2773.0 | 2898.0 | 3024.0 3048.0 | 138.0 | 3450.0 | 3588.0 | 3720.0 | 3864.0 | 4002. | 04140.0 | 4278.0 | 1416.0 | 4554-0 | 4692.0 | 4830.0 | 1968.0 |
| 127.0 | 766A.O | 1702.0 | 10200 | 2048.0 | 2176.0 | 2204-0 | 2413.0 2432.0 | 2560.0 | 2688.0 | 2816.0 | 2944.0 | 3072.0 | 140. | 3500.0 | 3040.0 | 3780.0 | 3920. | 4000. | 04200.0 | 14340.0 | 1400.0 | 4020.0 | 4700.0 | 490000 | 2040.0 |
| 129.0 | 1677.0 | 1806.c | 1935.0 | 2064.0 | 2193.0 | 2322.0 | 2451.0 | 2580.0 | 2730.0 | 2860.0 | 2990.0 | 3096.0 3120.0 3144.0 3168.0 | TAR | O 2 FTE | 012718.0 | Naxor. | 04004 | 04147 | 0 1200.0 | 14423.0 | 11570.0 | 14719.0 | 4794.0 4828.0 4862.0 | 10003.0 | 5112.0 |
| 131.0 | 1703.0 | 1834.0 1848.0 | 1985.0 | 2096.0 | 2244.0 | 2358.0 2376.0 | 2508.0 | 2640.0 | 2772.0 | 2904.0 | 3036.0 | 3168.0 | 144 | 03600. | 3744 | 3888. | 04032. | 4176 | 6 4320.0 | 4464.0 | 1608.0 | 4752.0 | 4896.0 | 5040.0 | 184.0 |
| - | - | Activity of the Asset | 1 | 11 | I con | an antein | Name and | house ! | Commence and | Contraction of | Lankin | Lucy | | a manage | | n committee | Andrews in the | - | - | P | 1 | 1 | - | 1 | and the state of |

From 133 Foot, by 13 Foot; to 252 Foot, by 2 From 145 Foot, by 25 Foot; bo 264 Foot, by 24 Foot, 36 Foot,

| | I, E. L. F. L. E. L. F. L. | 1 P. |
|--|--|--|
| 13.0 14.0 15.0 16.0 17.0 18.0 19.0 2 133.0 17.20 18.0 19.0 2 133.0 17.20 1862.0 1955.0 2128.0 2261.0 2304. 1527. 256 | 0.0 21.0 22.0 23.0 24.0 0. 2793. 2926. 3059. 3192. 0. 2814. 2948. 3082. 3216. | F. I. 25.0 26.0 27.0 28.0 29.0 30.0 31.0 32.0 33.0 34.0 35.0 36.0 36.0 36.0 36.0 36.0 36.0 36.0 36 |
| 135.0 1755.0 1890.0 2025.0 2160.0 2295.0 2434. 2565, 256.0 1768.0 1904.0 2040.0 2176.0 2312.0 2448, 2584. 272.0 1781.0 1918.0 2055.0 2192.0 2329.0 2466. 2603. 274 | | 147. 3675. 3822. 3969. 4116. 4263. 4410. 4557. 4704. 4851. 4998. 5145. 5922. 4440. 4582. 4736. 4884. 5032. 5180. 5228. 349. 3725. 3874. 4023. 4172. 4321. 4470. 4619. 4768. 4917. 5066. 5225. 5364. |
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| 160.0 2080.0 2240.0 2400.0 2500.0 2703.0 2862. 3021. 318 160.0 2080.0 2240.0 2400.0 2500.0 2720.0 2880. 3040. 320 161.0 2093.0 2254.0 2415.0 2576.0 2737.0 2898. 3059. 322 | 0. 3360. 3520. 3680. 3840. 0. 3381. 3542. 3703. 3864. | 172. 4300. 4472. 4644. 4816. 4988. 5160. 1332. 5504. 5676. 5848. 6020. 6192. 173. 4325. 4498. 4671. 4844. 5017. 5190. 5363. 5526. 5709. 5882. 6055. 6228 |
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| 188.0 2444.0 2632.0 2820.0 3008.0 3196.0 3384. 3572. 379 189.0 2457.0 2646.0 2835.0 3024.0 3213.0 3402. 3591. 379 | 80. 3969. 4158. 4347. 4536. | 200. 5000. 5200. 5400. 5600. 5800. 6000. 6400. 6600. 6800. 7000. 7200. 201. 5025. 5226. 5427. 5628. 5829. 6030. 6231. 6432. 6633. 6834. 7035. 7236. |
| 192.02496.0 2688.0 2880.0 3072.0 3264.0 3456. 3648. 384 | 20. 4011, 4202. 4393, 4584. 40. 4032. 4224. 4416. 4608. | 203. 5075. 5278. 5481. 5684. 5887. 6090. 6293. 6496. 6699. 6902. 7105. 7308 204. 5100. 5304. 5508. 5712. 5916. 6120. 6324. 6528. 6732. 6936. 7140. 7344 |
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| 203.02639.02842.03045.03248.03451.03654. 3857. 40 204.02652.02856.0300.03264.03468.03672. 3876. 40 | | 216. 5400. 5616. 5832. 6048. 6264. 6480. 6696. 6912. 7128. 7344. 7560. 7776 |
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| 209.0 2717.0 2926.0 3135.0 3344.0 3553.0 3762. 3971. 41 210.0 2730.0 2940.0 3150.0 3460.0 3570.0 3780. 3990. 42 211.0 2743.0 2954.0 3165.0 3376.0 3587.0 3798. 4009. 42 | 80. 4389. 4598. 4807. 5016. 00. 4410. 4620. 4830. 5040. | 221. 5525. 5746. 5967. 6188. 6409. 6630. 6851. 7072. 7293. 7514. 7735. 7996. 222. 5550. 5772. 5994. 6216. 6438. 6660. 6882. 7104. 7326. 7548. 7770. 7992. 223. 5575. 5798. 6021. 6244. 6467. 6690. 6913. 7136. 7359. 7582. 7805. 8028. 6000. 8824. 6048. 6690. 6913. 7136. 7359. 7516. 7840. 8068. |
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| 219.0 2847.0 3066.0 3285.0 3504.0 3723.0 3942. 4161. 43 220.0 2866.0 3080.0 3300.0 3520.0 3740.0 3960. 4180. 44 | 66. 4578. 4796. 5014. 5232. 86. 4599. 4818. 5037. 5256. 66. 4620. 4840. 5066. 5280. | 231. 5775. 6006. 6237. 6468. 6699. 6930. 7161. 7392. 7623. 7854. 8085. 8316 232. 5800. 6032. 6264. 6496. 6728. 6960. 7292. 7424. 7656. 7888. 8120. 8352 |
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| 225.c 2925.c 3150.c 3375.c 3600.c 3825.c 4050. 4275. 4575. 458.c 226.c 2938.c 3164.c 3390.c 3616.c 3842.c 4068. 4294. 4594. | 00. 4725. 4950. 5175 5400. 20. 4746. 4972. 5198. 5424. | 237. 5925. 6162. 6399. 6636. 6873. 7110. 7347. 7584. 7821. 8058. 8295. 8532. 238. 5950. 6188. 6426. 6664. 6902. 7140. 7378. 7616. 7854. 8092. 8330. 8568. 8295. 6214. 6452. 6602. 6021. 7170. 7409. 7648. 7887. 8126. 8365. 8604. |
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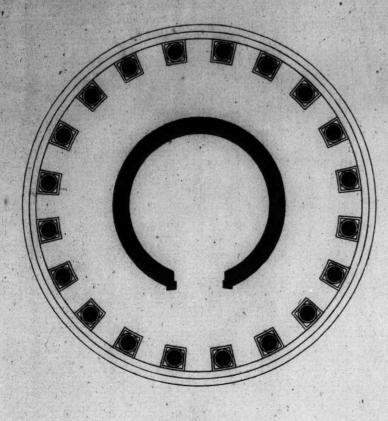


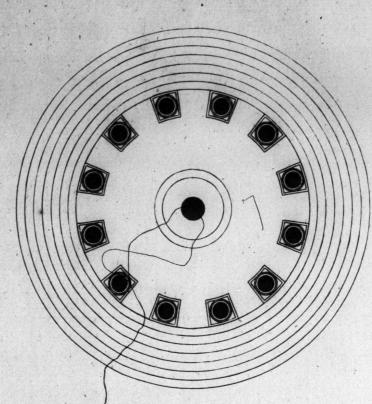
To face Page 30

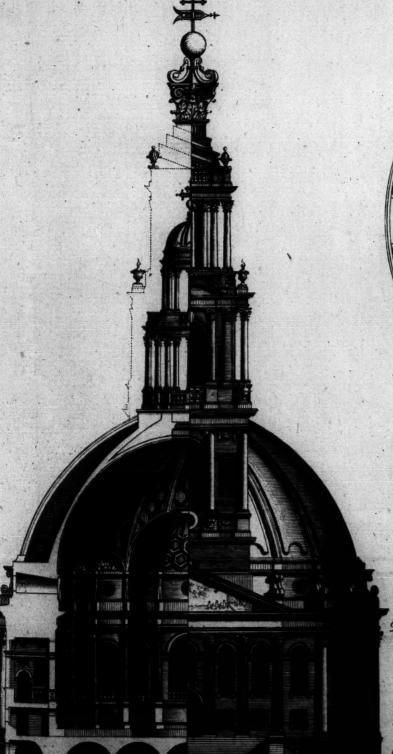
Plate 27

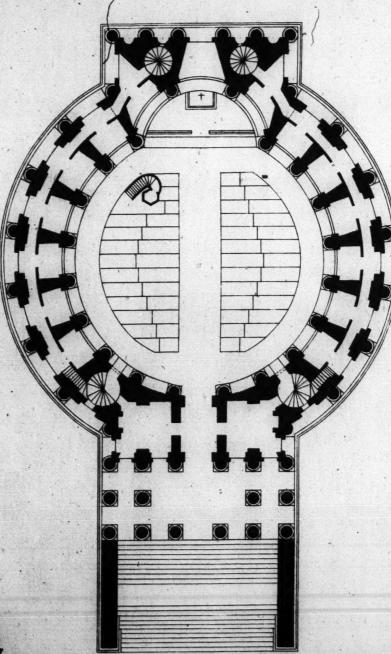
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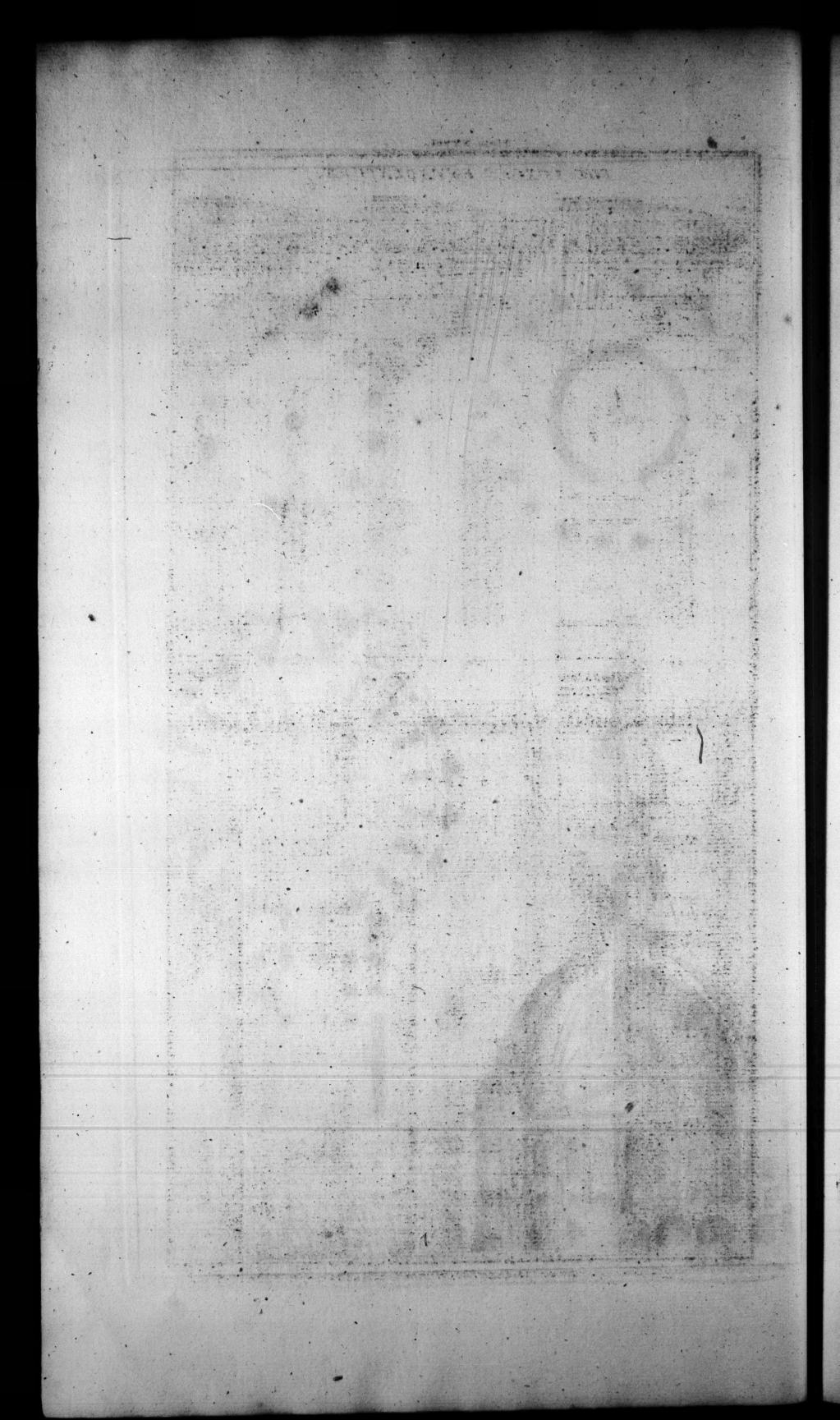


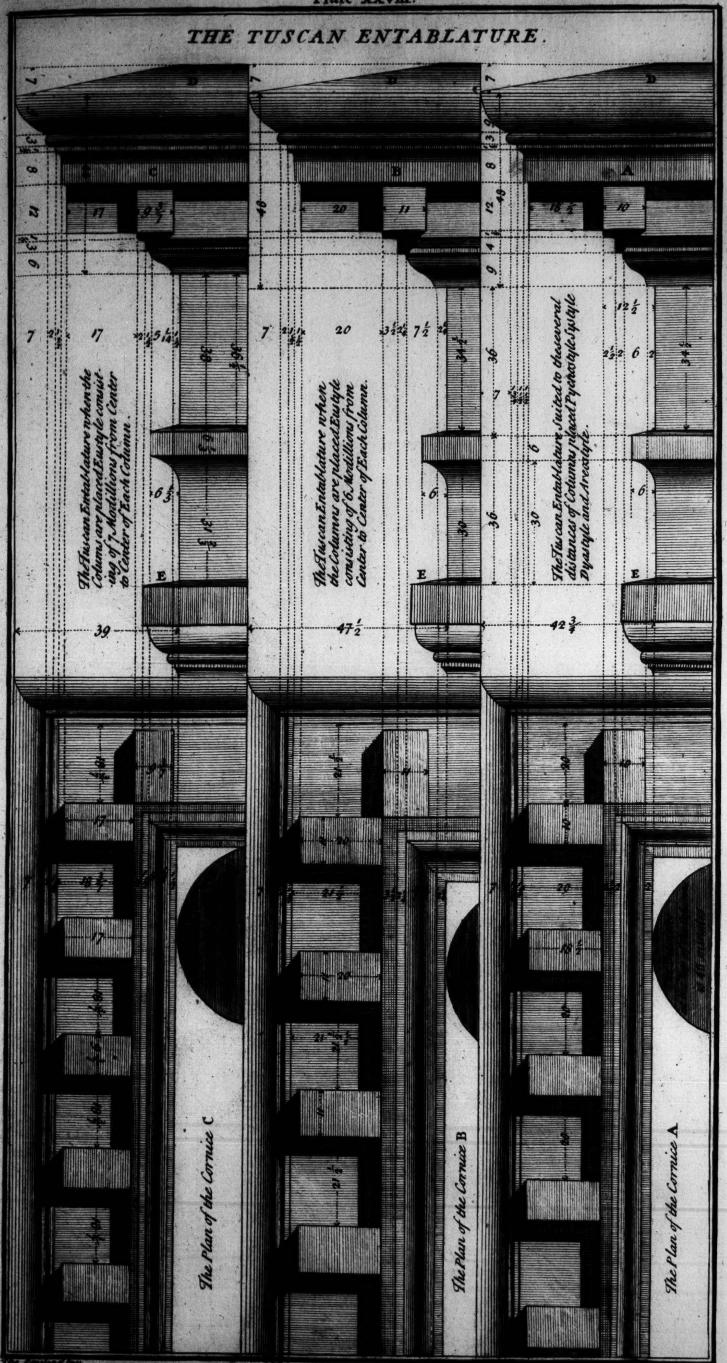


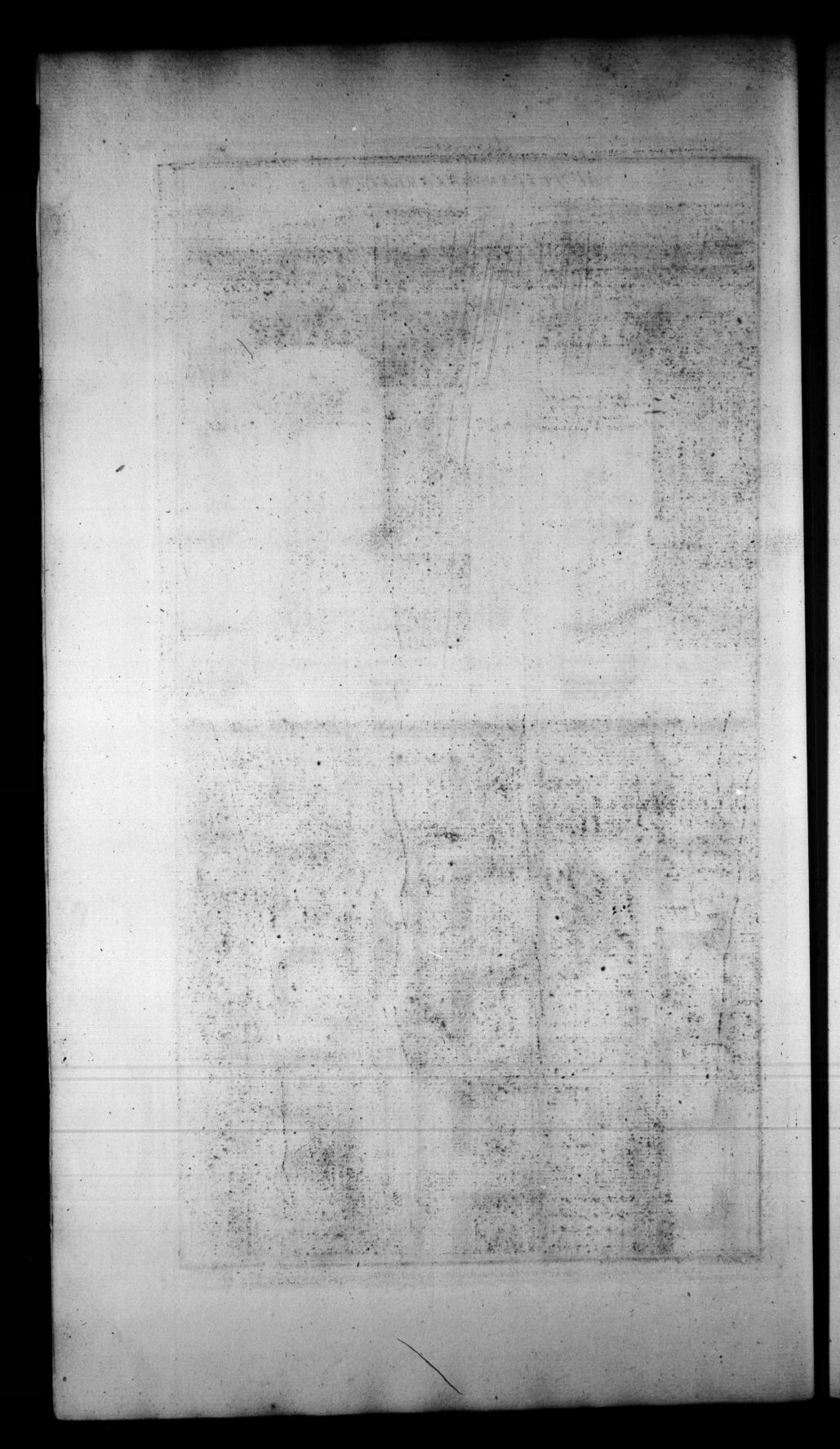
The Plan and Blovation of a Round or Circular Church, which is truly Noble & Grand, Juitable to the Jervice of Almighty God. There wants little or no Explanation, y whole disign being seen by Inspection. The Elevation is Half the Outside, and the Jection of Half y Inside, in the Center of the Arched Roof or Dome, is a Cupola, Consisting of two Orders of Columns, so contrived, as to be of little more Night, then those generally made of One Order and altho it should be much heavyer, yet the Butments and Arch is so strong, that it would bear ten times y Weight, The Invert on Steeple fory Bells &v is in y West Front as usual the some—thing different in Design from what I have seen.

The Ameland Orch, of Delinoanie

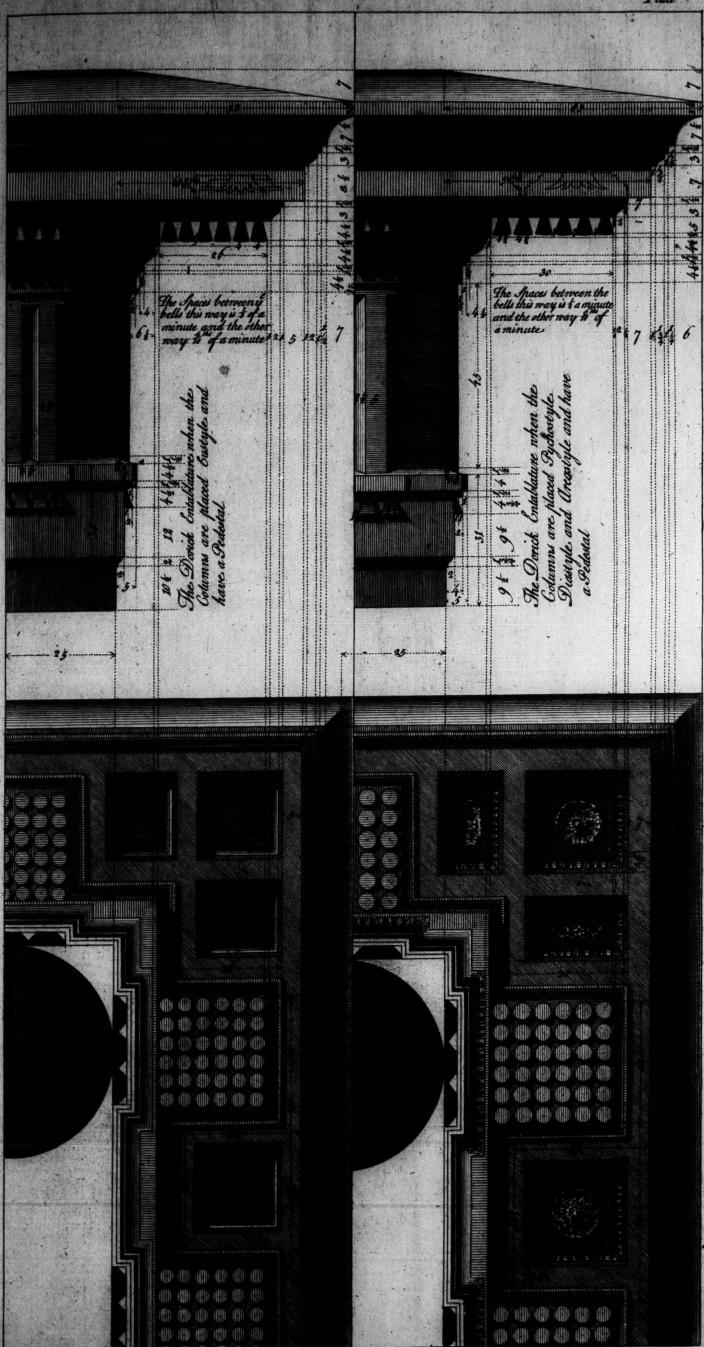
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